Application Quality Function Deployment (QFD) Tool in Design of Aero Pumps Based on System Engineering

Z. Soleymani, M. Amirzadeh

Abstract—Quality Function Deployment (QFD) was developed in 1960 in Japan and introduced in 1983 in America and Europe. The paper presents a real application of this technique in a way that the method of applying QFD in design and production aero fuel pumps has been considered. While designing a product and in order to apply system engineering process, the first step is identification customer needs then its transition to engineering parameters. Since each change in deign after production process leads to extra human costs and also increase in products quality risk, QFD can make benefits in sale by meeting customer expectations. Since the needs identified as well, the use of QFD tool can lead to increase in communications and less deviation in design and production phases, finally it leads to produce the products with defined technical attributes.

Keywords—Customer voice, engineering parameters, QFD, gear pump.

I. INTRODUCTION

THE goal of the paper is applying OFD tool in aero pump design. Since each product can be defined as a system, so the use of special tools in system engineering process causes that needs would be met. OFD was formed based on total quality control, it means that the control would be applied not only in production lines but also the needs should be considered before design phase. for the first time After World War II the Japanese companies focused on design quality [1], although before that the need to understand the design requirements was sensed but no normal system existed in order to transform customer needs to initial design [2], consequently QFD established as a design correction method for meeting customer needs. Design teams in suitable design of a product need to know what thing to be designed and also expectations of end users. QFD is a systematic method based on exact identification of customer needs and related to functional groups in companies; it means that by applying QFD the customer needs would be translated to design parameters and the details determined in product development.

II. EXPRESS AND DEVELOPMENT OF QFD

A. General

QFD is a tool that customer requirements are identified in design phase, this process done by different methods including: brain storming, compliments search, Warranty logs,

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customer visitation and concentrated groups. Akao was named as father of QFD. He defined "the method for design quality development which helps to customer satisfaction and customer requirements and transition to considered goals in desired design and quality, then it being used in production phases [3].

B. QFD Structure

The first stage of applying QFD is providing House Of Quality. The House is graphic tool in order to define the relationships between customer needs to product. Fig. 1 shows HOO format:

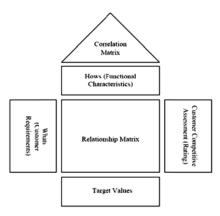


Fig. 1 HOQ Matrix [4]

C. Customer Needs

Firstly customer needs or WHATS are identified that may be stated as general and vague. The Japanese have called this stage "voice of customer"; these needs are expressed in different levels as primary, secondary, tertiary.

D. Engineering Attributes

Then engineering attributes or How's are selected based on customer needs and also should be measurable in a way that customer needs would be satisfied.

E. The Relationship between Customer Needs and Engineering Attributes

After putting Whats and Hows in house of quality, now the relationship between them is set by using symbols shown as:

- Strong relationship
- Medium relationship
- Weak relationship

F. Customer Rating of the Competition

It expresses that how new product competes with other available products; this aspect of product is vital for competition and get new product. Acceptable competitive comparison information would be acquired by engineers and taking note of what customers says at trade shows and retail outlets. The rate which representing the competition for each requirements are given from 0 to 5.

G. Correlation Matrix

The designers in design process have challenges because of no information about the impact of each design parameters on other parameters and how these factors can be effective on customer needs. The relationships among them in QFD's roof guide product designer. In relative and absolute importance part, total of scores is brought at bottom of chart, it states that how much customer needs are met.

H.OFD Advantages

This technique enables organizations to be more competitive in design, have better quality and less cost furthermore it helps to develop new product.

- Decrease engineering's changes

- Decrease set up changes
- Meet customer requirements
- It is proactive instead of reactive

Fig. 2 shows the whole process of QFD, as it is considered that another advantage of which is transition the available knowledge among different stages and be sure of tracing the requirements in a way that all requirements would be met and also final product toward main needs is traceable.

III. APPLICATION QFD

In the paper application QFD for aero pumps has been done according to Fig. 2, since the considered pump is prototype so, 3 and 4 stages have been merged. Pump is a tool which gets the required mechanical energy from external power like electromotor and affects passing fluid consequently; so energy of fluid is increased in pump outlet and it leads to pressure and flow. A pump should make the required flow as continuous and stable besides generate the considered pressure or Head in all stages of pump working. Therefore, a designer should consider these conditions while designing a pump in order to meet all user needs.

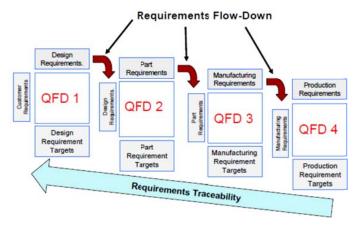


Fig. 2 Overall QFD Transfer Process [5]

Gear pumps combined by two or some gears which one is driver and others are driven, the entered force to pump by driver gear transfers to driven one. The gear of a pump is same as pump's heart; its most important function is transition of fluid. Aero pumps are considered as products with narrow markets so, customers have enough technical knowledge about their requirements. In order to reduce the risk here customer requirements and technical requirements have lots in common. Therefore, it is important to define precisely customer requirements. According to recent researches, customer technical requirements for considered pump as Fig. 5 in phase 1 QFD. The needs are defined as primary one then secondary or even more divisions.

In continuous impact of technical parameters of pump and organizational difficulty are put on chart besides relationship between parameters in chart's roof as Fig. 6. Then in right part of chart, the considered pumps in comparison with

competitors are shown in Fig. 7. In addition, the phase 1, QFD chart is shown in Fig. 8.

To proceed should formed phase 2 and 3 QFD charts. The phase 2, design parameters, and QFD chart are shown in Figs. 9 and 10. In addition, the phase 3, design parameters in manufacturing and QFD chart are shown in Figs. 11 and 12.



Fig. 3 Gear pump operation

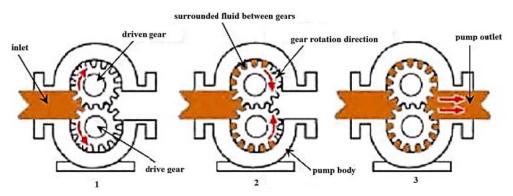


Fig. 4 Fluid transfer on gear pump

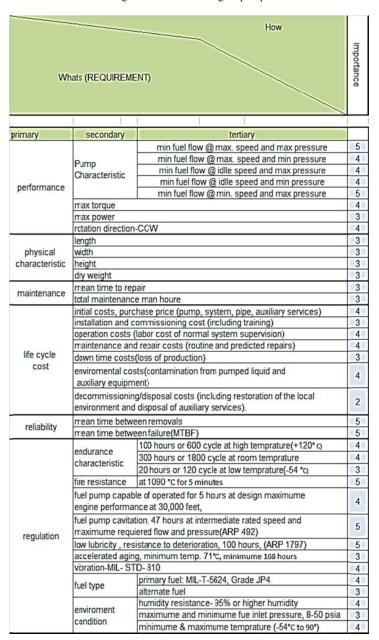


Fig. 5 Customer requirements

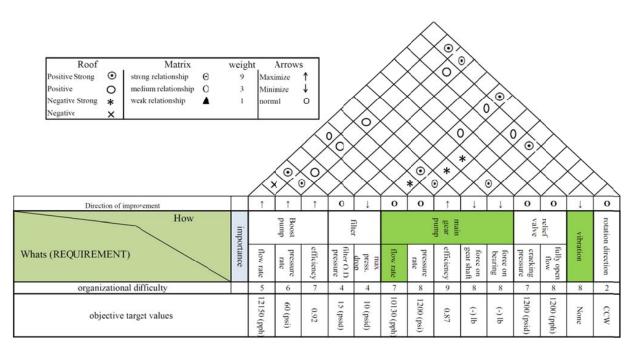


Fig. 6 Quality house's roof

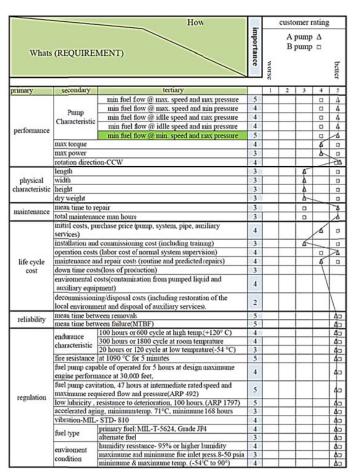


Fig. 7 Technical competitive comparison

		impo		Boost			filter			gear	•		valve	relief	vibi	rotation	
Whats	(REQUIREN	MENT)	importance	flow rate	pressure rate	efficiency	filter O.D. pressure	max press. drop	flow rate	pressure rate	efficiency	force on gear shaft	force on bearing	cracking pressure	fully open flow	vibration	rotation direction
rimary	secondary	tertiary															-
imary	secondary	min fuel flow @ max. speed and max pressure	5	Θ	Θ	0			Θ	Θ	Θ	-		0	Θ		+-
		min fuel flow @ max. speed and min pressure	4	Θ	Θ	0	_		Θ	Θ	Θ	 		0	<u> </u>		+-
	Pump	min fuel flow @ idlle speed and max pressure	4	Θ	Θ	0			Θ	Θ	Θ				_		+-
	Characteristic	min fuel flow @ idlle speed and min pressure	4	Θ	Θ	0			Θ	Θ	Θ			_			_
performance		min fuel flow @ min. speed and max pressure	5	Θ	Θ	0		A	Θ	Θ	Θ			_			_
	max torque		4	A	0	A .				A		Θ	0				
	max power		3	A	0	A			Θ	Θ	0	0					
	rotation direction	on-CCW	4														Θ
	length		3	•				- 1	A	A				1 2			
physical	width		3		7					A.							
haracteristic	height		3	A	1					A							
	dry weight		3		Ť.				A								
	mean time to re	pair	3			A		A			•	A	A				
naintenance	total maintenan	ce man houre	3		1							A	•				
	initial costs, pu services)	rchase price (pump, system, pipe, auxiliary	4	•	О	Θ	0	•	0	О	Θ	•	0	0	0	Θ	4
	installation and	commissioning cost (including training)	3		A	0		A	A	A						A	
	operation costs	(labor cost of normal system supervision)	4	•	A	A				A	0		J.			A .	1
life cycle	maintenance an	d repair costs (routine and predicted repairs)	4		0	0		A	A	A	0	0	0		•	0	
cost	down time cost	s(loss of production)	3			A			8		•						
	enviromental co auxiliary equip	osts(contamination from pumped liquid and ment)	4			0					•					A	
		ng/disposal costs (including restoration of the ent and disposal of auxiliary services).	2									0	0				
reliability	mean time betw	reen removals	5		A	0	0	0			A	0	A	Θ		Θ	
renaomity	mean time betw	veen failure(MTBF)	5		A	0	0	0				0	A	Θ		Θ	
	endurance	100 hours or 600 cycle at high temp.(+120° C)	4	A	0	Θ			Θ	Θ	Θ	A	A	A		0	
	abarantariatia	300 hours or 1800 cycle at room temprature	4	A	A	Θ			Θ	Θ	0	A	A	A	A	0	1
		20 hours or 120 cycle at low temprature(-54 °C)	3	<u> </u>	0	9			Θ	Θ	Θ	A	A	A	A	0	-
		at 1090 °C for 5 minutes	5	A		0	_		A		A	_					+
		ble of operated for 5 hours at design maximume ance at 30,000 feet,	4		0	Θ			0	0							
		ation, 47 hours at intermediate rated speed and				1000	_	-				-		<u> </u>	-5-6.5		+-
regulation		niered flow and pressure(ARP 492)	5	•	•	0	•	A	0	0		0	0		•	0	
low lutricity, resistance to deterioration, 100 hours, (ARP 1797) accelerated aging, minimum temp. 71°C, minimume 168 hours		5	0	A	0			A		Θ	0	0	A		A		
		3	A	-	A			A					A			-	
	vibration-MIL-STD-810		4		A	_	A					Θ		0		0	1
		primary fuel: MIL-T-5624, Grade JP4	4	<u> </u>	A		A	A	A	A	A				A		4—
		alternate fuel	3		A	A .	A	A	A	A	A	-	-		A		+-
		humidity resistance- 95% or higher humidity maximume and minimume fue inlet press.8-50 psia	3	A	0	A .	Θ		0 0 (A)	0	0	-			-		+-
			4			A	Θ	A .	A	0	•		•	A			+-
minimume & maximume temp. (-54°C to 90°) organizational difficulty					6	7	4	4	7	8	9	8	8	7	8	8	2
		5	0	1	4	4	1	0	9	9	0	/:	0	0	1 2		

Fig. 8 Phase 1 of QFD chart

Part Design Parameters			propertice										main pump											propertice	filter			relief valve propertice	
(HOW)	customer targets		tip elearance							propertice	gear					diffre	inlet		bearing		inlet area	pump rpm	filter	spring	elemer	elem	relief valve	sealing s	valve
Design requirement	argets	nce	rance impeller/housing	pitch	width	teeth number	pressure angle	pitch diameter	root diameter	clearance gears(\$)	gear core hardness	gear case hardness	tip clearance gear/body	geometry total runout	tooth profile tolerance	intial pressure	et pressure	bearing O.D.	bearing I.D.	surface roughness	ea	pm	spring siffness	ing seat area	element mesh number	element mesh size	ve spring stiffness	sealing surface roughness	e cross area
design difficulty			8	5	4	1	4	6	6	7	9		8			5	5	6	6	6	3	3	5	5	5	5	5	8	5
parameter values			0.008-0.015 in	(-) 1/in	(-) in	(-)	20 degree	(-)in	(-) in	•	(-) HRC	(-) HRC	(-) in	(-) in	(-) in	(-) psid	(-) psig	(-) in	(-) in	(-) µ.in	(-) squre.in	(-) rpm	(-) lb/in	(-) squre.in	(-)	(-) in	(-) lb/in	(-) µ.in	(-) squre.in

Fig. 9 Design parameters of phase 2

Design requirement	relief valve propertice			filter	propertice							_	_			main pump										impeller	propertice			Part Design Parameters		
Description Secondary Se	sealing s	relief valv	elem	elemen	spri	filter	pump n	inlet ar		bearing propertice		inl	diffre					gear	propertice							ing	tip clearance	importa	customer t	(HOW)		
Boost Pressure rate Co(psi) 4 0 0 0 0 0 0 0 0 0	sealing surface roughness	relief valve spring stiffness	ent mesh size	t mesh number	ng seat area	spring siffness	pm	ca	surface roughness	bearing I.D.	bearing O.D.	et pressure	ntial pressure	tooth profile tolerance	geometry total runout	tip clearance gear/body	gear case hardness	gear core hardness	clearance gears(ξ)	root diameter	pitch diameter	pressure angle	teeth number	width	pitch	seller angle	e impeller/housing	nce	argets	ent	sign requiremen	De
Boost Pressure rate Co(psi) 4 0 0 0 0 0 0 0 0 0				_							_										_	_						_	1	tartings	casandani	neim ne
Boost Pump Pressure rate 60(psi) 4 0 0 0 0 0 0 0 0 0	+				-	_	0	0	\vdash		-	0	\vdash			$\overline{}$	\vdash		_	-	-	-	-	\vdash	-	0	0	5	12150(nob)	ternary	_	primary
Pump efficiency	++		\vdash			_	_	_	-		-	_		_	_	-	\vdash		_	-	-	-	-									Boost
filter O.D. pressure 15(psid) 5	+							-	-		-	Ť					\vdash		_	-	\vdash	-	-	-	-			-				pump
Title max. pressure drop 10(psid) 4	$\overline{}$				Θ	Θ	-	-			-	-					\Box			-	-			-	-	-			7.17.20			
Figure F	\top		Θ	0		_									1															rop		filter
main gear gear generate 1200(psi) 5 O Ø O <	0						Θ					0	0			Θ					0	Θ	Θ	Θ	Θ					-1		
Part	0						Θ				$\overline{}$	0	Θ			0	0	0	0	Θ	0	0	0	Θ	0							main
pump force on gear shaft force on gear shaft force on bearing (-) lb 4 O A O O A O O A O O A O O A O O A O O A O	0						Θ		0		-	Θ	Θ			Θ			Θ			0		0				4				
force on bearing (-) lb 4							A							•	0	0	Θ	Θ	0			0		0		A	0	4	(-) lb	aft	force on gear shaft	pump
valve fully open flow 1200(pph) 5 0									•	Θ	Θ						0											4	(-) lb			
vibration (-)g(ft/s²-2) 5 O O O A O O A O A O A O O O O O A O O A O	ЭΘ	Θ											0				A				\Box							5	1200(psid)	e	cracking pressure	relief
rotation direction CCW 2 Θ																												5	1200(pph)		fully open flow	valve
design difficulty 8 6 5 4 1 4 6 6 7 9 8 5 5 6 6 6 3 3 5 5 5 5							0		A				A	Θ	Θ	A	Θ	Θ	Θ			A	Θ	0		0		5	(-)g(ft/s^2)		on	vibrati
																										Θ		2	CCW	DD-e-121	direction	rotation
(-) H (-) H (-) H (-) Deparameter values	5 8	5	5	5	5	5	3	3	6	6	6	5	5			8		9	7	6	6	4	1	4	5	6	8	100		ifficulty	design diff	
Trecin in i	(-) µ.in	(-) lb/in	(-) in	(-)	(-) squre.in	(-) lb/in	(-) rpm	(-) squre.in	(-) μ.in	(-) in	(-) in	(-) psig	(-) psid	(-) in	(-) in	(-) in	(-) HRC	(-) HRC	©	(-) in	(-)in	20 degree	•	(-) in	(-) 1/in	(-) Degree	0.008-0.015 in			r values	parameter v	

Fig. 10 Phase 2 of QFD chart

Manufacture Design Parameter	Milling	CNC			Gear Manufacture					parameter	Spring		Summer	Tuening
(HOW)	JAXIS	A		Parameters	Hob		case depth	spring mate	residual s		Process Parameter		Cui	Fee
Part Design requirement	Cutting Speed	Feeding Speed	Special class tolerance	axial feeding(in/wrev)	Radial feeding(in)	cutting speed(in/min)	h hardening (μ.in)	spring material type and grade	stress in the spring	clamping stress	clamping temprature	clamping time	Cutting Speed	Feeding Speed
difficulty	8	6	9	7	8	8	9	7	6	8	6	5	6	6
parameter values	NA	NA	μ.in	in/wrev	'n	in/min	μ.in	NA	NA	NA	NA	NA	NA	NA

Fig. 11 Design parameters in manufacturing (phase 3)

IV. ANALYSIS

In QFD table-phase 3, the parameter "special class tolerance" that used in hob machinery, has most important percentage (14.7%).

The manufacture design parameter has impact on part design requirement with equal importance coefficient as:

- Clearance gears (ξ): importance factor=5x9=45
- Tip clearance gear /body: importance factor=5x9=45
- Geometry total run out: importance factor=5x9=45
- Tooth profile tolerance: importance factor=5x9=45

All four part design requirements belong to design

requirements of pump wheel gear since the impact of each mentioned points on customer needs in phase 1 is widespread so, one point with simple analysis is selected for analysis.

Refer to phase 2 of QFD absolute importance of four part design requirements mentioned in previous stage shows that two parameters clearance gear and tip clearance gear /body have most absolute importance equal to 113. These two parameters effect different design requirements that most important of them are brought in Table I, regarding amount of impressionable.

As a result, vibration and main gear pump -flow rate have most effective. Refer to phase 1 QFD amount of effectiveness

of mentioned parameters on customer needs shows that flow rate has absolute importance 399 and vibration has absolute importance 214. Consequently, tip clearance of gear/body has most effectiveness on engineering parameters in phase 1 QFD. Now it is stated the impact of parameter special class tolerance of phase 3 QFD on main gear pump – flow rate of phase 1 QFD and also customer requirements. Before that, a definition of hob tool is expressed.

A. Hob

Hob is a tool that often used for produce gear profile. The production of gear is done with continues index process by rotating piece and hob together with a fixed ratio and at the same time, the hob being driven into pieces [6].

Hob tooth creates progressively and each tooth is in a different position. Hobs are made in 5 different classes. 3 classes have profile grinding and 2 classes do not have profile grinding [7].

Hob that has profile grinding:

- AA: very high accuracy
- A: high accuracy
- B: standard
- Hob that does not have profile grinding:
- C: high accuracy
- D: standard

		Manufacture Design Parameter			Milling	CNC			Gear Manufacture	1				parameter	2		Summ	1
		(HOW)	customer targets	importance	JAMS	5 A C		Machine Parameters	Hob		case depth	spring mate	residual si	I al allicect	Process Parameter		Cut	Fee
	art Design equirement		ırgets	ice	Cutting Speed	Feeding Speed	Special class tolerance	axial feeding(in/wrev)	Radial feeding(in)	cutting speed(in/min)	case depth hardening (µ.in)	spring material type and grade	residual stress in the spring	clamping stress	clamping temprature	clamping time	Cutting Speed	Feeding Speed
			9 8	_														_
primary	secondary	tertiary	0.000.0.015	-									_			_	-	_
impeller		nce impeller/housing	0.008-0.015	5	Θ	Θ										_	_	
propertice	11	mpeller angle	(-) Degree	5	Θ	Θ			_			_		_		_		—
		pitch	(-) 1/in	4					A	<u> </u>								—
		teeth number	(-)	5			•	•	•	0								_
	}	pressure angle	20 degree	_							-							<u> </u>
	1	pitch diameter	(-)in	4		-	0	A	<u> </u>	<u> </u>								_
	gear	root diameter	(-) in	5				0	0	0								_
main	propertice	clearance gears(ξ)	(-)	4			Θ	Θ	0	0	Θ					_	_	—
pump		gear case hardness	(-) lb	5			Θ	0		0	Θ					_	-	-
		tip clearance gear/body	(-) in	5			Θ	Θ	<u> </u>	0						_	-	-
		geometry total runout	(-) in	_	_	_			0		-					_	_	—
L Company		tooth profile tolerance	(-) in	5	\vdash	_	Θ	Θ	Θ	0	-					_		_
	bearing	bearing O.D.	(-) in	3					_		-					_	A	A
	propertice	bearing I.D.	(-) in	5												_	Φ	Θ
121		surface roughness	(-) μ.in	3							\vdash		-			_	Θ	Θ
filter propertice	filte	r spring siffness	(-) lb/in	4								Θ	Θ	Θ	Θ	Θ		
1:-C1	relief va	alve spring stiffness	(-) lb/in	4								Θ	Θ	Θ	Θ	Θ		
relief valve propertice	sealing	surface roughness	(-) μ.in	5													Θ	Θ
propertice		ilve cross area	(-) squre.in	3													A	A
	diffi	culty			8	6	9	7	8	8	9	7	6	8	6	5	6	6
	paramete	er values			NA	NA	μ.in	in/wrev	in	in/min	μ.in	NN	NA	NA	VN	NN	AN	NA
	al	bsolute importance			90	90	200	198	102	91	36	72	72	72	72	72	102	99
		absolute weight			6.6	6.6	14.6	14.5	7.5	6,652	2.6	5.3	5.3	5.3	5.263	5.3	7.5	7.2

Fig. 12 Phase 3 of QFD chart

TABLE I
IMPACT OF GAINED DESIGN PARAMETERS TO ENGINEERING PARAMETERS

-		Tip clearance gear/ body	Clearance gear
Main gear	Flow rate	Importance factor=45	-
pump	efficiency	Importance factor=36	Importance factor=36
vibra	tion	-	Importance factor=45

The selection of Class accuracy depends on the piece that is built by its tolerance. For example, if hob diametric pitch is 3-3.999, hob accuracy as Table II.

TABLE II
HOB ACCURACY FOR DIAMETRIC PITCH 3-3 999 [7]

HOB ACCURACY FOR DIAMETR	IC PITCH	3-3.99	9 [7]	
Hob special class tolerance	AA	A	В	
Hob diameter runout	2	4	6	
Outside diameter runout	5	15	25	
Lead variation tooth to tooth	4	4	6	
Pressure angle or tooth profile	2	3	5	
Tooth thickness(minus only	15	15	15	

Assume that change hob tolerance class makes change outside diameter of gear about " α ", then tip clearance gear/body (radial clearance) is changed about " $\alpha/2$ ".

Pump capacity in equal condition depends on radial clearance between pump body and tooth head and also inclusion fluid film, if it does not fit, leakage of fluid occurs from high pressure zone to low pressure. For gear with common size, the radial clearance range is variable from $0.8 \mu.$ in $0.8 \mu.$ in

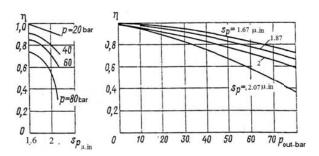


Fig. 13 The impact of radial clearance on gear pump volumetric efficiency [8]

According to Fig. 13, change of tip clearance about " $\alpha/2$ " makes efficiency change about " β ". Because the volumetric efficiency of gear pump is related directly to pump flow rate, so flow rate varies in ratio " β " as per (1).

$$\eta = Q_{ef} / Q_i \to Q_{ef} = \eta \times Q_i \tag{1}$$

 Q_{ef} : Effective flow rate of pump; Q_i : Nominal flow rate of pump; η : Pump efficiency.

As observed in phase 1, QFD table, engineering parameter "main gear pump-flow rate" affects different requirements, by considering the importance of requirement the most effectiveness as:

- Min fuel flow at max. Speed and max. Pressure → importance factor: 5x9=45
- Min fuel flow at min. Speed and max. pressure \rightarrow importance factor: 5x9=45

The point is that what to be noted most is that the gear pump internal leakage sequence of radial clearance can be occurred further at low speed. The internal leakage sequence of radial clearance to total internal leakage is minimal by increase in pump speed. Due to radial clearance, the change in effective flow rate of pump has most effectiveness on requirement "min fuel flow at min. speed and max pressure".

V.CONCLUSION

As shown, QFD model facilitates translation of total and vague requirements into technical measurable requirements. Consequently, the existence of such structure leads to manage complexity in systems so, QFD is a tool for transition customer needs to technical design parameters which increases customer satisfaction and also decreases of problems in initial stage of design phase. QFD in itself does not engineering's problems; it is a forum for gathering and organizing all the data related to a design. The reason of usage QFD in aero industry is its ability to integrate physically besides the integration among customer needs, design requirements, parts characteristics, process key activities, and production requirements. In recent case study which shows the QFD matrix as a powerful tool representing the relationship between customer needs and design parameter's pump. The matrix is for negotiation between requirements in a way that it decreases no certainty in product design. The traditional method of a QFD developed in mentioned research. At first stage customer needs identified so, it compliances between customer need and product's one made. Then in following step by determining technical parameters in order to meet the needs, they were entered into QFD chart. Then the relationship between the parameters set in quality house's roof. According to calculations' results that given in last chart, absolute weights are as Table III.

TABLE III

	A	BSOLUTE WEIGHT	
Turning		Feeding Speed	7.2
Turning		Cutting Speed	7.5
	Hot Set	Clamping Time	5.3
a :	Process	Clamping Temp	5.3
Spring Parameter	Parameter	CLAMPING stress	5.3
rarameter	R	esidual Stress in the Spring	5.3
	Spr	ing Material Type and Grade	5.3
	(case depth hardening(μ.in)	2.6
		Cutting Speed(in/min)	6.7
Gear	Hob	Radial Feeding(in)	7.5
Manufacture	Machine	Axial Feeding(in/wrew)	14.3
	Parameters	Special Class Tolerance Values in	14.7
		μ.in	- 1.7
CNC Milling	5 axis	Feeding Speed	6.6
CNC Milling	Jakis	Cutting Speed(in/min)	6.6

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The calculations for technical parameters represents that the most percentage is related to special class tolerance used in machinery in 14.7; it means that the mentioned parameter has most importance regarding to customer requirements.

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