

Compact Slotted Broadband Antenna for Wireless Applications

M. M. Sharma, Swati Gupta, Deepak Bhatnagar, and R. P. Yadav

Abstract—This paper presents the theoretical investigation of a slotted patch antenna. The main objective of proposed work is to obtain a large bandwidth antenna with reduced size. The antenna has a compact size of 21.1mm x 20.25mm x 8.5mm. Two designs with minor variation are studied which provide wide impedance bandwidths of 24.056% and 25.63% respectively with the use of parasitic elements when excited by a probe feed. The advantages of this configuration are its compact size and the wide range of frequencies covered. A parametric study is also conducted to investigate the characteristics of the antenna under different conditions. The measured return loss and radiation pattern indicate the suitability of this design for WLAN applications, namely, Wi-Max, 802.11a/b/g and ISM bands.

Keywords—Inset feed, microstrip antenna, parasitic patch, shorting wall, slot, wi-max.

I. INTRODUCTION

EXTENSIVE research has been done on microstrip antennas in recent years to exploit their small size and low cost. Although these antennas have proved to be excellent radiators for various applications; they have an inherently narrow bandwidth and low gain. The bandwidth, typically 1-2% is a major limiting factor for the widespread application of these antennas. Various techniques have been implemented in the past to overcome these shortcomings including the use of parasitic elements and multilayer configurations [1]-[5]. Thick, low permittivity substrates have also been used [5] - [6], which further increase the size and inductivity of the antenna. Size reduction is obtained by shorting the patch with the ground plane using a wall or a pin at the point of minimum voltage [1, 3, 5]. These advancements have witnessed a corresponding progress in the fields where microstrip antennas are used. Recent years have witnessed tremendous

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advancements in wireless communications technologies. Technologies such as UWB [4] have been identified as potentially revolutionary in the coming years.

In this paper, the radiation performance of a compact slotted broadband antenna is obtained by electromagnetic coupling with a parasitic element and by designing it on a thick low permittivity substrate. The design is simulated using 'Microstripes 7.5TM' [7] based on the TLM technique of analysis. The present structure is intended for use with the existing and upcoming wireless communication systems.

II. ANTENNA DESIGN

In this paper, we have proposed a compact slotted antenna having dimensions $L1 \times W1$ and designed on a thick foam substrate having relative permittivity equal to 1.04 and a loss tangent equal to 0.0016. A shorting wall having dimensions 3mm x 1mm x 7mm is used as shown in Fig. 1. The ground plane of antenna has a size of 40mm x 40 mm. Adjacent to the radiating patch, a parasitic patch of dimensions $L2 \times W2$ is placed as shown in Fig. 1. For the present investigations, two sets of parameters with small variations in slot size and dimensions of the parasitic element are considered. These are: For Design - 1: $L1 = 15\text{mm}$, $W1 = 9\text{mm}$, $L2 = 20.25\text{mm}$, $W2 = 9.6\text{mm}$
For Design - 2: $L1 = 15\text{mm}$, $W1 = 9\text{mm}$, $L2 = 16.4\text{mm}$, $W2 = 8.2\text{mm}$

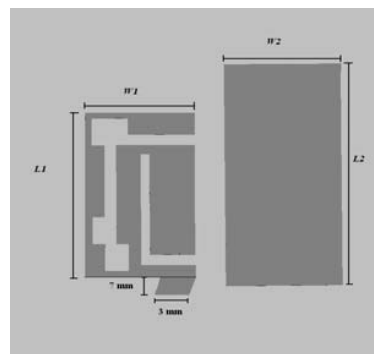


Fig. 1 Antenna geometry with dimensions of the radiating patch and the parasitic patch

Through top view of these antenna geometries in Fig. 2a and Fig. 2b, internal dimension corresponding to Design-1 and Design-2 are shown. Fig. 2c shows a 3-dimensional view of this geometry. Both these geometries have inset feed as shown in Fig. 2a and Fig. 2b.

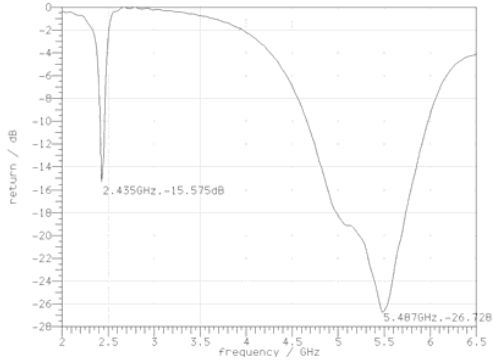


Fig. 3 (a) Variation of return loss with frequency (Design-1)

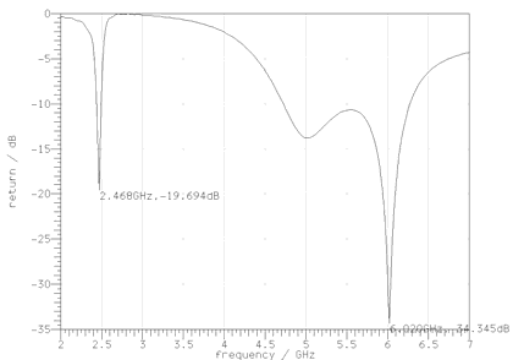


Fig. 3 (b) Variation of return loss with frequency (Design-2)

cut are still in broadside direction ($\theta = 0^\circ$) but for 135° cut maximum radiation is obtained in $\theta = 255^\circ$. The 3dB beamwidth for Design-2 in these two cuts are 165.782° and 52.09° respectively.

The gain, directivity and antenna efficiency of Design-1 for the 5.487 GHz frequency band are 4.633 dBi, 4.657dBi and 99.433% respectively are obtained while for 2.435GHz band, these are 0.978 dBi, 1.889 dBi and 91.542% respectively. For Design-2, corresponding to 6.020 GHz band, gain, directivity and antenna efficiency are 5.640 dBi, 5.642 dBi, 99.96% respectively while the 2.468 GHz band these are 1.294 dBi, 1.337 dBi and 99.007% respectively. It is noticed that the parasitic patch enhances the bandwidth of the antenna. Design-1 without a parasitic patch yields a lower gain (0.618 dBi less at the higher resonant frequency of the geometry) and a bandwidth 2.76% less than that of the proposed design. The shorting wall and the slots on the parasitic patch also enhance the response remarkably. Design-1 without a parasitic patch and a shorting wall has a return loss greater than -10dB. The return loss falls to below -10dB with the introduction of a shorting wall and a bandwidth of 8.38% is obtained. Further introduction of slots increases the bandwidth to 24.056%.

A parametric study of the antenna is also conducted to investigate its response to the parasitic patch as well as the substrate thickness. The parameters $L2$, $W2$, substrate thickness h , and the distance between the radiating and parasitic patches d for design1 are selected for parametric study. All the other parameters are kept invariant. The results are shown in Table I. Some interesting results are obtained

from this study. On increasing the separation, between the radiating and parasitic patches, $F2/F1$ ratio increases almost linearly.

The bandwidth corresponding to frequency $F1$ decreases marginally then increases till separation is made $d = 2.5$ mm and finally it decreases. Similarly gain and antenna efficiency corresponding to frequency $F1$ decreases on increasing separation, between the radiating and parasitic patches but corresponding to frequency $F2$, both these parameters increases marginally.

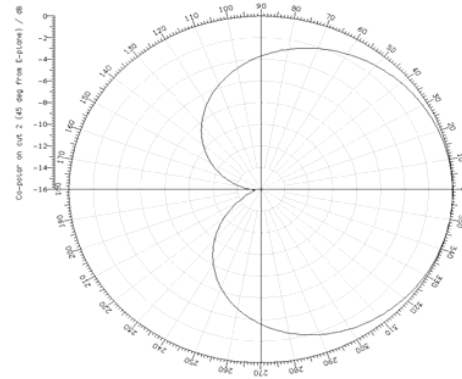


Fig. 4 (a) Co-polar radiation pattern at 45 degrees cut from the E-plane (Design-1) at 2.435 GHz

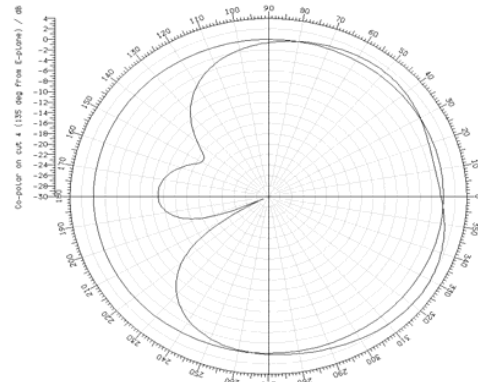


Fig. 4 (b) Co-polar radiation pattern at 135 degrees cut from the E-plane (Design-1) at 5.487 GHz

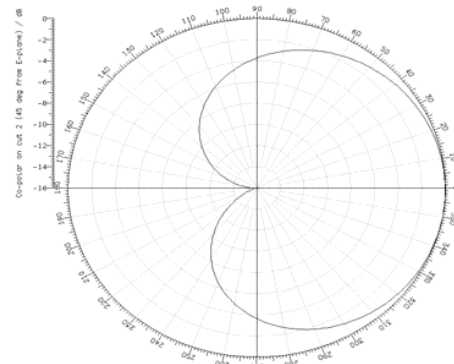


Fig. 5 (a) Co-polar radiation pattern at 45 degrees cut from the E-plane (Design -2) at 2.468 GHz

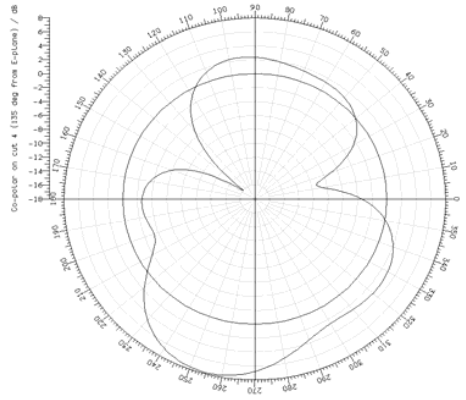


Fig. 5 (b) Co-polar radiation pattern at 135 degrees cut from the E-plane (Design-2) at 6.020 GHz

On increasing substrate height, bandwidth of antenna corresponding to frequency F₂ increases. Similarly on increasing parameters L₂ and W₂, bandwidth of antenna increases significantly. In this communication, more emphasis is given to the enhancement of bandwidth of antenna. One must keep in mind that the gain-bandwidth product for an antenna remains almost constant therefore improved bandwidth values at the cost of reduced gain values are accepted in this communication. The antenna geometries proposed in this communication are suitable for applications in various wireless systems applicable for Wi-Max-802.16, 802.11a/b/g and ISM bands. These may also be used for ultrawideband signals.

IV. CONCLUSION

A compact slotted broadband antenna is proposed. It is observed that with appropriate substrate height, separation between radiating and parasitic patch and dimensions of parasitic patch, a higher bandwidth and antenna efficiency may be achieved which are the main requirements for an antenna applicable for modern communication systems including wireless systems.

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TABLE I
PARAMETRIC STUDY OF ANTENNA GEOMETRIES UNDER DIFFERENT CONDITIONS

PARAMETER	VALUE (mm)	OTHER PARAMETER VALUES (mm)	F ₁ (GHz)	F ₂ (GHz)	F ₂ /F ₁	BW (%)		GAIN (dBi)		ANTENNA EFFICIENCY (%)	
						F ₁	F ₂	F ₁	F ₂	F ₁	F ₂
d	0.5	h = 7 W ₂ = 9.6 L ₂ = 20.25	2.358	5.078	2.153	2.078	14.021	1.097	4.958	91.894	97.209
	1.5		2.422	5.312	2.193	2.023	22.816	1.020	4.607	91.816	99.256
	2.5		2.435	5.487	2.253	1.889	24.056	0.978	4.633	91.542	99.433
	3.5		2.444	5.689	2.327	1.882	22.99	0.948	5.969	91.120	99.547
h	5	d = 2.5 W ₂ = 9.6 L ₂ = 20.25	2.456	5.565	2.265	1.87	14.86	0.781	4.705	88.919	93.255
	6		2.441	5.425	2.222	1.925	20.921	0.906	4.821	90.591	99.076
	7		2.435	5.487	2.253	1.889	24.075	0.978	4.633	91.542	99.433
	8		2.422	5.510	2.274	1.857	26.297	1.011	4.521	91.32	98.762
W ₂	7.6	d = 2.5 h = 7 L ₂ = 20.25	2.436	5.493	2.254	1.88	23.903	0.956	4.688	91.233	99.565
	8.6		2.436	5.485	2.251	1.847	23.956	0.967	4.668	91.380	99.603
	9.6		2.435	5.487	2.253	1.889	24.056	0.978	4.633	91.542	99.433
	10.6		2.434	5.488	2.254	1.93	24.125	0.990	4.591	91.705	99.045
	11.6		2.434	5.581	2.292	1.93	23.99	1.003	4.571	91.854	98.437
L ₂	18.25	d = 2.5 h = 7 W ₂ = 9.6	2.433	5.586	2.295	1.849	21.876	0.980	5.160	91.577	99.521
	19.25		2.433	5.559	2.284	1.89	23.007	0.985	4.886	91.616	99.515
	20.25		2.435	5.487	2.253	1.889	24.075	0.978	4.633	91.542	99.433
	21.25		2.435	5.338	2.192	1.889	25.327	0.980	4.395	91.587	99.437