Simulation of the Finite Difference Time Domain in Two Dimension

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Abstract—The finite-difference time-domain (FDTD) method is one of the most widely used computational methods in electromagnetic. This paper describes the design of two-dimensional (2D) FDTD simulation software for transverse magnetic (TM) polarization using Berenger's split-field perfectly matched layer (PML) formulation. The software is developed using Matlab programming language. Numerical examples validate the software.

Keywords—Finite difference time domain (FDTD) method, perfectly matched layer (PML), split-filed formulation, transverse magnetic (TM) polarization.

I. INTRODUCTION

THE finite-difference time-domain (FDTD) method is a flexible and powerful solution tool for solving Maxwell's equations [1-5]. Further, the efficient and accurate solution of electromagnetic wave interaction problems in unbounded regions is one of the greatest challenges of the FDTD method. For such problems, an absorbing boundary condition (ABC) must be introduced at the outer grid boundary to simulate the extension of the grid to infinity.

Recently, among a few important studies on ABC was J.P. Berenger's Perfectly Matched Layer (PML) method [6]. In the PML, he created an artificial medium with magnetic conductivity (σ^*) that will make the boundary condition to work as wave absorber region. This paper describes the design of a two-dimensional (2D) FDTD simulation software for transverse magnetic (TM) polarized incident wave using Berenger's split-field perfectly matched layer (PML) formulation. The software is developed using Matlab programming language.

II. TWO-DIMENSIONAL TM POLARIZATION

The Maxwell's curl equations as modified by Berenger are expressed in their time-dependent form as,

$$\mu \frac{\partial H_x}{\partial t} + \sigma_y^* H_x = -\frac{\partial \left(E_{zx} + E_{zy}\right)}{\partial y} \tag{1}$$

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$$\mu \frac{\partial H_{y}}{\partial t} + \sigma_{x}^{*} H_{y} = \frac{\partial \left(E_{zx} + E_{zy} \right)}{\partial x}$$
(2)

$$\varepsilon \frac{\partial E_{zx}}{\partial t} + \sigma_x E_{zx} = \frac{\partial H_y}{\partial x}$$
(3)

$$\varepsilon \frac{\partial E_{zy}}{\partial t} + \sigma_y E_{zy} = -\frac{\partial H_x}{\partial y}$$
(4)

In order to solve these equations numerically, they are discretized according to finite differencing techniques. The central difference approximation is used in this case. For example, in equations (1) and (3), central differencing results in the following equations

$$H_{x}^{n+1}(i+1/2,j) = e^{-\sigma_{y}^{i}(i+1/2,j)\delta i/\mu} H_{x}^{n}(i+1/2,j)$$

$$-\frac{\left(1-e^{-\sigma_{y}^{i}(i+1/2,j)\delta i/\mu}\right)}{\sigma_{y}^{*}(i+1/2,j)\delta x} \begin{bmatrix} E_{zx}^{n+1/2}(i+1/2,j+1/2) + E_{zy}^{n+1/2}(i+1/2,j+1/2) \\ -E_{zx}^{n+1/2}(i+1/2,j-1/2) - E_{zy}^{n+1/2}(i+1/2,j-1/2) \end{bmatrix}$$

$$E_{zx}^{n+1/2}(i+1/2,j+1/2) = e^{-\sigma_{x}^{*}(i+1/2,j+1/2)\delta i/\varepsilon} E_{zx}^{n-1/2}(i+1/2,j+1/2)$$

$$-\frac{\left(1-e^{-\sigma_{x}^{*}(i+1/2,j+1/2)\delta i/\varepsilon}\right)}{\sigma_{y}^{*}(i+1/2,j+1/2)\delta x} \begin{bmatrix} H_{y}^{n}(i,j+1/2) - H_{y}^{n}(i+1,j+1/2) \end{bmatrix}$$
(6)

Based on the above formulation, a 2-D FDTD code has been written in Matlab programming language to simulate the fields of a plane wave source in lossy media. The formulation and the FDTD code are validated by checking the numerical results for homogeneous media against the analytical solution. The code for 2D FDTD is shown in Appendix.

In order to test and validate the FDTD code, an electromagnetic wave source interacting with dielectric cylinder ($\varepsilon_r = 4.0$, $\sigma = 0.12$) of radius 6 cm is simulated in this section, shown in Fig. 1. A 1 mW/cm² plane wave is used as source, and the frequency is setup to 2.5 GHz. The reason for using dielectric cylinder is there exist an analytical solution to this problem [7]. A +y-directed plane wave source :

ezy(:,jebc+2) = ezy(:,jebc+2) + 61.4*sin(omega*n*dt)is used to generate the incident wave at j = jebc + 2 and n = 1. Where *jebc* is thickness of the PML region, n is time step in FDTD code and dt is 5.0 psec. Fig. 2 shows a comparison of FDTD calculated results with analytic solution along the center axis o the cylinder. The simulation was made with a code attached in Appendix.



Fig. 1 Schematic representation of the FDTD computational domain



Fig. 2 Waveform comparison of the FDTD results (with different PML thicknesses) and the analytical solution for a plane wave source

III. PROCEDURE FOR PAPER SUBMISSION

In this section, various numerical simulations are performed to illustrate the effectiveness of PML code [8]. Fig. 3 shows the two FDTD computational domains used in the experiments: a test domain, $\Omega_{\rm T}$, and the much larger benchmark domain $\Omega_{\rm B}$. By calculating the difference between the FDTD solutions in the two domains at each grid-point at each time-step, a measure of the spurious reflection caused by the test ABC is obtained. Initially, a 2-D test domain 100×50 cells long was examined. A square cell was used, with $\delta = 0.015$ m, and the time step was chosen based on the stability criterion $\delta t = \delta/2c$, where *c* is the speed of light in vacuum. In all the cases examined here, the excitation was a pulse exhibiting a very smooth transition to zero, as used in [8], and defined as follows,

$$E_{z,T}\Big|_{50,25}^{n} = \begin{cases} \frac{1}{32} \begin{bmatrix} 10 - 15\cos(\pi n/20) + \\ 6\cos(2\pi n/20) - \cos(3\pi n/20) \end{bmatrix} & n \le 40 \ (7) \\ 0 & n > 40 \end{cases}$$



Fig. 3 Test and benchmark computational domains

Then, the local error of the computed field in $\Omega_{\rm T}$, due to reflections from the PML, is obtained by subtracting the field at any point within $\Omega_{\rm T}$ at a given time step from the field at the corresponding point in $\Omega_{\rm B}$. Here, E_z is used to define the error

$$e_{local}\Big|_{i,j}^{n} = E_{z,T}\Big|_{i,j}^{n} - E_{z,B}\Big|_{i,j}^{n}$$
(8)

where $E_{z,T}$ and $E_{z,B}$ are, respectively, the FDTD computed Efields within the test and benchmark domains. Further, the global error was defined as

$$e_{global}\Big|^{n} = \sum_{i} \sum_{j} \left| E_{z,T} \Big|_{i,j}^{n} - E_{z,B} \Big|_{i,j}^{n} \right|^{2}$$
(9)

In Fig. 4 and 5, different numbers of PML are used outside the FDTD simulation region to test the efficiency of the PML ABC for the lossy media. The accuracy of the PML ABC is compared with that of standard second-order Mur ABC [9]. The numbers of PML used are 16, 8 and 4, respectively. As is evident from the result, 16 PML are good enough to absorb most of the incident waves at the boundaries.

IV. CONCLUSION

The FDTD method is widely used because it is simple to implement numerically. It provides a flexible means for directly solving Maxwell's time-dependent curl equations by using finite differences to discretize them. This paper describes the design of two-dimensional (2D) FDTD simulation software for transverse magnetic (TM) polarized incident wave using Berenger's split-field perfectly matched layer (PML) formulation. The software is developed using Matlab programming language. The numerical results agree very well with the analytical results for homogeneous media.

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Fig. 4 Global error within a 100×50 cell two-dimensional TM test grid



Fig. 5 Comparative local error measures for Mur and PML ABCs along the test grid outer boundary at time-step n = 100.

APPENDIX

% *************************************
% Fundamental constants
% ******************
cc = 2.99792458e8; % speed of light in free space
muz = 4.0*pi*1.0e-7; %permeability of free space
$epsz = 1.0/(cc^*cc^*muz);$ % permittivity of free space
freq = $2.5e+9$; % frequency of source excitation
omega = 2.0*pi*freq;
% *******************
% Grid parameters
% *******************
ie = 50; %number of grid cells in x-direction
je = 50; %number of grid cells in y-direction
ib = ie + 1;
jb = je + 1;
dx = 3.0e-3; %space increment of square lattice
dt = dx/(2.0*cc); % time step
nmax = 500; % total number of time steps
ish a Que Of this har and a laft and sight DML sector
1 lebc = 8; % thickness of left and right PML region
$jebc = \delta;$ % unckness of front and back PML region
rmax = 0.00001;
orderbc = 2;

rmax = 0.00001; orderbc = 2; ibbc = iebc+1; jbbc = jebc+1;

iefbc = ie + 2*iebc;jefbc = je + 2*jebc; ibfbc = iefbc + 1;jbfbc = jefbc + 1;%***** ****** % Material parameters %******* ***** media = 2;eps = [1.0 4.0]; sig = [0.0 0.12]; mur = [1.0 1.0]; $sim = [0.0 \ 0.0];$ %********* ***** Field arrays % %********* ***** ez = zeros(ibfbc,jbfbc); %fields in main grid ezx = zeros(ibfbc,jbfbc); ezy = zeros(ibfbc,jbfbc); hx = zeros(iefbc,jefbc); hy = zeros(iefbc,jefbc); %***** ***** Updating coefficients % **** % for i = 1:media eaf = dt*sig(i)/(2.0*epsz*eps(i));ca(i) = (1.0-eaf)/(1.0+eaf);cb(i) = dt/epsz/eps(i)/dx/(1.0+eaf); $haf = dt^*sim(i)/(2.0^*muz^*mur(i));$ da(i) = (1.0-haf)/(1.0+haf);db(i) = dt/muz/mur(i)/dx/(1.0+haf);end ******* %** % Geometry specification (main grid) % ****** Initialize entire main grid to free space % caezx(1:ibfbc,1:jbfbc) = ca(1);cbezx(1:ibfbc,1:ibfbc) = cb(1);caezy(1:ibfbc,1:jbfbc) = ca(1);cbezy(1:ibfbc,1:jbfbc) = cb(1); dahxy(1:iefbc,1:jefbc) = da(1); dbhxy(1:iefbc,1:jefbc) = db(1); dahyx(1:iefbc,1:jefbc) = da(1); dbhyx(1:iefbc,1:jefbc) = db(1); Add dielectric cylinder % % diameter of cylinder: 6 cm diam = 40° rad = diam/2.0;% radius of cylinder: 3 cm ic = iefbc/2; % i-coordinate of cylinder's center jc = jefbc/2; % j-coordinate of cylinder's center for i = iebc+1:ie+iebc-1 for j = jebc+1:je+jebc-1 dist2 = (i-ic)^2 + (j-jc)^2; if dist2 <= rad^2 caezy(i,j) = ca(2);cbezy(i,j) = cb(2);caezx(i,j) = ca(2);cbezx(i,j) = cb(2);end end end ****** %*** % Fill the PML regions ***** %**** delbc = iebc*dx;sigmam=-log(rmax/100.0)*epsz*cc*(orderbc+1)/(2*delbc); bcfactor=eps(1)*sigmam/(dx*(delbc^orderbc) * ... (orderbc+1));

% FRONT region caezy(1:ibfbc,1) = 1.0; cbezy(1:ibfbc,1) = 0.0;

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for j = 2: jebc y1 = (jebc-j+1.5)*dx;y2 = (jebc-j+0.5)*dx;sigmay = bcfactor*(y1^(orderbc+1)-y2^(orderbc+1)); ca1 = exp(-sigmay*dt/(epsz*eps(1))); cb1 = (1.0-ca1)/(sigmay*dx);caezy(1:ibfbc,j) = ca1;cbezy(1:ibfbc,j) = cb1;end sigmay = bcfactor*(0.5*dx)^(orderbc+1); ca1 = exp(-sigmay*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmay*dx);caezy(1:ibfbc,jbbc) = ca1; cbezy(1:ibfbc,jbbc) = cb1; for j=1:jebc y1 = (jebc-j+1)*dx;y2 = (jebc-j)*dx;sigmay = bcfactor*(y1^(orderbc+1)-y2^(orderbc+1)); sigmays = sigmay*(muz/(epsz*eps(1))); da1 = exp(-sigmays*dt/muz); db1 = (1-da1)/(sigmays*dx);dahxy(1:iefbc,j) = da1;dbhxy(1:iefbc,j) = db1; end % BACK region caezy(1:ibfbc,jbfbc) = 1.0; cbezy(1:ibfbc,jbfbc) = 0.0;for j = 1: jebc-1 y1 = (j+0.5)*dx; $v^2 = (i - 0.5)^* dx;$ sigmay = bcfactor*(y1^(orderbc+1)-y2^(orderbc+1)); ca1 = exp(-sigmay*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmay*dx);caezy(1:ibfbc,jbfbc-jebc+j) = ca1;cbezy(1:ibfbc,jbfbc-jebc+j) = cb1; end sigmay = bcfactor* $(0.5*dx)^{(orderbc+1)}$; ca1 = exp(-sigmay*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmay*dx);caezy(1:ibfbc,jefbc-jebc+1) = ca1; cbezy(1:ibfbc,jefbc-jebc+1) = cb1; for j = 1:jebc y1 = j*dx;y2 = (j-1)*dx;sigmay = bcfactor*(y1^(orderbc+1)-y2^(orderbc+1)); sigmays = sigmay*(muz/(epsz*eps(1))); da1 = exp(-sigmays*dt/muz); db1 = (1-da1)/(sigmays*dx);dahxy(1:iefbc,jefbc-jebc+j) = da1; dbhxy(1:iefbc,jefbc-jebc+j) = db1; end % LEFT region caezx(1,1:jbfbc) = 1.0;cbezx(1,1:jbfbc) = 0.0;for i = 2:iebc x1 = (iebc-i+1.5)*dx;x2 = (iebc-i+0.5)*dx;sigmax = bcfactor*(x1^(orderbc+1)-x2^(orderbc+1)); ca1 = exp(-sigmax*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmax*dx);caezx(i,1:jbfbc) = ca1; cbezx(i,1:jbfbc) = cb1; end sigmax = $bcfactor^{*}(0.5^{*}dx)^{(orderbc+1)};$ ca1 = exp(-sigmax*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmax*dx);caezx(ibbc,1:jbfbc) = ca1; cbezx(ibbc,1:jbfbc) = cb1;

for i = 1:iebc x1 = (iebc-i+1)*dx; $x^2 = (iebc-i)^*dx;$ sigmax = bcfactor*(x1^(orderbc+1)-x2^(orderbc+1)); sigmaxs = sigmax*(muz/(epsz*eps(1))); da1 = exp(-sigmaxs*dt/muz); db1 = (1-da1)/(sigmaxs*dx);dahyx(i,1:jefbc) = da1; dbhyx(i,1:jefbc) = db1; end % RIGHT region caezx(ibfbc,1:jbfbc) = 1.0; cbezx(ibfbc,1:jbfbc) = 0.0; for i = 1 iebc-1 x1 = (i+0.5)*dx;x2 = (i-0.5)*dx;sigmax = bcfactor*(x1^(orderbc+1)-x2^(orderbc+1)); ca1 = exp(-sigmax*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmax*dx);caezx(ibfbc-iebc+i,1:jbfbc) = ca1; cbezx(ibfbc-iebc+i,1:jbfbc) = cb1; end sigmax = bcfactor*(0.5*dx)^(orderbc+1); ca1 = exp(-sigmax*dt/(epsz*eps(1))); cb1 = (1-ca1)/(sigmax*dx);caezx(ibfbc-iebc+1,1:jbfbc) = ca1; cbezx(ibfbc-iebc+1,1:jbfbc) = cb1; for i = 1:iebc $x1 = i^*dx;$ $x^2 = (i-1)^* dx;$ sigmax = bcfactor*(x1^(orderbc+1)-x2^(orderbc+1)); sigmaxs = sigmax*(muz/(epsz*eps(1))); da1 = exp(-sigmaxs*dt/muz); db1 = (1-da1)/(sigmaxs*dx);dahyx(iefbc-iebc+i,1:jefbc) = da1; dbhyx(iefbc-iebc+i,1:jefbc) = db1; end % *********** % BEGIN TIME-STEPPING LOOP for n = 1:nmax%****** ****** % Update electric field EZ in main grid %**** ezy(:,jebc+2) = ezy(:,jebc+2) + 61.4*sin(omega*n*dt);ezx(2:iefbc,2:jefbc)= caezx(2:iefbc,2:jefbc).*ezx(2:iefbc,2:jefbc) + ... cbezx(2:iefbc,2:jefbc).*(hyx(2:iefbc,2:jefbc)- hyx(1:iefbc-1,2:jefbc)); ezy(2:iefbc,2:jefbc)= caezy(2:iefbc,2:jefbc).*ezy(2:iefbc,2:jefbc) + ... cbezy(2:iefbc,2:jefbc).*(hxy(2:iefbc,1:jefbc-1)- hxy(2:iefbc,2:jefbc)); ez = ezx + ezy;%************

(ezx(1:iefbc,1:jefbc) + ezy(1:iefbc,1:jefbc) - ... ezx(1:iefbc,2:jbfbc) - ezy(1:iefbc,2:jbfbc));

hyx(:,:) = dahyx(:,:).*hyx(:,:) + dbhyx(:,:).*... (ezx(2:ibfbc,1:jefbc) + ezy(2:ibfbc,1:jefbc) - . ezx(1:iefbc,1:jefbc) - ezy(1:iefbc,1:jefbc));

% END TIME-STEPPING LOOP

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