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Carbon Dioxide Recovery by Membrane Assisted Crystallization

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 $\mbox{\it Abstract}$ —This study addresses the effect of impurities on the crystallization of Na_2CO_3 produced within a strategy for capturing CO_2 from flue gases by alkaline absorption. A novel technology - membrane assisted crystallization - is proposed for Na_2CO_3 crystallization from mother liquors containing impurities. High purity of $Na_2CO_3 {\bullet} 10 H_2O$ crystals was obtained without impacting the performance of the mass transfer of water vapor through membranes during crystallization.

Keywords—Carbon dioxide recovery, crystal morphology, membrane crystallization, purity.

I. INTRODUCTION

THE prospect of global warming due to the tremendous rise of CO_2 concentration in the atmosphere has attracted worldwide concerns [1]. Membrane contactors have been proposed as an advanced technology for CO_2 capture from flue gases by absorption in alkaline solutions [2]. However, regeneration of the alkaline reagent and further CO_2 sequestration are pending issues. In this work, membrane assisted crystallization is proposed for crystallizing Na_2CO_3 , which allows its reuse, after CO_2 absorption from flue gases.

Due to the existence of impurities (i.e., NO_x, SO₂) in the gas stream other than CO₂, the impurities (Na₂SO₄ and NaNO₃) that may be present and may play an influence on the crystallization of Na₂CO₃. In this study, we aim at investigating the possibility of crystallizing Na₂CO₃ crystals with high purity from a Na₂CO₃ solution containing impurities, such as NaNO₃, and Na₂SO₄ in order to consider the presence of impurities from flue gases and NaCl from a realistic scenario namely the osmotic solution for crystallization. The morphology and purity of the Na₂CO₃ crystal were evaluated to investigate the interference posed by these impurities [3].

II. APPROACH

A hollow fiber membrane contactor was used as the system to perform the membrane assisted crystallization. The characteristics of the membrane contactor are shown in Table I.

 $\label{table I} TABLE\ I$ Characteristics of Membrane Contactor and Hollow Fibers

| Housing Characteristics | | | | | | | |
|------------------------------|----------------------------|--|--|--|--|--|--|
| Material | Polycarbonate/polyurethane | | | | | | |
| Cartridge configuration | Parallel Flow | | | | | | |
| Hollow Fiber Characteristics | | | | | | | |
| Membrane | X50 Fiber | | | | | | |
| Material | Polypropylene | | | | | | |
| Porosity | 40% | | | | | | |
| Effective pore size | 0.04 μm | | | | | | |
| Internal diameter | 220 μm | | | | | | |
| Outer diameter | 300 μm | | | | | | |
| Active surface area | 0.18 m^2 | | | | | | |
| Number of fibers | 2300 | | | | | | |

The microporous hydrophobic membrane acts as the physical support to separate the mother solution (i.e., Na₂CO₃) from the osmotic solution flow (i.e., NaCl) under isothermal conditions. The hydrophobic nature of the membrane allows the transfer of water between the Na₂CO₃ solution and NaCl solution through the pores as vapor phase. Furthermore, the hydrophobic membrane can also avoid both the Na₂CO₃ and NaCl solutions from wetting the membrane. The driving force for the mass transfer in a membrane contactor mainly depends on the vapor pressure gradient between the bulk solutions at both interfaces of membrane, which is created by a difference in their activities [3]. Thus, the overall mass transfer coefficient can be obtained experimentally according to (1):

$$J_{w} = K_{tot}(p_{p}^{*}a_{p} - p_{f}^{*}a_{f})$$
 (1)

where $J_{\rm w}$ is the transmembrane flux obtained from the experiment, $K_{\rm tot}$ is the overall mass transfer coefficient, $a_{\rm f}$ and $a_{\rm p}$ are the water activities, $p_{\rm f}^*$ and $p_{\rm p}^*$ are the water vapor pressures of the feed solution and draw solution, respectively.

The pure water vapor pressure $(p^*(T), Pa)$ which depends on the temperature $(T, {}^{\circ}C)$ can be calculated by the following equation [4]:

$$p^{\text{vap}}(T) = 133.32 \exp\left(8.07131 - \frac{1730.63}{233.426 + T}\right)$$
 (2)

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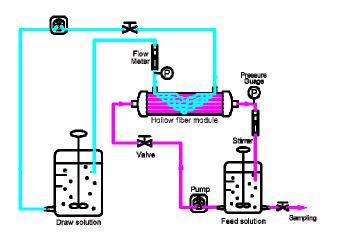


Fig. 1 Schematic diagraph of the experimental setup

Fig. 1 shows the schematic diagram of the experimental setup for membrane assisted crystallization. Two peristaltic pumps (Watson Marlow 503S-Belgium and Gilson Minipuls III-The Netherlands) were used to circulate the feed stream and the stripping stream from the cylindrical glasses to the membrane contactor in a counter-current mode. All the experiments were performed at room temperature $(20 \pm 1^{\circ}C)$.

A morphological assessment was performed for the grown crystals by imaging with an Olympus Microscope. A Dionex ICS-2000 ion chromatograph was used for detecting the possible anion impurities (Cl⁻, NO₃⁻, SO₄²⁻) in the crystals.

III. RESULTS AND DISCUSSION

A. Effect of Impurities on the Morphology of the Crystals

In order to investigate the influence of the impurities on the shape of the obtained crystals, the morphology of the crystals obtained from Na₂CO₃ solutions doped with the impurities is shown in Fig. 2.

The images of grown crystals in Figs. 2 (b) and (c) demonstrate that the morphology of the crystal surfaces was approximately the same as the reference compound (Fig. 2 (a)). Due to the morphology of the crystal surface has a strong dependency on the growth step [5], it can be implied that NO₃ and Cl⁻ impurities had no significant influence on the Na₂CO₃ crystal growth rate. However, the presence of SO₄²⁻ (Fig. 2 (d)) has a strong influence on the shape of the crystals and triclinic crystals were obtained. Impurities affect the morphologies of the crystals in several ways: (1) Adsorbing to the growth surface, thus bringing to a halt for the material delivery to the crystal surface; (2) Causing a decrease of the specific surface energy for crystal growth; or an interruption for the surface sites and prevention for the growing steps of crystals [4]. Thus, the impurity of Na₂SO₄ may adsorb on a certain surface of Na₂CO₃ crystals when they were growing, leading to a decrease of the growth steps of that specific surface, and determining the shape of the crystals.

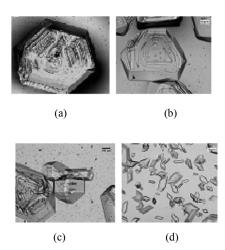


Fig. 2 Microscopy images of Na₂CO₃ crystals. Feed solution containing 200 g/L Na₂CO₃ with: a) no impurities; b) 0.6 mol/L NaNO₃; c) 0.6 mol/L NaCl; and d) 0.6 mol/L Na₂SO₄

B. Effect of Impurities on the Purity of Obtained Crystals

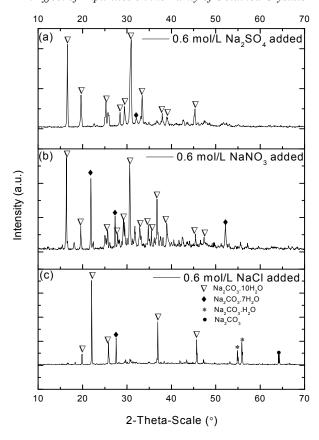


Fig. 3 XRD patterns of crystals obtained from solutions of Na₂CO₃ mixed with different impurities: (a) Na₂SO₄; (b) NaNO₃; (c) NaCl

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Fig. 3 shows the XRD patterns of the crystals from the feed solution doped with 0.6 mol/L impurities of Na₂SO₄ (Fig. 3 (a)), NaNO₃ (Fig. 3 (b)), and NaCl (Fig. 3 (c)), respectively. It can be observed that no peaks in the XRD patterns related to compounds other than Na₂CO₃ appear. It indicates that the kind of impurities has no apparent effect on the crystallography of Na₂CO₃ formed by membrane assisted crystallization, with the main XRD pattern of Na₂CO₃·10H₂O. Furthermore, no impurity crystalline patterns were observed in crystals, which means no co-crystallization happened during membrane crystallization of Na₂CO₃. However, when a common evaporator is used, co-crystallization of the impurities was observed and different crystals, such as the burkeite crystal, Na₂CO₃·2Na₂SO₄ or sodium dicarbonate crystals, can form after crystallization in the Na₂CO₃ solution with a high concentration of Na₂SO₄ [6]. This is due to the fact that the common evaporator is operated at high temperature (above 100 °C). To comparison, membrane crystallization can avoid the co-crystallization since it can be operated at a controllable

temperature, and works at a room temperature [7], [8].

The final purity of the obtained crystals is shown in Table II. As it shows in Table II, crystals from Na_2CO_3 solutions doped with different kind of salts in different concentrations had the same high purity as the reference, higher than for conventional crystallization technology (99.0% purity of Na_2CO_3 from Na_2CO_3 and Na_2SO_4 mixed solution) [9]. This is due to the fact that membrane crystallization allows the water to evaporate slower (as it shows in Table III) than traditional evaporators ($\sim 0.0936 \text{ kg.h}^{-1}$) [8], resulting in a lower supersaturation rate. Thus target products can grow in a controllable supersaturation rate in membrane crystallizers [8].

As it indicates in Table III, the mass transfer coefficient is almost constant within the range of uncertainty, which means that the mass transfer coefficient is irrespective of concentration of impurities and the kind of impurities. The impurities pose no negative effect on the performance of the membranes.

TABLE II Final Purity in Obtained Crystals from Mixed Solutions

| THAT I CAN I IN OBTAINED CATOTALD TROWN WINED GOLD TIONS | | | | | | | | | | | |
|---|---|----------|--------|--------|--------|--------|--------|------------|--------|--------|--|
| | | Impurity | | | | | | | | | |
| | Reference Na ₂ CO ₃ * | $NaNO_3$ | | | NaCl | | | Na_2SO_4 | | | |
| Initial concentration of impurities in feed solution (mol·L ⁻¹) | 0 | 0.2 | 0.4 | 0.6 | 0.2 | 0.4 | 0.6 | 0.2 | 0.4 | 0.6 | |
| W _{Na2CO3} (%) | ≥99.37 | ≥99.50 | ≥99.10 | ≥99.25 | ≥99.37 | ≥99.50 | ≥99.35 | ≥99.43 | ≥99.43 | ≥99.41 | |

TABLE III

EVAPORATION RATE OF WATER VAPOR AND OVERALL MASS TRANSFER COEFFICIENT AS A FUNCTION OF THE CONCENTRATION OF IMPURITIES

| Impurity | - | NaNO ₃ | | | | NaCl | | Na_2SO_4 | | | |
|--|----------|-------------------|----------|----------|----------|----------|----------|------------|----------|----------|--|
| Content (mol/L) | 0 | 0.2 | 0.4 | 0.6 | 0.2 | 0.4 | 0.6 | 0.2 | 0.4 | 0.6 | |
| Evaporation rate (dm/dt) (kg.h ⁻¹) | 0.0138 | 0.0137 | 0.0129 | 0.0118 | 0.0136 | 0.0124 | 0.0110 | 0.0134 | 0.0122 | 0.0112 | |
| | 8.54E-11 | 8.97E-11 | 8.95E-11 | 8.74E-11 | 8.89E-11 | 8.84E-11 | 8.75E-11 | 8.87E-11 | 8.69E-11 | 8.65E-11 | |
| Mass transfer coefficient | ± | ± | ± | ± | ± | ± | ± | ± | ± | ± | |
| | 1.01E-11 | 6.53E-12 | 1.08E-11 | 8.52E-12 | 8.61E-12 | 1.08E-11 | 1.18E-11 | 1.18E-11 | 1.03E-11 | 1.17E-11 | |

IV. CONCLUSIONS

The experimental results indicate that the presence of Na_2SO_4 affected the morphology of the Na_2CO_3 crystals while $NaNO_3$ and NaCl had no apparent effect on the crystalline products. Furthermore, the impurities have no effect on the XRD patterns of crystals. The main XRD pattern of crystals is $Na_2CO_3\cdot 10H_2O$. In addition, membrane crystallization is proved to be a feasible technology for crystallizing Na_2CO_3 from CO_2 capture by using alkali solution. Obtained crystals demonstrated an acceptable purity and can possibly be reused in the industry.

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