

# High Aspect Ratio SiO<sub>2</sub> Capillary Based On Silicon Etching and Thermal Oxidation Process for Optical Modulator

N. V. Toan, S. Sangu, T. Saitoh, N. Inomata, T. Ono

**Abstract**—This paper presents the design and fabrication of an optical window for an optical modulator toward image sensing applications. An optical window consists of micrometer-order SiO<sub>2</sub> capillaries (porous solid) that can modulate transmission light intensity by moving the liquid in and out of porous solid. A high optical transmittance of the optical window can be achieved due to refractive index matching when the liquid is penetrated into the porous solid. Otherwise, its light transmittance is lower because of light reflection and scattering by air holes and capillary walls. Silicon capillaries fabricated by deep reactive ion etching (DRIE) process are completely oxidized to form the SiO<sub>2</sub> capillaries. Therefore, high aspect ratio SiO<sub>2</sub> capillaries can be achieved based on silicon capillaries formed by DRIE technique. Large compressive stress of the oxide causes bending of the capillary structure, which is reduced by optimizing the design of device structure. The large stress of the optical window can be released via thin supporting beams. A 7.2 mm x 9.6 mm optical window area toward a fully integrated with the image sensor format is successfully fabricated and its optical transmittance is evaluated with and without inserting liquids (ethanol and matching oil). The achieved modulation range is approximately 20% to 35% with and without liquid penetration in visible region (wavelength range from 450 nm to 650 nm).

**Keywords**—Thermal oxidation process, SiO<sub>2</sub> capillaries, optical window, light transmittance, image sensor, liquid penetration.

## I. INTRODUCTION

ACQUIRING three-dimensional (depth) information by using a camera system has attracted attention in the field of image-sensing applications, such as object identification by in-vehicle camera [1] and machine vision applications [2]-[4]. The light field camera, where microlens array is employed [5], [6], is one of solutions to record such imagery information. The microlens array is located in front of an image sensor and serves as an output image pixel. A disadvantage of the usage of the microlens array is a trade-off relationship between the spatial and angular resolutions. A promising option to replace the microlens array is coded aperture imaging [7], [8], where refractive optical elements, such as lenses, are not used.

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Images from multiple apertures will overlap at the surface of the image sensor and then a computational algorithm is performed to reconstruct the original image. However, its disadvantage is low optical transmittance due to reflection and scattering effects caused by the air holes and inner walls pinholes, which results in a low signal-to-noise ratio. Therefore, devices capable of the integration of the image sensor for the high resolution light field information are still urgent requirements for functional image sensing applications.

For purpose of an optical modulator, porous solid was proposed in [9], where optical modulation can be achieved by moving a liquid in and out of the porous solid. In order to obtain high optical transmittance, SiO<sub>2</sub> is a suitable material as a modulator material. Also SiO<sub>2</sub> is widely used in micro devices because of its superior dielectric properties. SiO<sub>2</sub> films can be formed by a variety of methods including thermal oxidation, low pressure chemical vapor deposition (LPCVD), sputtering, etc. Unfortunately, deposited thick SiO<sub>2</sub> film generally has very high stress that causes cracking or peeling in the film [10], [11]. A low stress SiO<sub>2</sub> film can be deposited by plasma enhanced CVD (PECVD). SiO<sub>2</sub> can be patterned by reactive ion etching (RIE) method [12-13]. However, due to etching anisotropy and low selectivity against a mask material, the aspect ratio of fabricated structures is limited. A trench filling of low stress SiO<sub>2</sub> by using PECVD and sub-atmospheric chemical vapor deposition (SACVD) has been studied in [14]. However, the aspect ratio is not so high and the voids are easily formed during the filling process.

Dry etching technologies of silicon have been studied for many years, and have well developed recently. The etching process of silicon has easily done by deep RIE technique with high aspect ratio structure [12], [15], [16]. Silicon can be oxidized and converted to SiO<sub>2</sub> by employing thermal oxidation process as mentioned in [17], [18]. Nevertheless, formed SiO<sub>2</sub> layers have a high compressive stress due to volume expansion that causes bending or fracturing of device structures.

Basically, a high aspect ratio of SiO<sub>2</sub> capillaries using oxidation process can be achieved from the capillaries structure with thin silicon sidewalls by a combination of electron beam (EB) lithography [16], [19] or nano-imprint [20] techniques and deep RIE. In this research, fabrication process of high aspect ratio SiO<sub>2</sub> capillaries using a combination of deep RIE of Si and thermal oxidation technique is proposed. A repeating process of oxidation and etching is investigated and performed in order to obtain thin

silicon sidewalls of capillaries before final oxidation step. The large compressive stress of the oxide is reduced by optimizing the design of device structure. Moreover, an application of SiO<sub>2</sub> capillaries with and without liquid insertion has been proposed for obtaining high resolution light field information and their optical characteristics are evaluated. A FEM simulation using COMSOL software has been also performed in order to compare with experimental results.

## II. DEVICE STRUCTURE AND WORKING PRINCIPLE

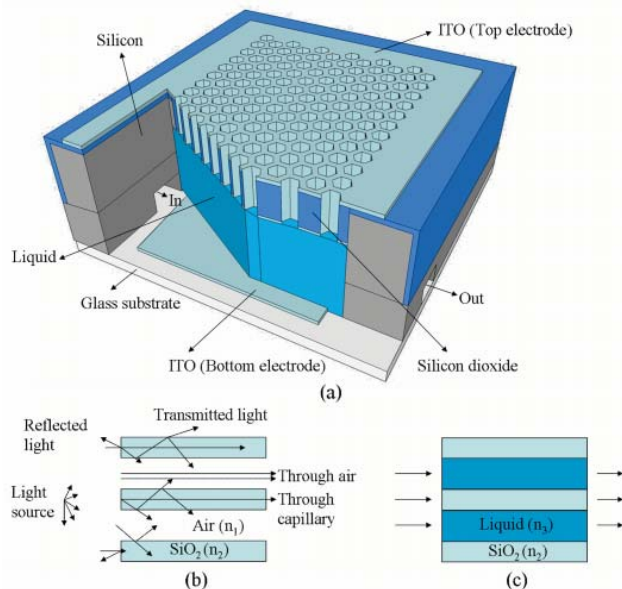


Fig. 1 (a) Device concept, (b) Opaque state, (c) Transparent state

The device concept and working principle are elaborated as shown in Fig. 1. Its structure is basically consisted of micrometer-order SiO<sub>2</sub> capillaries (porous solid), a top indium tin oxide (ITO) electrode, a bottom ITO electrode, liquid and a glass substrate. The device can be directly mounted on an image sensor chip and is expected to have a large optical modulation range for functional image sensing applications.

The operation of this device is based on electro-wetting phenomenon-controlled capillary force [21]-[23]. When a DC voltage is applied to the structure, the liquid moves into the capillaries. Therefore, the porous solid gets transparent due to the refractive index matching. The reflected light inside of the capillaries will be disappeared because of refractive index matching at the interface ( $n_2 = n_3$ ). Thus, a high optical transmittance will be obtained (Fig. 1 (c)). In case without liquid in the capillaries, the light transmittance of the capillary is lower than that with liquid because of the reflected light by air holes and capillary walls (Fig. 1 (b)) and it works ideally as an opaque state. Thus, by shifting the liquid in and out of the porous solid, the light transmittance can be electrically controlled.

## III. FABRICATION PROCESS DESCRIPTION AND EXPERIMENTAL RESULTS

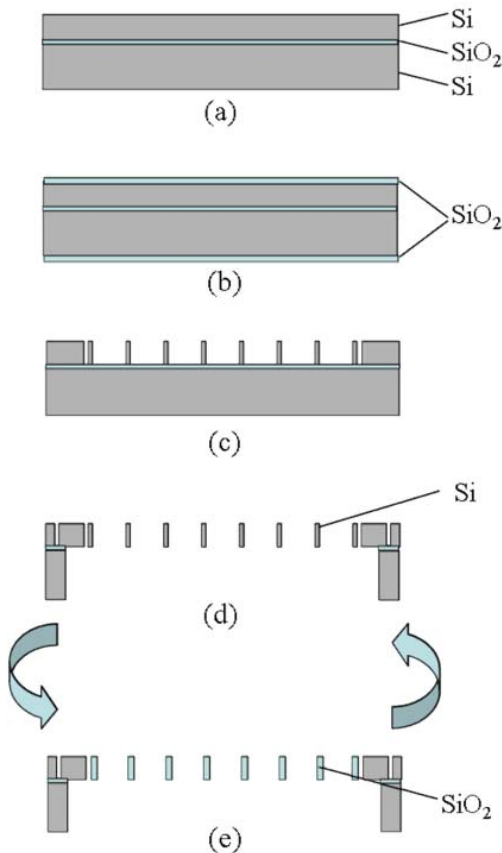


Fig. 2 Fabrication process: (a) SOI wafer (b) Thermal oxidation (c) Photolithography, RIE and deep RIE (d) Backside photolithography, deep RIE and SiO<sub>2</sub> removal (e) Repeating oxidation process

The fabrication process of the capillary plate is illustrated in Fig. 2. The fabrication process begins with a silicon on insulator (SOI) wafer, which consists of a 7  $\mu\text{m}$ -thick top silicon device layer, 1  $\mu\text{m}$ -thick oxide layer and 300  $\mu\text{m}$ -thick silicon handling layer (Fig. 2 (a)). A 400 nm-thick SiO<sub>2</sub> layer is formed on the SOI wafer by wet thermal oxidation as an etching mask of the silicon device layer (Fig. 2 (b)). On this SiO<sub>2</sub> layer, a resist pattern is formed by immersion photolithography. Then, the SiO<sub>2</sub> layer is etched by using reactive ion etching (RIE) using a gas mixture of CHF<sub>3</sub> and Ar with a power of 120 W and a chamber pressure of 5 Pa. The micro-capillary structures are formed by using DRIE by Bosch process using SF<sub>6</sub> and C<sub>4</sub>F<sub>8</sub> for short etching and passivation cycles (etching time 2.5 s, passivation time 2.5 s) for creating low scallops (Fig. 2 (c)). Next, the backside photolithography and deep RIE are performed, and then SiO<sub>2</sub> of the box layer is etched in HF solution for releasing the optical window structures, as the fabrication result of the 7.2 mm x 9.6 mm optical window is shown in Fig. 3 (a). A thin silicon sidewall of around 600 nm and silicon capillaries of around 1.3  $\mu\text{m}$  diameter are achieved as shown in Fig. 3 (b).

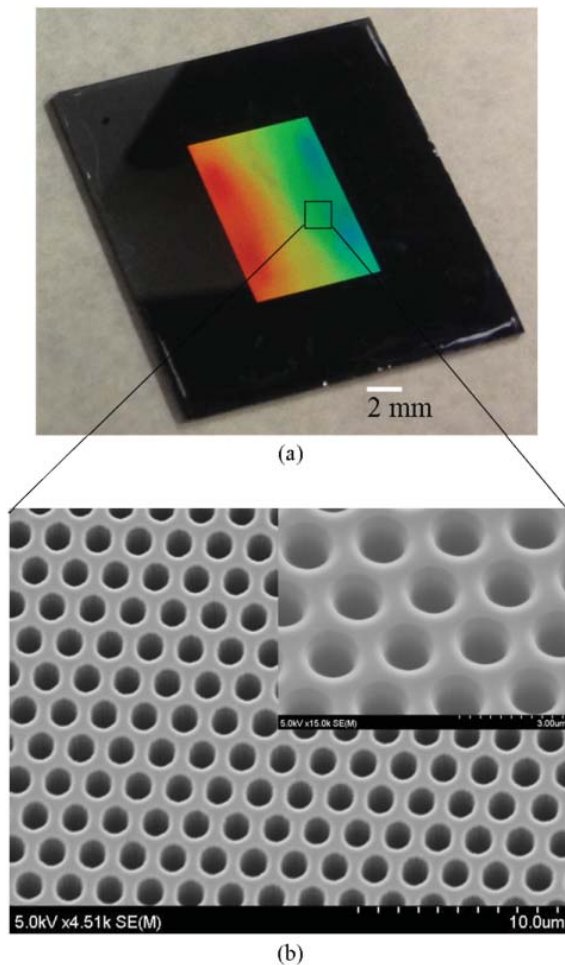


Fig. 3 (a) Silicon optical window (b) Close-up view of silicon capillaries

The silicon capillaries are thermally oxidized to form  $\text{SiO}_2$  capillaries (Fig. 2 (e)). However, approximately 44% of silicon at surface is consumed during the thermal oxidation process [17], [18]. Therefore, the repeating oxidation and etching processes are performed to achieve the thin silicon sidewalls of the capillaries as shown in Fig. 4 (a). The silicon sidewall width and capillary diameter have been reached to 150 nm and 1.75 μm, respectively, after three repeating times of wet thermal oxidation process under conditions of temperature at 1100 °C,  $\text{O}_2$  flow rate of 0.5 l/min and oxidation time of 30 minutes. 600 nm-wide sidewall capillaries are finally obtained after the oxidation process as shown in Fig. 4 (b).

Thus, the silicon capillaries are completely converted into  $\text{SiO}_2$  capillaries with dimensions of 7 μm depth, 600 nm sidewall width, and 1.3 μm capillary diameter. A high aspect ratio of  $\text{SiO}_2$  capillaries with an aspect ratio of approximately 11.5 has been achieved. In order to obtain higher aspect ratio of  $\text{SiO}_2$  capillary sidewalls, the thinner and deeper silicon capillary sidewalls are needed.

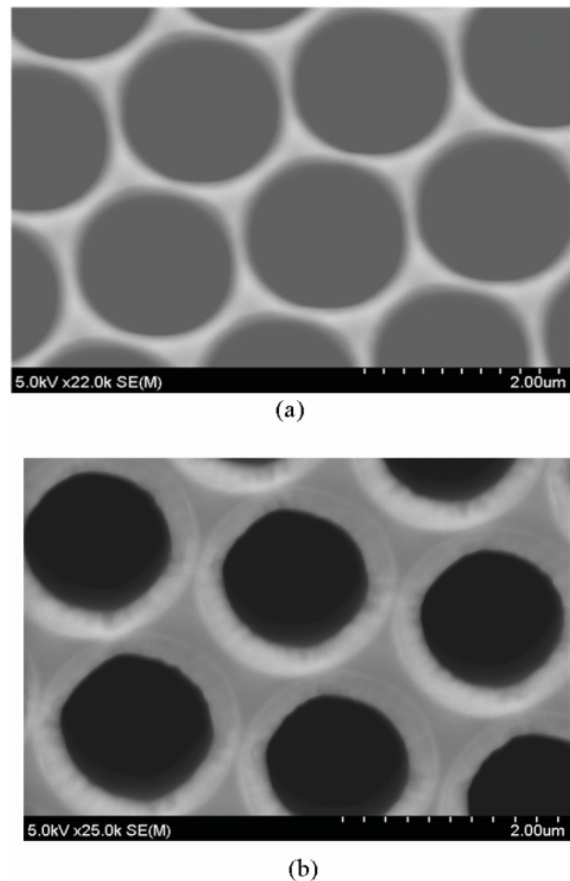


Fig. 4 (a) Silicon capillaries after repeating oxidation process (b)  $\text{SiO}_2$  capillaries after final oxidation process

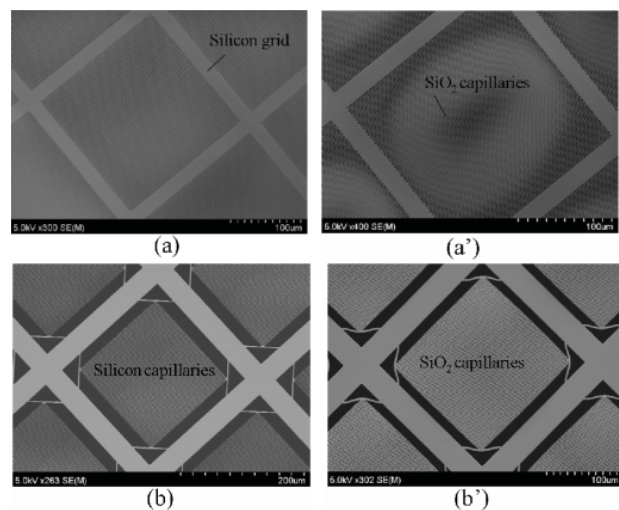


Fig. 5 SEM images of the optical windows (a) Before oxidation process of design #1 (a') After oxidation process of design #1 (b) Before oxidation process of design #2 (b') After oxidation process of design #2

Single crystalline silicon has no stress; therefore, no deformation is observed in the fabricated silicon optical



windows as shown in design #1 (Figs. 5 (a)) and design #2 (Figs. 5 (b)). When the silicon capillaries are turned into SiO<sub>2</sub> capillaries by using oxidation process, a large deformation is observed as shown in Figs. 5 (a'). This reason is due to compressive stress caused by the volume expansion of the structure during the oxidation process. In the design #1, the SiO<sub>2</sub> capillaries are supported by rigid silicon grid. The stress along horizontal direction cannot be released due to the silicon grid, as shown in Fig. 5 (a'). Therefore, the deformation is observed in the center of the optical window with approximately 10  $\mu\text{m}$  of displacement in this design. In order to release the stress of the optical window structure, four thin beams at the corners with width of 1.5  $\mu\text{m}$  in the design #2 are employed, as shown in Figs. 5 (b) and (b'). The optical window does not bend after final oxidation step and the four thin supporting beams are bent by around 3  $\mu\text{m}$ . It means that the stress into in-plane direction is reduced.

A FEM simulation of the relationship between displacement and stress is investigated, as shown in Fig. 6. The simulating parameters of design #1 and supporting beam of design #2 present in Table I. In the design #1, the highest deformation is located in the center of optical window (Fig. 6 (a)) and the stress is at center of the window edge (Fig. 6 (a')). When the optical window gets 10  $\mu\text{m}$  of displacement, it generates a high stress of 1900 MPa. A supporting beam is simulated only in the design #2. The correlative deformation of 3  $\mu\text{m}$  displacement (Fig. 6 (b)) of the beam structure has a high stress of 1870 MPa (Fig. 6 (b')). Thus, the high stress of the optical window (design #1) can be almost released via the thin supporting beams.

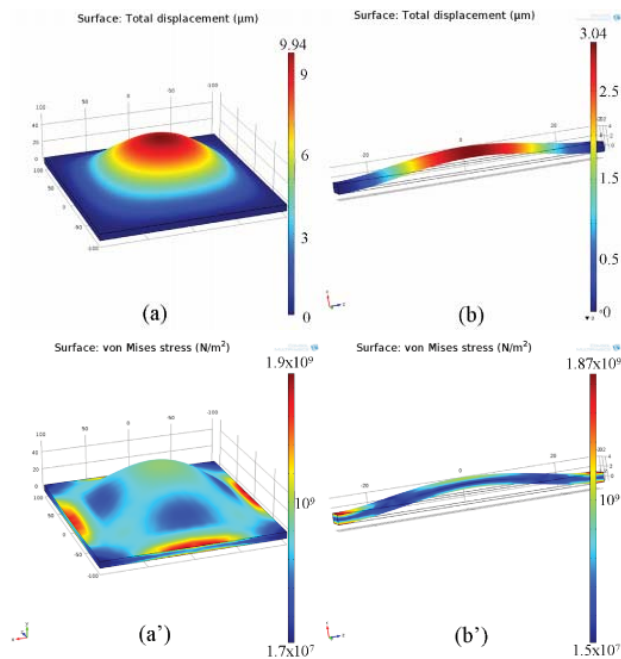


Fig. 6 FEM simulation (a) Displacement of design #1 (a') Stress of design #1 (b) Displacement of supporting beam of design #2 (b') Stress of supporting beam of design #2

TABLE I  
A RELATIONSHIP BETWEEN DISPLACEMENT AND STRESS OF DESIGN #1 AND SUPPORTING BEAM OF DESIGN #2

	Design #1	Supporting beam of design #2
Dimensions		
. Width ( $\mu\text{m}$ )	200	1.5
. Length ( $\mu\text{m}$ )	200	45
. Thickness ( $\mu\text{m}$ )	7	7
Total displacement ( $\mu\text{m}$ )	10	3
Stress (MPa)	1900	1870

#### IV. MEASUREMENT SETUP

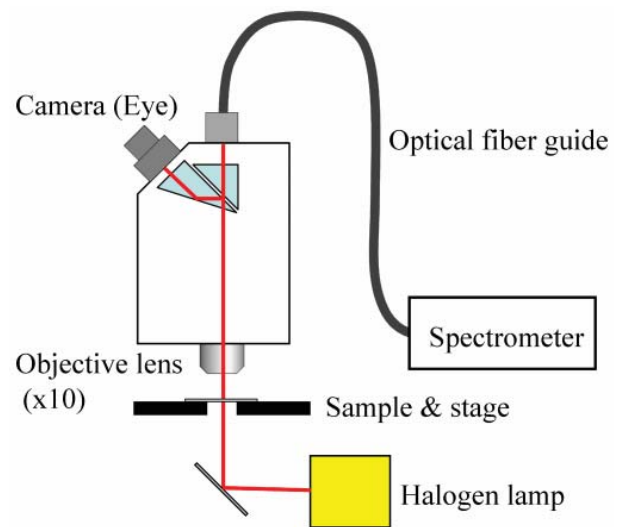


Fig. 7 Measurement setup

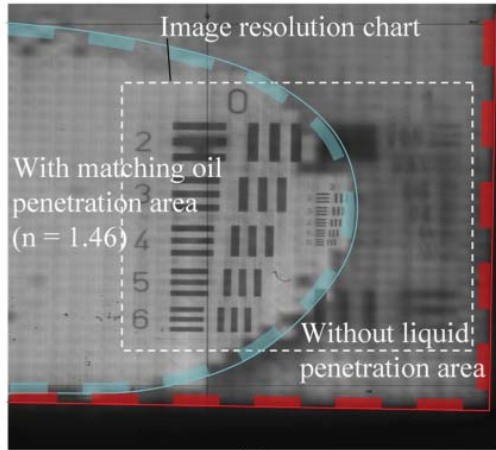
The optical measurement setup, sketched in Fig. 7, is used to evaluate the optical window characteristics. As shown in this figure, an optical microscope equipped with a spectrometer is employed for spectrum measurement in visible range and a halogen lamp is used for illumination via an aperture with a diameter of 10 mm. The distance between the source and the surface sample is around 300 mm.

#### V. MEASUREMENT RESULTS

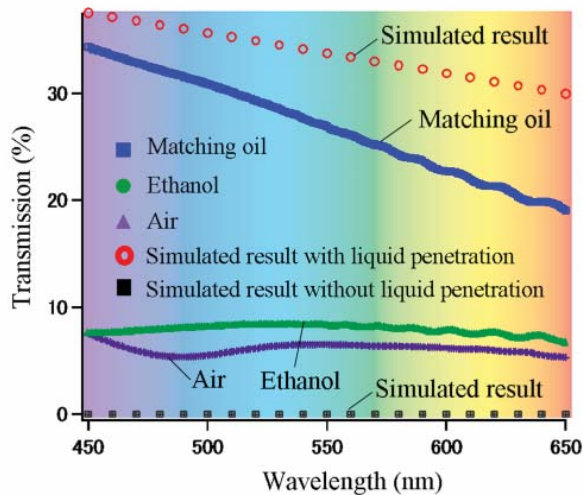
A liquid (ethanol or matching oil) is inserted into the capillaries by just putting the liquid droplet on the device partly. A qualitative comparison of transmittances of the optical window structure, supported by four thin beams at corner, with and without liquid penetration is shown in Fig. 8 (a). Area of matching oil penetration becomes obviously clear than that without matching oil penetration through the captured image of Fig. 8 (a).

A quantitative comparison of transmittances with and without liquid penetration is shown in Fig. 8 (b) and Table II. A low transmittance of the optical window has been observed when it is measured in air environment without liquid penetration. The low transmission light in this case is due to the reflected light on the SiO<sub>2</sub> surfaces of the capillaries as explained before. Around 3% higher light transmission has been obtained with ethanol penetration (refractive index of ethanol: 1.36) than that with air environment (refractive index

of ethanol: 1). A higher transmitting light of around 20% to 35% can be achieved by using matching oil (refractive index of matching oil: 1.46) in a visible region from 450 nm to 650 nm. The possible reason is due to the refractive index matching with SiO<sub>2</sub> capillaries (refractive index of SiO<sub>2</sub>: 1.45 to 1.49). Furthermore, a FEM simulation using COSOL software based on electromagnetic wave propagating has been performed, which is coincident with the measurement results.



(a)



(b)

Fig. 8 (a) Optical image of test pattern via the optical window with and without liquid penetration areas (b) Evaluation of optical properties with and without inserting liquid

Silicon grids, existed in the current design (Fig. 5) may be absorbed light source; therefore, the light transmittance in case of liquid penetration is not so high (around 30%). A evaluation of the optical window which consists only of silicon grid (without SiO<sub>2</sub> capillary structure) show 36 % transmission (Table II). It means 64% of light transmission is reflected and absorbed by these silicon grid structures. It is necessary to remove them for higher optical modulation range in the further investigation. A FEM simulation indicates that 88% light transmittance can be obtained for the case without the silicon

grid (Table II).

## VI. CONCLUSIONS

In this paper, we have designed and fabricated optical windows consisted of micrometer-order SiO<sub>2</sub> capillaries for application of optical modulators. Additional evaluation of its optical characteristic has been also performed. A high aspect ratio of SiO<sub>2</sub> capillaries of around 11.5 has been achieved by employing thermal oxidation process. A very high compressive stress of oxidation process due to volume expansion is reduced by optimizing the design model. The high stress of optical window can be released via thin supporting beams. Its optical transmittance is evaluated under the conditions with and without liquid penetrations. The modulation range is approximately 20% to 35% for cases with and without matching oil in a wavelength range of visible region.

TABLE II  
MEASUREMENT AND SIMULATION RESULTS AT WAVELENGTH OF 500 NM

State of optical windows	Transmission (%)
Air	5%
Ethanol	8%
Matching oil	31%
Simulated result without liquid penetration	0%
Simulated result with liquid penetration	35%
Optical window without capillaries	36 %
Simulated result with liquid penetration and without silicon grids	88%

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