

# Reconfiguration of Deregulated Distribution Network for Minimizing Energy Supply Cost by using Multi-Objective BGA

H. Kazemi Karegar, S. Jalilzadeh, V. Nabaei, A. Shabani

**Abstract**—In this paper, the problem of finding the optimal topological configuration of a deregulated distribution network is considered. The new features of this paper are proposing a multi-objective function and its application on deregulated distribution networks for finding the optimal configuration. The multi-objective function will be defined for minimizing total Energy Supply Costs (ESC) and energy losses subject to load flow constraints. The optimal configuration will be obtained by using Binary Genetic Algorithm (BGA). The proposed method has been tested to analyze a sample and a practical distribution networks.

**Keywords**—Binary Genetic Algorithm, Deregulated Distribution Network, Minimizing Cost, Reconfiguration.

## I. INTRODUCTION

NOWADAYS, distribution networks are rapidly growing, therefore an efficient operation method is essential for reducing costs and increasing effective operation. This can be achieved by networks reconfiguration [1]. Several approaches are used to find the optimal configuration with the following subjects:

- Reducing power system losses by using ant-colony and genetic algorithm [2, 3, 4]
- Improving service restoring for the isolated portion of a distribution system [5, 6]
- Enhancing system reliability by introducing an analytical mathematical model [7]
- Improving load factors to facilitate load aggregation in distribution networks [8]
- Improving load balancing by using customer information in a customer information system (CIS) [9]
- Minimizing energy losses by using the genetic algorithm [10, 11]
- Minimizing energy losses by using a heuristic algorithm [12, 13, 14]
- Finding non-inferior solution by using the simulated annealing method [15, 16, 17]

All of the above researches have been done on traditional distribution power systems, but in many countries traditional distribution networks are transforming to deregulated

networks. The main difference between them networks is the existence of many energy vendors with various conditions for selling energy in a competitive price. In this new environment, consumers and Distribution Companies (Disco) have authority to select an energy vendor whose energy price has more interest. As a consequence, the topology of the network changes according to the Discos' decision. On the other hand, energy losses are also important for energy vendors. Therefore, the new challenge is finding the optimal network reconfiguration with considering minimum energy losses and minimum energy supply cost.

This paper focuses on large-scale power distribution systems in a deregulated environment while the other previous researches have been done on traditional and small distribution networks. For this purpose, a multi-objective function in a deregulated environment is considered for finding the optimal configuration. The objective function of the optimization problem is to minimize the cost of power losses including consumer's load cost. The BGA is also used to solve this optimization problem. By altering the open/closed states of switches the configuration of the networks will change. Therefore, the distribution network reconfiguration problem has a discrete or binary nature. A comprehensive computer program in MATLAB has been written to find the optimal configurations of 16-bus & 83-bus deregulated test systems subject to load flow constraints including permissible voltage and current variations.

This paper is organized as follows. In section 2, a review of some basic power market models are presented. In section 3, the proposed objective functions are explained. In section 4, the BGA and algorithm for obtaining the optimal solution is described. In section 5, the numerical results of the test systems are discussed and finally, conclusions are presented in section 6.

## II. POWER MARKET MODELS REVIEWING

There are three main power market models:

- Poolco Model
- Bilateral Contracts Model
- Hybrid Model

The Poolco model is defined as a centralized marketplace that clears market for buyers and sellers. Electric power sellers/buyers submit bids to the pool for the amounts of power that they are willing to trade in the market. Sellers in a

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power market would compete for the right to supply energy to the grid, and not for specific customers.

The bilateral contracts are negotiable agreements on delivery and receipt of power between two traders. These contracts set the terms and conditions of agreements independent of the ISO. However, in this model the ISO would verify that a sufficient transmission capacity exists to complete the transactions and maintain the transmission security.

The hybrid model combines various features of the previous two models. In the hybrid model, the utilization of a Poolco is not obligatory, and any customer would be allowed to negotiate a power supply agreement directly with suppliers or choose to accept power at the spot market price. In this model, Poolco would serve all participants (buyers and sellers) who choose not to sign bilateral contracts. However, allowing customers to negotiate power purchase arrangements with suppliers would offer a true customer choice and an impetus for the creation of a wide variety of services and pricing options to best meet individual customer needs. In our discussion of market structure, we assume the use of a hybrid model [18].

### III. PROBLEM STATEMENT

In traditional distribution networks, loss minimization is the primary object of optimal operation. However, besides energy loss minimization, the cost minimization is also suggested as a new objective function in deregulated distribution networks.

The problem can be stated as shown in Fig. 1.

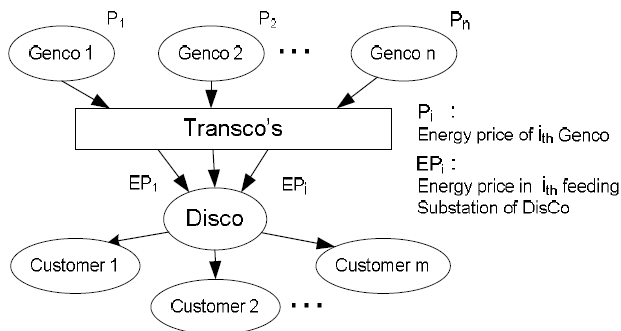


Fig. 1 Disco and other market entities in power system

Disco buys energy from generator companies (Genco's) and transmits it via several transmitter companies (Transco's) to customers. Disco makes some contracts with Genco's and Transco's for buying and transmitting the energy. A Disco should determine the power quantity that each substation delivers to the network during a specific time interval in order to minimize the total energy supply cost with maintaining the service quality considerations. If the network losses are not considered, the solution of the stated problem will be simple, each substation should be utilized in a sequence according to the energy cost, the first one is the cheapest one. Nevertheless, power losses must be taken into account, therefore a special procedure should be developed to obtain a solution, which minimizes the total energy buying cost.

In this paper, it is considered that Disco provides energy according to the bilateral contracts. The total energy supply cost to the consumers during the time interval  $T$  is *Fitness1*:

$$Fitness1 = \sum_{i=1}^n EP_i \left\{ \sum_{k=1}^m \int_0^T P_k(t) dt \right\} \quad (1)$$

Equation (1) can be written as expression (2) when the average power  $P_k$  was considered instead of instantaneous power  $P_k(t)$ .

$$Fitness1 = \sum_{i=1}^n EP_i \left( \sum_{k=1}^m P_k \right) T \quad (2)$$

On the other hand, if the losses at each feeder  $P_{lk}$  are known, then the second objective function *Fitness2* can be expressed as:

$$Fitness2 = \left( \sum_{k=1}^m P_{lk} \right) T \quad (3)$$

As a result, the optimal problem can be formulated as follows:

*Objective functions*

*Minimize:*

$$Fitness1 = \sum_{i=1}^n EP_i \left( \sum_{k=1}^m P_k \right) T \quad (4)$$

$$Fitness2 = \left( \sum_{k=1}^m P_{lk} \right) T \quad (5)$$

*Subject to:*

$$V_{min} \leq |V_k| \leq V_{max} \quad (6)$$

$$|I_k| \leq I_{max} \quad (7)$$

$$P_k \neq 0 \quad (8)$$

Expressions (6) to (8), explain the load and operation constraints. According to the expression (6) and (7), voltages and currents of consumers must be in allowable variations. Expression (8) declares that no feeder section can be left out service.

### IV. SOLUTION METHOD

#### A. String Definition

The open/closed switches change the configuration of a distribution network, hence the states of the switches can be described by a binary string and each state is considered as a gene (binary bits).

|       |        |       |        |     |       |        |
|-------|--------|-------|--------|-----|-------|--------|
| State | Switch | State | Switch | ... | State | Switch |
| 1     |        | 2     |        |     | n     |        |

Each bit accepts only zero or one implying that the corresponding switch is open or close, respectively. For example, the following string describes the situation of

switches in a given distribution network with 16 switches, where the switches 3, 5 and 10 are open.

$String = [1\ 1\ 0\ 1\ 0\ 1\ 1\ 1\ 1\ 0\ 1\ 1\ 1\ 1\ 1\ 1]$

#### B. Adaptive Mutation

The mutation is usually constant throughout the whole GA search process. However, it has been reported that in the practical application of distribution network reconfigurations, an adaptive mutation process is preferable [19]. Consequently, in this paper an adaptive mutation according follows expression has been used.

$$p(k+1) = \begin{cases} p(k) - p_{step} & \text{Fitness1}(k) \& \text{Fitness2}(k) \text{ unchanged} \\ p(k) & \text{Fitness1}(k) \& \text{Fitness2}(k) \text{ decreased} \\ p_{final} & p(k) - p_{step} < p_{final} \end{cases}$$

(9)

$$p(0) = p_{initial} = 1.0$$

$$p_{step} = 0.001$$

$$p_{final} = 0.05$$

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#### C. Proposed Method Flowchart

A flowchart describing the main computational process is shown in Fig. 2.

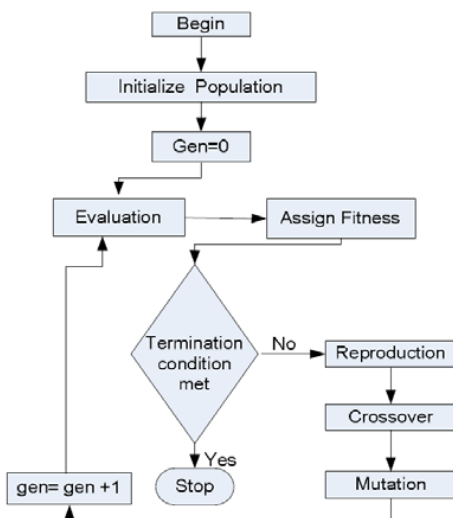


Fig. 2 The flowchart of the proposed method

In this paper, the back/forward sweep distribution power flow is used [20].

## V. NUMERICAL RESULTS

To verify the application of the proposed method, two distribution networks are selected. A network with 16-bus is used as case study 1 and the Taiwan distribution network with 83-bus is used as case study 2.

#### A. Case Study 1

A three-feeder distribution network with 16 buses, 13 sectionalizing switches and 3 tie switches as shown in Fig 3 is selected as case study 1. The tie switches are: S15, S21, S26 and the system load is assumed to be constant with  $S_{base}=100$  MW. It is also assumed that a distribution company (Disco) operates this network and supplies the demand power via three feeders 1, 2 and 3. The energy purchase price in the feeding substations 1, 2 and 3 are 11.4 \$/MWh, 11.6 \$/MWh and 11.2 \$/MWh, consecutively. The other data of the distribution network is shown in Table I.

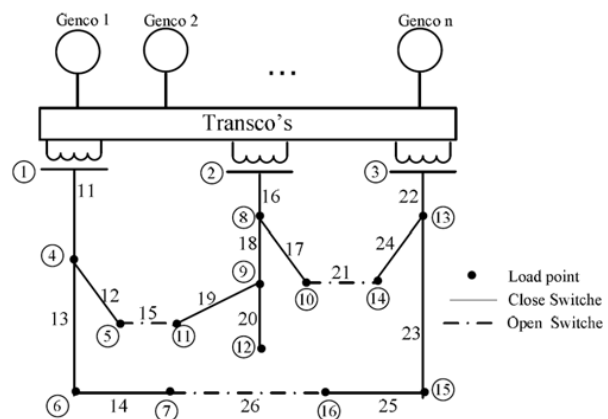


Fig. 3 Three-feeder distribution networks

The parameters of the proposed method for BGA algorithm is also shown in Table II.

If the objective function would be the power loss minimization in a conventional distribution system, then the optimal configuration happened when switches 17, 19 and 26 are opened. In this case, the power loss reduces to 0.00466 P.U. and the total energy supply cost is 8016.62 \$. However, the objective function of the deregulated networks is to minimize the total energy supply cost and power loss minimization. In this case, the total energy supply cost reduces from 8016.62 \$ to 8012.78 \$ when switches 13, 17 and 19 are opened, on the other hand the power loss minimization increases from 0.00466 to 0.00479 P.U. where shown in bold type in Table III. These two cases are shown in Table III as C1 and C2 for traditional and deregulated distribution networks.

Under optimal configuration in the deregulated distribution network, the power loss, feeder-load, energy price and energy supply cost of each feeder are shown in Table IV. As the proof of the proposed method, 190 possible configurations are obtained and the fitness values of the functions *Fitness1* and *Fitness2* are shown in Fig. 4 and Fig. 5, respectively. These figures also indicate the proposed method find the optimum configuration.

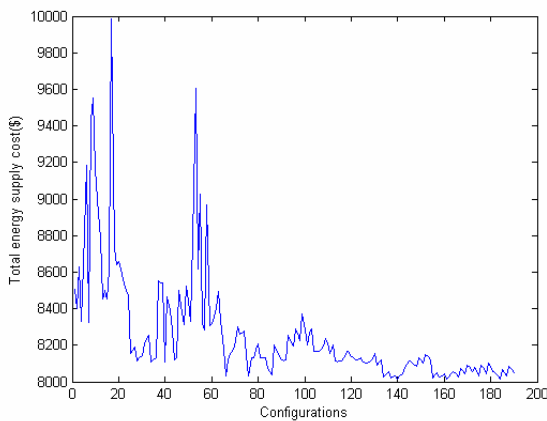


Fig. 4 Total energy supply cost minimization fitness

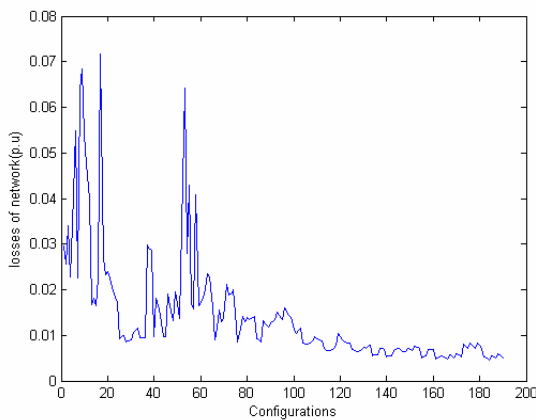


Fig. 5 Loss minimization fitness function

### B. Case Study 2

The second example is a practical distribution network of Taiwan Power Company. It is a three-phase, 11.4 kV system with 11 feeders, 83 normally closed sectionalizing switches, and 13 normally open tie switches which is shown in Fig. 6. Three-phase balance and constant load are assumed. It is also considered that a distribution company (Disco) operates this network and supplies the demand power in its feeding substation via 11 feeders A,B,C,D,E,F,G,H,I,J,K. The other information of the network is shown in Table V.

For this case, the parameters of the proposed method are shown in Table VI. The optimal solution obtained after 690 iterations. For the optimal configuration the share of the each feeder is shown in Table VII. In addition the comparison between the deregulated and conventional distribution network is also explained in Table VIII. Table VIII shows that the total energy supply cost will be reduced to 7723.7 US\$ whereas the power losses will be increased to 0.48464 P.U. in compare with conventional distribution power system

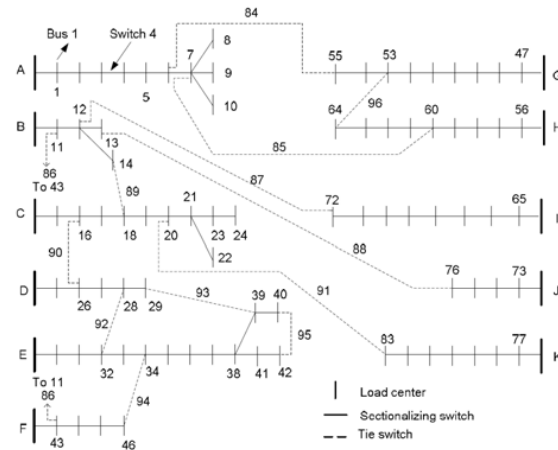


Fig. 6 A distribution system of Taiwan Power Company

## VI. CONCLUSIONS

In this paper, a new multi-objective function for reducing the total energy supply cost and power losses for deregulated distribution network proposed. The method was applied on a sample and a practical distribution network. The obtained results show that the proposed method could investigate the optimal configuration among various possible configurations and reduced the total energy supply cost with adaptive mutation.

## VII. MATHEMATICAL SYMBOLS

|               |   |
|---------------|---|
| $i$           | Number of substation feeders            |
| $k$           | Number of loads at feeder $i$           |
| $EP_i$        | Energy price at substation $i$ (\$/MWh) |
| $P_{lk}$      | Losses at each feeder                   |
| $P_k(t)$      | Instantaneous power of consumer $k$     |
| $P_k$         | Average power of consumer $k$           |
| $P_{initial}$ | Initial mutation                        |
| $P_{final}$   | Final mutation                          |
| $P_{step}$    | Step of mutation variation              |
| $p(k)$        | Adaptive mutation                       |
| $V_{min}$     | Minimum voltage                         |
| $V_{max}$     | Maximum voltage                         |
| $I_k$         | Consumer current                        |
| $I_{max}$     | Maximum current                         |

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TABLE I  
DATA OF THE THREE-FEEDER DISTRIBUTION SYSTEM

| Bus to Bus | Section<br>Resistance (P.U.) | Section<br>Reactance (P.U.) | End Bus<br>Load<br>(MW) | End Bus<br>Load<br>(MVAR) | End Bus Fixed Capacitor<br>(MVAR) |
|------------|------------------------------|-----------------------------|-------------------------|---------------------------|-----------------------------------|
| 1-4        | 0.075                        | 0.1                         | 2.0                     | 1.6                       | 0.0                               |
| 4-5        | 0.08                         | 0.11                        | 3.0                     | 1.5                       | 1.1                               |
| 4-6        | 0.09                         | 0.18                        | 2.0                     | 0.8                       | 1.2                               |
| 6-7        | 0.04                         | 0.04                        | 1.5                     | 1.2                       | 0.0                               |
| 2-8        | 0.11                         | 0.11                        | 4.0                     | 2.7                       | 0.0                               |
| 8-9        | 0.08                         | 0.11                        | 5.0                     | 3.0                       | 1.2                               |
| 8-10       | 0.11                         | 0.11                        | 1.0                     | 0.9                       | 0.0                               |
| 9-11       | 0.11                         | 0.11                        | 0.6                     | 0.1                       | 0.6                               |
| 9-12       | 0.08                         | 0.11                        | 4.5                     | 2.0                       | 3.7                               |
| 3-13       | 0.11                         | 0.11                        | 1.0                     | 0.9                       | 0.0                               |
| 13-14      | 0.09                         | 0.12                        | 1.0                     | 0.7                       | 1.8                               |
| 13-15      | 0.11                         | 0.11                        | 1.0                     | 0.9                       | 0.0                               |
| 15-16      | 0.04                         | 0.04                        | 2.1                     | 1.0                       | 1.8                               |
| 5-11       | 0.04                         | 0.04                        | 0                       | 0                         | 0                                 |
| 10-14      | 0.04                         | 0.04                        | 0                       | 0                         | 0                                 |
| 7-16       | 0.12                         | 0.12                        | 0                       | 0                         | 0                                 |

TABLE II  
THE OTHER PARAMETERS OF THE PROPOSED METHOD

| CASE                       | CASE STUDY I |
|----------------------------|--------------|
| LENGTH OF CHROMOSOME       | 16           |
| POPULATION SIZE            | 10           |
| CROSSOVER PROBABILITY (PM) | 0.7          |
| MUTATION PROBABILITY (PC)  | ADAPTIVE     |
| NUMBER OF ITERATION        | 70           |

TABLE III  
COMPARATIVE NUMERICAL RESULTS OF EXAMPLE I

| CASE | OPEN SWITCHES | VOLTAGE OF BUSES<br>V <sub>MIN</sub> | BUS | POWER LOSS<br>(P.U) | TOTAL ENERGY SUPPLY COST (\$) |
|------|---------------|--------------------------------------|-----|---------------------|-------------------------------|
| C1   | 17,19,26      | 0.972                                | 12  | 0.00466             | 8016.62                       |
| C2   | 13,17,19      | 0.972                                | 12  | 0.00479             | 8012.78                       |

TABLE IV  
DETAILS OF ENERGY SUPPLY COST CALCULATION FOR BEST CONFIGURATION (C3) OF EXAMPLE I

| NUMBER OF FEEDERS  | 1       | 2       | 3       |
|--|---------|---------|---------|
| LOSS OF FEEDER (MW)  | 0.05968 | 0.31708 | 0.10252 |
| LOADS OF FEEDER (MW)   | 7.6     | 13.5    | 7.6     |
| ENERGY PRICE IN FEEDER (\$/MWH)  | 11.4    | 11.6    | 11.2    |
| ENERGY SUPPLY COST IN FEEDER (\$)  | 2095.68 | 3846.67 | 2070.43 |
| SYSTEM TOTAL ENERGY SUPPLY COST (\$) = 2095.68 + 3846.67 + 2070.43 = 8012.78 |         |         |         |

TABLE V  
DATA OF TAIWAN POWER COMPANY

| BUS TO<br>BUS | SECTION<br>R ( ) | SECTION<br>X ( ) | END BUS<br>LOAD<br>(KW) | END<br>BUS<br>LOAD<br>(KVAR) | BUS TO<br>BUS | SECTION<br>R ( ) | SECTION<br>X ( ) | END BUS<br>LOAD<br>(KW) | END BUS<br>LOAD<br>(KVAR) |
|---------------|------------------|------------------|-------------------------|------------------------------|---------------|------------------|------------------|-------------------------|---------------------------|
| A-1           | 0.1944           | 0.6624           | 0                       | 0                            | G-47          | 0.2430           | 0.8280           | 0                       | 0                         |
| 1-2           | 0.2096           | 0.4304           | 100                     | 50                           | 47-48         | 0.0655           | 0.1345           | 0                       | 0                         |
| 2-3           | 0.2358           | 0.4842           | 300                     | 200                          | 48-49         | 0.0655           | 0.1345           | 0                       | 0                         |
| 3-4           | 0.0917           | 0.1883           | 350                     | 250                          | 49-50         | 0.0393           | 0.0807           | 200                     | 160                       |
| 4-5           | 0.2096           | 0.4304           | 220                     | 100                          | 50-51         | 0.0786           | 0.1614           | 800                     | 600                       |
| 5-6           | 0.0393           | 0.0807           | 1100                    | 800                          | 51-52         | 0.0393           | 0.0807           | 500                     | 300                       |
| 6-7           | 0.0405           | 0.1380           | 400                     | 320                          | 52-53         | 0.0786           | 0.1614           | 500                     | 350                       |
| 7-8           | 0.1048           | 0.2152           | 300                     | 200                          | 53-54         | 0.0524           | 0.1076           | 500                     | 300                       |
| 7-9           | 0.2358           | 0.4842           | 300                     | 230                          | 54-55         | 0.1310           | 0.2690           | 200                     | 80                        |
| 7-10          | 0.1048           | 0.2152           | 300                     | 260                          | H-56          | 0.2268           | 0.7728           | 0                       | 0                         |
| B-11          | 0.0786           | 0.1614           | 0                       | 0                            | 56-57         | 0.5371           | 1.1029           | 30                      | 20                        |
| 11-12         | 0.3406           | 0.6944           | 1200                    | 800                          | 57-58         | 0.0524           | 0.1076           | 600                     | 420                       |
| 12-13         | 0.0262           | 0.0538           | 800                     | 600                          | 58-59         | 0.0405           | 0.1380           | 0                       | 0                         |
| 12-14         | 0.0786           | 0.1614           | 700                     | 500                          | 59-60         | 0.0393           | 0.0807           | 20                      | 10                        |
| C-15          | 0.1134           | 0.3864           | 0                       | 0                            | 60-61         | 0.0262           | 0.0538           | 20                      | 10                        |
| 15-16         | 0.0524           | 0.1076           | 300                     | 150                          | 61-62         | 0.1048           | 0.2152           | 200                     | 130                       |
| 16-17         | 0.0524           | 0.1076           | 500                     | 350                          | 62-63         | 0.2358           | 0.4842           | 300                     | 240                       |
| 17-18         | 0.1572           | 0.3228           | 700                     | 400                          | 63-64         | 0.0243           | 0.0828           | 300                     | 200                       |
| 18-19         | 0.0393           | 0.0807           | 1200                    | 1000                         | I-65          | 0.0486           | 0.1656           | 0                       | 0                         |
| 19-20         | 0.1703           | 0.3497           | 300                     | 300                          | 65-66         | 0.1703           | 0.3497           | 50                      | 30                        |
| 20-21         | 0.2358           | 0.4842           | 400                     | 350                          | 66-67         | 0.1213           | 0.4140           | 0                       | 0                         |
| 21-22         | 0.1572           | 0.3228           | 50                      | 20                           | 67-68         | 0.2187           | 0.7452           | 400                     | 360                       |
| 21-23         | 0.1965           | 0.4035           | 50                      | 20                           | 68-69         | 0.0480           | 0.1656           | 0                       | 0                         |
| 23-24         | 0.1310           | 0.2690           | 50                      | 10                           | 69-70         | 0.0729           | 0.2484           | 0                       | 0                         |
| D-25          | 0.0567           | 0.1932           | 50                      | 30                           | 70-71         | 0.0567           | 0.1932           | 200                     | 1500                      |
| 25-26         | 0.1048           | 0.2152           | 100                     | 60                           | 71-72         | 0.0262           | 0.0528           | 200                     | 0                         |
| 26-27         | 0.2489           | 0.5111           | 100                     | 70                           | J-73          | 0.3240           | 1.1040           | 0                       | 0                         |
| 27-28         | 0.0489           | 0.1650           | 1800                    | 1300                         | 73-74         | 0.0324           | 0.1104           | 0                       | 150                       |
| 28-29         | 0.1310           | 0.2690           | 200                     | 120                          | 74-75         | 0.0567           | 0.1932           | 1200                    | 950                       |
| E-30          | 0.1965           | 0.3960           | 0                       | 0                            | 75-76         | 0.0486           | 0.1656           | 300                     | 180                       |
| 30-31         | 0.1310           | 0.2690           | 1800                    | 1600                         | K-77          | 0.2511           | 0.8556           | 0                       | 0                         |
| 31-32         | 0.1310           | 0.2690           | 200                     | 150                          | 77-78         | 0.1296           | 0.4416           | 400                     | 360                       |
| 32-33         | 0.0262           | 0.0538           | 200                     | 100                          | 78-79         | 0.0486           | 0.1656           | 2000                    | 1300                      |
| 33-34         | 0.1703           | 0.3497           | 800                     | 600                          | 79-80         | 0.1310           | 0.2640           | 200                     | 140                       |
| 34-35         | 0.0524           | 0.1076           | 100                     | 60                           | 80-81         | 0.1310           | 0.2640           | 500                     | 360                       |
| 35-36         | 0.4978           | 1.0222           | 100                     | 60                           | 81-82         | 0.0917           | 0.1883           | 100                     | 30                        |
| 36-37         | 0.0393           | 0.0807           | 20                      | 10                           | 82-83         | 0.3144           | 0.6436           | 400                     | 360                       |
| 37-38         | 0.0393           | 0.0807           | 20                      | 10                           | 5-55          | 0.1310           | 0.2690           |                         |                           |
| 38-39         | 0.0786           | 0.1614           | 20                      | 10                           | 7-60          | 0.1310           | 0.2690           |                         |                           |
| 39-40         | 0.2096           | 0.4304           | 20                      | 10                           | 11-43         | 0.1310           | 0.2690           |                         |                           |
| 38-41         | 0.1965           | 0.4035           | 200                     | 160                          | 12-72         | 0.3406           | 0.6994           |                         |                           |
| 41-42         | 0.2096           | 0.4304           | 50                      | 30                           | 13-76         | 0.4585           | 0.9415           |                         |                           |
| F-43          | 0.0486           | 0.1656           | 0                       | 0                            | 14-18         | 0.5371           | 1.0824           |                         |                           |
| 43-44         | 0.0393           | 0.0807           | 30                      | 20                           | 16-26         | 0.0917           | 0.1883           |                         |                           |
| 44-45         | 0.1310           | 0.2690           | 800                     | 700                          | 20-83         | 0.0786           | 0.1614           |                         |                           |
| 45-46         | 0.2358           | 0.4842           | 200                     | 150                          | 28-32         | 0.0524           | 0.1076           |                         |                           |
|               |                  |                  |                         |                              | 29-39         | 0.0786           | 0.1614           |                         |                           |
|               |                  |                  |                         |                              | 34-46         | 0.0262           | 0.0538           |                         |                           |
|               |                  |                  |                         |                              | 40-42         | 0.1965           | 0.4035           |                         |                           |
|               |                  |                  |                         |                              | 53-64         | 0.0393           | 0.0807           |                         |                           |

TABLE VI  
THE PARAMETER OF THE PROPOSED METHOD FOR CASE STUDY 2

| CASE                       | EXAMPLE II |
|----------------------------|------------|
| LENGTH OF CHROMOSOME       | 96         |
| POPULATION SIZE            | 60         |
| CROSSOVER PROBABILITY (PM) | 0.7        |
| MUTATION PROBABILITY (PC)  | ADAPTIVE   |
| NUMBER OF ITERATION        | 690        |

TABLE VII  
DETAILS OF ENERGY SUPPLY COST CALCULATION FOR BEST CONFIGURATION (C2) OF EXAMPLE II

| FEEDING<br>SUBSTATION<br>NUMBER               | LOSS OF<br>FEEDER<br>(KW) | LOADS OF<br>FEEDER<br>(KW) | ENERGY<br>PRICE<br>IN FEEDER<br>(\$/MWH) | ENERGY SUPPLY<br>COST<br>IN FEEDER<br>(US\$) |
|---|---------------------------|----------------------------|--|--|
| A   | 48.05                     | 2270                       | 11.1                                     | 617.5  |
| B   | 53.28                     | 3200                       | 10.9                                     | 851.1  |
| C   | 75.03                     | 4050                       | 11                                       | 1089   |
| D   | 49.66                     | 3080                       | 10.8                                     | 811.208                                      |
| E   | 15                        | 1800                       | 11.9                                     | 518.36                                       |
| F   | 14.046                    | 1930                       | 11                                       | 513.23                                       |
| G   | 61.822                    | 3100                       | 11.9                                     | 903.02                                       |
| H   | 56.093                    | 2170                       | 10.5                                     | 560.98                                       |
| I   | 53.561                    | 2450                       | 11.4                                     | 684.97                                       |
| J   | 7.66                      | 1200                       | 11.3                                     | 327.52                                       |
| K   | 50.436                    | 3100                       | 11.2                                     | 846.84                                       |
| System Total Energy Supply Cost (\$) = 7723.7 |                           |                            |  |  |

TABLE VIII  
COMPARATIVE NUMERICAL RESULTS OF EXAMPLE II

|    | CASE  | OPEN SWITCHES  | VOLTAGE OF BUSES |     | POWER LOSS<br>(MW) | TOTAL ENERGY<br>SUPPLY COST<br>(\$) |
|----|---|--|------------------|-----|--------------------|-------------------------------------|
|    |   |  | V <sub>MIN</sub> | BUS |                    |                                     |
| C1 | UN-DEREGULATED SYSTEMS WITH ONLY<br>LOSSES MINIMIZATION     | 55, 7, 86, 72, 13, 89, 90, 83, 92,<br>39, 34, 42, 62 | 0.9532           | 71  | 0.46985            | 7750.6                              |
| C2 | DEREGULATED SYSTEMS WITH ENERGY<br>SUPPLY COST MINIMIZATION | 55, 7, 63, 86, 72, 76, 89, 90, 82,<br>42, 32, 34, 36 | 0.9517           | 9   | 0.48464            | 7723.7                              |