

On The Design of Robust Governors of Steam Power Systems Using Polynomial and State-Space Based H_∞ Techniques: A Comparative Study

Rami A. Maher, Ibraheem K. Ibraheem

Abstract—This work presents a comparison study between the state-space and polynomial methods for the design of the robust governor for load frequency control of steam turbine power systems. The robust governor is synthesized using the two approaches and the comparison is extended to include time and frequency domains performance, controller order, and uncertainty representation, weighting filters, optimality and sub-optimality. The obtained results are represented through tables and curves with reasons of similarities and dissimilarities.

Keywords—Robust control, load frequency control, steam turbine, H_∞ -norm, system uncertainty, load disturbance.

I. BACKGROUND AND MOTIVATION

POWER system stability can be defined as that property of a power system that enables it to remain in state of operating equilibrium under normal operating conditions and to regain an acceptable state of equilibrium after being subjected to a disturbance. The quality of power supply must meet certain minimum standard requirements with special attention being given to the constancy of frequency [1], [2]. Our main concern in work paper concerns the above issue. Most universal method of electric generation is accomplished using thermal generation, and the most common machine for this production is the steam turbines. In the world most of the generation is powered by steam-turbine-driven generators [2]. Poor balancing between generated power and demand can cause the system frequency to deviate away from the nominal value, and create inadvertent power exchanges between control areas. To avoid such a situation, load frequency controllers (LFC) are designed and implemented to automatically balance between generated power and the demand power in each control area [1], [3], [4].

The problem of load frequency control has been investigated by many researchers. In [5] speed governors have been designed based on PID techniques with different philosophies because of its simplicity and ease of implementation. Fuzzy sliding mode controller for LFC has been designed in [6] to account for the system's parameters variations and the governor backlash. Genetic algorithm (GA) is a global search optimization technique. The researchers in

[7] used GA for tuning the control parameters of the proportional-integral (PI) control subject to the H_∞ constraints in terms of LMI. Modern control techniques have been reported in [8], [9] in which a load frequency controller for power systems has been designed using LQR techniques. The work in [10] investigated the design problem of robust load frequency controller using LMI methods for solving the H_∞ control problem. This paper is organized as follows: Section II describes the modeling of steam turbine system, Section III presents the design formulation for the H_∞ governor using polynomial and state-space approaches, Section IV is devoted to the performance evaluation of the robust governors. The conclusions are summarized in Section V.

II. STEAM TURBINES AND SPEED GOVERNING SYSTEM

A steam turbine converts stored energy of high pressure and high temperature steam into mechanical energy, which is in turn converted into electrical energy by the generator. The heat source for the boiler supplying the steam may be a nuclear reactor or a furnace fired by fossil fuel (coal, oil, or gas) [1], [2]. A typical mechanical-hydraulic speed governing system consists of a Speed Governor (SG), a Speed Relay (SR), a Hydraulic Servomotor (SM), and Governor-Controller Valves (CVs). In steam turbine-generator system, the governing is accomplished by a speed transducer, a comparator, and one or more force-stroke amplifiers. Fig. 1 depicts the complete system block diagram of a steam turbine generator [2].

Speed Governor (SG):

$$S_G = \frac{1}{R} \quad (1)$$

where R is the steady-state speed regulation. The value of R determines the steady-state speed load characteristic of the generating unit.

Speed Relay (SR):

$$S_R(s) = \frac{1}{sT_{SR} + 1} \quad (2)$$

where T_{SR} is the time constant of the speed relay.

Rami A. Maher is with Isra University, Electrical Engineering Department, P.O. 11622, Amman, Jordan. (e-mail: ramiamahir@yahoo.com).

Ibraheem K. Ibraheem is with the Department of Electrical Eng. Dept. / Engineering College / Baghdad University, Iraq (phone: 009647702562658; P.O.B: 47273; e-mail: ibraheem151@gmail.com).

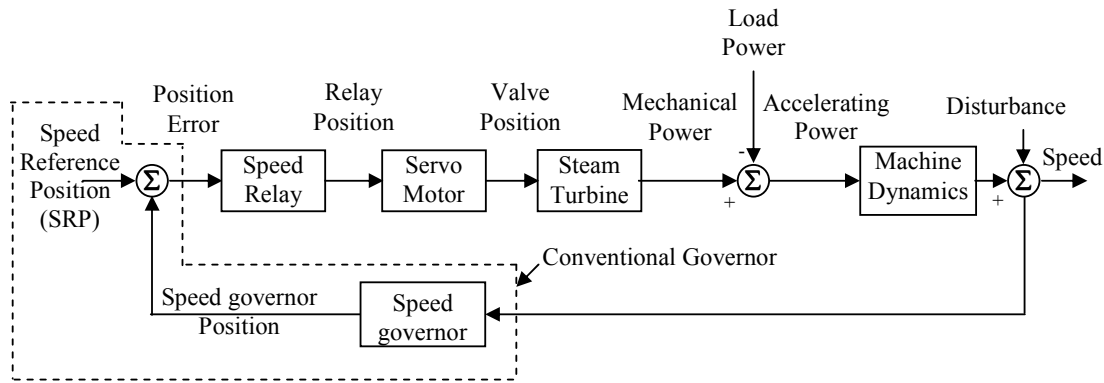
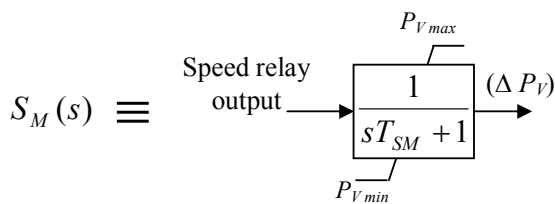
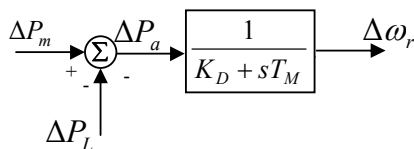


Fig. 1 Block diagram of steam turbine control system

Servo Motor (SM):Fig. 2 Servo Motor transfer function representation
 T_{SM} is the time constant of the servo motor**Steam Turbine (ST):**

$$S_T(s) = \frac{\Delta P_m}{\Delta P_V} = \frac{(F_{HP}(sT_{CO}+1)(sT_{RH}+1) + F_{LP}(sT_{CO}+1) + F_{LP})}{(sT_{CH}+1)(sT_{CO}+1)(sT_{RH}+1)} \quad (3)$$

where T_{CO} , T_{RH} , T_{CH} are the time constants for the cross over, reheater, and steam chest respectively.

Machine Dynamics (MD):Fig. 3 Transfer function representation of the synchronous machine
 T_M is the mechanical starting time, ΔP_m is the incremental change of the mechanical power, ΔP_L is the incremental change of load power, ΔP_a is the incremental change of accelerating power, $\Delta \omega_r$ is the deviation of the angular speed of the synchronous generator

The model of the complete steam turbine system has been derived with typical values of the listed in Table I [1], [2], [11]. This model is applicable to a tandem-compound single reheat turbine of fossil-fuelled units.

III. ROBUST GOVERNOR DESIGN PROCEDURE

A different configuration for the problem of LFC of steam turbine has been proposed in this work as shown in Fig. 4.

Parameter	Description	Value	Unit
K_D	Damping factor = torque (pu) / speed (pu)	2	pu
T_M	Mechanical starting time	8	sec
F_{IP}	IP turbine power fraction	0.4	-
F_{LP}	LP turbine power fraction	0.3	-
F_{HP}	HP turbine power fraction	0.3	-
T_{CO}	Crossover time constant	0.4	sec
T_{SR}	Speed relay time constant	0.1	sec
T_{SM}	Servomotor time constant	0.2	sec
T_{CH}	Steam chest time constant	0.25	sec
T_{RH}	Reheater time constant	7	sec
P_{Vmax}	Maximum valve position	1	pu
P_{Vmin}	Minimum valve position	0	pu
f_o	Speed disturbance bandwidth	0.5-2	Hz

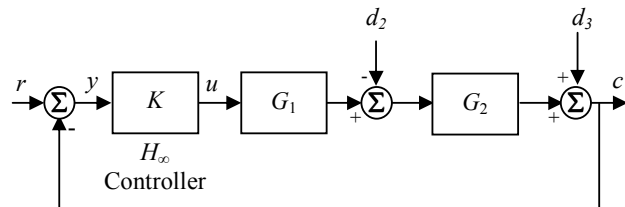


Fig. 4 Proposed configuration for LFC of steam turbine

IN the proposed configuration the controller (governor) is placed in the feed forward path in contrast to the conventional governor in which the controller is positioned in the feed backward path. In what follows the above proposed configuration together with the robustness tools will be used to setup the problem within the framework of the H_∞ design methodology using the polynomial methods.

A. Formulation of the Design Problem: A Polynomial Approach

Fig. 5 represents the mixed sensitivity problem for steam turbine plant which includes the performance shaping filters ($V(s)$ and $W_1(s)$) and the uncertainty filters $W_2(s)$ where additive uncertainty is used to compensate for neglected dynamics which is represented as unstructured uncertainty through $W_2(s)$, Δ Stable unknown transfer function. The

design of the shaping filters is highly depends on the model at hand and certain considerations have to be taken in the design of these shaping filters like uncertainty, high frequency roll-off, and integral control.

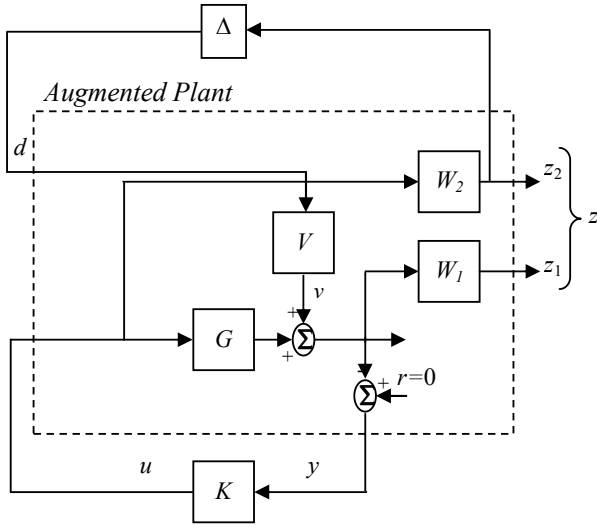


Fig. 5 Mixed Sensitivity Configuration

$$G(s) = \frac{N(s)}{D(s)}, \quad V(s) = \frac{M(s)}{D(s)}, \quad W_1(s) = \frac{A_1(s)}{B_1(s)}, \quad W_2(s) = \frac{A_2(s)}{B_2(s)}$$

Fig. 5 defines the standard problem whose generalized plant has the following transfer function matrix [12]-[13]:

$$[z] = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix}, \quad \begin{bmatrix} z \\ y \end{bmatrix} = P \begin{bmatrix} d \\ u \end{bmatrix}$$

$$P = \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix} = \begin{bmatrix} W_1 V & W_1 G \\ 0 & -W_2 \\ -V & -G \end{bmatrix} = \begin{bmatrix} \frac{A_1 M}{B_1 D} & \frac{A_1 N}{B_1 D} \\ 0 & \frac{A_2}{B_2} \\ -\frac{M}{D} & -\frac{N}{D} \end{bmatrix}$$

$$= D^{-1} N = [D_1 \quad D_2]^{-1} [N_1 \quad N_2] \quad (4)$$

The mixed sensitivity problem schematized above is the problem of minimizing the H_∞ -norm of the closed-loop transfer function matrix [12]-[13]:

$$T_{zw}(s) = \begin{bmatrix} W_1 S V \\ W_2 R V \end{bmatrix} \quad (5)$$

where $\begin{bmatrix} z_1 \\ z_2 \end{bmatrix} = T_{zw}(s) [d]$

Now the problem can be stated as:

Design a stabilizing controller such that the H_∞ -norm $\|T_{zw}(s)\|_\infty$ of the above closed-loop transfer function is minimized, i.e. $\|T_{zw}(s)\|_\infty \leq \gamma$. Knowing that T_{zw} is the closed-loop transfer matrix defined as [12], [13]:

$$T_{zw} = F_l(P, K) = P_{11} + P_{12} K (I - P_{22} K)^{-1} P_{21} \quad (6)$$

γ is the solution of the H_∞ optimization, and $F_l(P, K)$ lower linear fractional transformation. In the SISO case the H_∞ -norm of T_{zw} is given by [14], [15]:

$$\|T_{zw}\|_\infty = \sup_{-\infty < \omega < \infty} \left(|W_1(j\omega) S(j\omega) V(j\omega)|^2 + |W_2(j\omega) R(j\omega) V(j\omega)|^2 \right) \quad (7)$$

where sup is the supremum or the least upper bound. With suitably chosen weighting filters matrices W_1 , W_2 and V a suitably chosen shaping matrix. The selection of the weighting filters is not an easy task for a specific design problem and often involves ad hoc, and fine-tuning. It is very hard to give a general formula for the weighting filters that will work in every case. Finally, the selection of the uncertainty weighting filter depends on the dynamics of the system and the nominal model chosen. After a thorough analysis, the weighting filters are found to be:

$$W_1(s) = \frac{s + 0.85}{s}$$

$$W_2(s) = \frac{(272s + 0.08) \cdot (s + 80)}{(1000s + 80) \cdot 160}$$

$$V(s) = \frac{M_{nom}(s)}{D_{nom}(s)} = \frac{(s + 2)(0.72 + 1.2s + s^2)}{(0.25s + 1)(7s + 1)(8s + 2)}$$

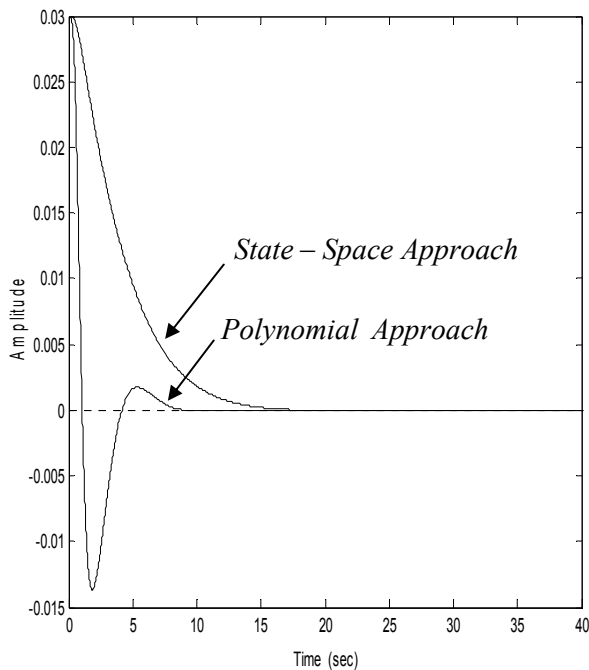
B. Formulation of the Design Problem: A State-Space Approach

The block diagram of the augmented plant including the performance and uncertainty weighting filters together with plant is shown in Fig. 6 where an output multiplicative uncertainty is assumed in the system as indicated by the uncertainty weighting filter $W_I(s)$ and the input d_1 . In symbolic notations:

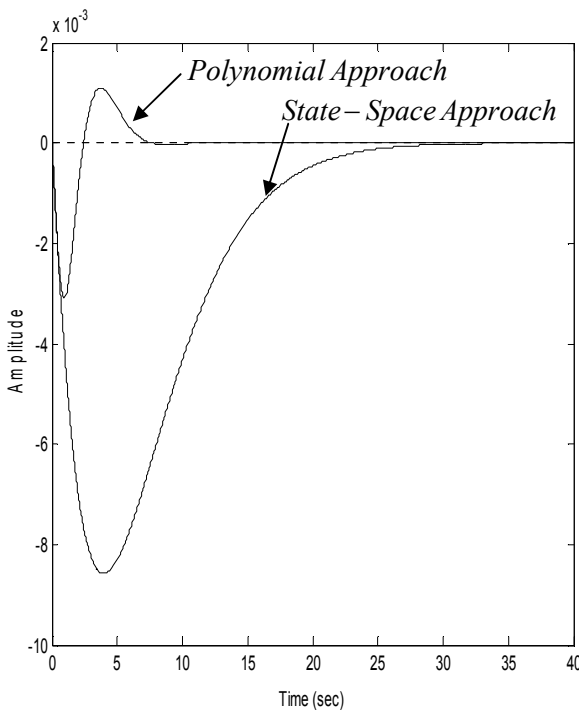
$$z = \begin{bmatrix} z_1 \\ z_2 \\ z_3 \end{bmatrix}, \quad w = \begin{bmatrix} d_1 \\ d_2 \\ d_3 \end{bmatrix}, \quad \begin{bmatrix} z \\ y \end{bmatrix} = P(s) \begin{bmatrix} w \\ u \end{bmatrix} = \begin{bmatrix} P_{11}(s) & P_{12}(s) \\ P_{21}(s) & P_{22}(s) \end{bmatrix} \begin{bmatrix} w \\ u \end{bmatrix} \quad (8)$$

According to these definitions, the open loop generalized plant can be obtained as [16], [17]:

$$P(s) = \begin{bmatrix} 0 & 0 & 0 & W_I G_1 \\ 0 & 0 & 0 & W_U \\ W_p G_2 & -W_p G_2 & W_p W_{D3} & W_p G_1 G_2 \\ -G_2 & G_2 & -W_{D3} & G_1 G_2 \end{bmatrix} := \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix} \quad (9)$$



(a)



(b)

Fig. 7 Transient response of $\Delta\omega_r$ in response to, (a) Speed disturbance step change, (b) Load disturbance step change

Finally, Integral control can be designed easily in the polynomial approach than the state-space approach. The reason is state-space approach doesn't accept a pole on $j\omega$ -

axis in the weighing functions or the plant $G(s)$, while there is no such limitation in the polynomial approach. Furthermore, high frequency roll-off can be obtained by using improper weighting filters in the design procedure. This can be done in the polynomial approach by using improper $W_2(s)$ which is not allowed in the state-space approach.

TABLE II
TIME DOMAIN SPECIFICATIONS OF THE CLOSED LOOP SYSTEM

Parameter	State-Space Approach		Polynomial Approach	
	Without uncertainty	With uncertainty	Without uncertainty	With uncertainty
Settling time /sec	23.7	20.3	7.06	10.4
Undershoot	8.58×10^{-3}	8.46×10^{-3}	5.56×10^{-3}	4.27×10^{-3}

TABLE III
ORDERS OF H_∞ CONTROLLER FOR DIFFERENT APPROACHES

Parameter	State-Space Approach		Polynomial Approach	
	Without uncertainty	With uncertainty	Without uncertainty	With uncertainty
Formula	$\text{ord}(G) + \text{ord}(W_p) + \text{ord}(W_t) + \text{ord}(W_f)$		$\text{ord}(G) + \text{ord}(1/W_2)$	
Order	8	6	7	5
Order after reduction	5	4	3	2

TABLE IV
FREQUENCY DOMAIN SPECIFICATIONS OF THE CLOSED-LOOP SYSTEM

Parameter	State-Space Approach		Polynomial Approach	
	Without uncertainty	With uncertainty	Without uncertainty	With uncertainty
Phase Margin	78°	72°	37°	32°
Gain Margin /dB	25	56	8.3	11
Phase crossover frequency rad/sec	2.68	3.91	3.58	2.375
Gain crossover frequency rad/sec	0.227	0.26	1.4	0.965

V. CONCLUSION

In this research, a comparison study is introduced to solve the problem of the load frequency control for the steam turbines of the power systems. Both approaches result in a proposed robust controller which ensures both robust stability and robust performance and satisfy time and frequency domains specifications but it is important to stress that better results, with respect to the transient response characteristics are obtained by using the polynomial approach while state-space approach achieves slightly better results in the frequency domain than the polynomial approach. Finally, problem formulation and satisfying the design requirements is much easier to do with the polynomial approach than with the state-space one.

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