# Comparison of Ageing Deterioration of Silicone Rubber Outdoor Polymer Insulator under Salt Water Dip Wheel Test

## J. Grasaesom, S. Thong-om, W. Payakcho, A. Oonsivilai and B. Marungsri

**Abstract**—This paper presents the experimental results on ageing deterioration of silicone rubber outdoor polymer insulator under salt water dip wheel test based on IEC 62217. In order to comparison effect of chemical contents, silicone rubber outdoor polymer insulators having same configuration and leakage distant from two manufactures were tested together continuously 30,000 test cycles. Many discharge activities were observed in during the test. After 30,000 test cycles, in spite of same configuration, differences in degree of surface aging were observed. Physical analysis such as decreasing in hydrophobicity and increasing in hardness measurement were measured on two-type tested specimen surface in order to confirm degree of surface ageing. Furthermore, chemical analysis by ATR-FTIR to diagnose the chemical change of tested specimen surface was conducted to confirm the physical analysis results.

*Keywords*—ageing of silicone rubber, salt water dip wheel test, silicone rubber polymer insulator

## I. INTRODUCTION

CILICONE rubber or polydimethylsiloxane (PDMS) has Deen widely used to produced housing material for insulators in high voltage outdoor insulation system. Silicone rubbers have advantages of low cost, light weight, high mechanical strength, low surface tension energy and good electrical strength comparing with porcelain and glass insulators. Due to silicone rubber or PDMS having organic nature, environmental conditions are important factor for structural changing in PDMS material. In addition, electrical stress is mainly caused discharge activities to polymer insulator surface such as dry band arc and corona discharge etc. Resulting, polymer insulator surface was damaged by environmental and electrical conditions. Physical change (such as tracking) and chemical change (such as loss of hydrophobicity) were affected to ageing on polymer insulator surface [1-5].

Yu et al. [6] studied about the properties of tracking wheel test method under DC voltages such as positive DC voltage and negative DC voltage. The result of tested under DC

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voltage compared with the result of tested under AC voltage.

Muncivi et al. [7] used the software and hardware computer control were studied the tracking of the silicone rubber polymer insulators. The testing of silicone rubber polymer insulators were tested 181 cycles base on BS EN 62217:2006.

This paper reports the experimental study on ageing deterioration of silicone rubber outdoor polymer insulator for 22 kV distribution systems under salt water dip wheel test.

#### **II. TEST ARRANGEMENTS**

#### A. Specimen

Straight shed polymer insulators made of HTV silicone rubber with ATH (Alumina trihydrate) were used in this experimental. This type of polymer insulator is used for 22 kV distribution systems. However, amounts of chemical contents of housing material are different due to different manufactures. All specimens having same configuration and dimension were tested together under test conditions based on IEC 62217 [8]. Configuration and dimension of the specimen are illustrated in Fig. 1.



## B. Test Method

Test methods for salt water dip wheel test were based on IEC 62217 [9]. Cyclic test was conducted continuously for 30,000 cycles. One test cycle takes 192 second and includes 4 test positions, energized, de-energized, salt water dip and deenergized, respectively. At each position, specimen remains stationary for 40 second and takes 8 second for rotate to the next position. Salt water was re-newed every week with renewing time less than 1 hour. Test arrangement for dip wheel test is shown in Fig. 2 and the specimen arrangement during test is shown in Fig. 3.



Fig. 2 Test arrangement for salt water dip wheel test



Fig. 3 Specimen arrangement during salt water dip wheel test

## C. Test Condition

Test was conducted based on test conditions in IEC 62217, as illustrated in Table I. Test voltage was generated from 22 kV, 30 kVA single phase transformer.

TABLE I	
TEST CONDIT	IONS
Voltage stress	35 V/mm (AC voltage)
NaCl content of de-ionized water	$1.4 \text{ kg/m}^3 \pm 0.06 \text{ kg/m}^3$
Test duration (1 cycle = $192$ second)	30,000 cycles

#### III. EXPERIMENTAL RESULTS AND DISCUSSIONS

Degree of physical damaged was inspected by visual observation, reduction of hydrophobicity, surface contamination degree and hardness after 30,000 test cycles. In addition, any chemical changing of specimen surface was analyzed by using ATR-FTIR. The chemical analysis results were used to confirm the physical changing.

## A. Visual observation

During test, visual observation was used to observe the physical changing of silicone rubber polymer insulators surface. Many discharge activities were observed during the test, dry band arc and corona discharge were often observed on the trunk surface.

As shown in Fig. 4, visible discharge activities during the test were often observed on the trunk surface for all specimens. Yellow light paths indicate dry band arcing and purple light spot indicate corona discharges. These phenomenons caused reduction of hydrophobic and ageing deterioration on surface of silicone rubber polymer insulators [9-12].



Fig. 4 Visible discharge activities during salt water dip wheel test.

After 30,000 test cycles, significant changing on the specimen surface was observed on all tested specimen. Many types of surface ageing, such as erosion and tracking etc., were observed.

As shown in Fig. 5 (a), dirt was observed on both shed and trunk surfaces of tested specimen.

As shown in Fig. 5 (b), slightly surface tracking was observed on parting line of trunk surface near the energized end.

As shown in Fig 5 (c) and Fig. 5 (d), severely tracking was observed on the parting line of trunk surface near the grounded end. The occurrence of surface tracking on such position may due to higher electric field stress. Electrical discharges may cause surface damaged [13].

As shown in Fig. 6 (a), dirt was observed on both shed and trunk surface of type-B specimen same as type-A specimen

As shown in Fig. 6 (b) and Fig. (c), slightly surface tracking was observed on both shed and trunk surface near the energized end.As shown in Fig. 6 (d), punched of trunk near

ground end was observed. The puncture was observed on the parting line of trunk.



Fig. 5 Surface damaged of Type-A specimen





After contaminant removal

(c) Tracking on trunk

(a) Dirt on shed surface



ninant rei

ant remova

(d) Tracking on trunk





(b) Tracking on shed parting line



(c) Tracking on parting line of trunk.

(d) Tracking on parting line of trunk. Fig. 6 Surface damaged of Type-B specimens

Before contam

## B. Contamination Degree

Under contamination condition, contamination layer causes leakage current along the specimen surface and leakage current causes dry band. Finally, higher electric field stress over dry band causes dry band arcing. Dry band arcs cause tracking on the insulator surface. Therefore, salt deposit density (SDD) is used to identify the contamination level along the insulators surface. The formulas for SDD calculation are as follows.

$$S_a = \left(5.7\sigma_{20}\right)^{1.03} \tag{1}$$

 $SDD = \frac{S_a \times V}{A}$ (2)

where:

is the volume conductivity at temperature of 20°C  $\sigma_{20}$ (S/m)

$$S_a$$
 is salinity (kg/m<sup>3</sup>)

*SDD* is the salt deposit density 
$$(kg/m^2)$$

- V is the volume of the suspension  $(m^3)$
- is the area of the cleaned surface  $(m^2)$  [14,15]. A

TABLE II							
SDD AFTER 30,000 TEST CYCLES							
	SDD, mg/cm <sup>2</sup>						
Type-A Specimen Type-B Specimen							
No. 1	0.0205	No. 1	0.0228				
No. 2	0.0178	No. 2	0.0149				

As illustrated in Table II, no significant different in SDD was obtained. This may due to tested specimen having same configuration and dimension.

## C. Hydrophobicity

By products from discharge activities such as heat and UV

can cause reduction of hydrophobicity of polymer insulator surface. STRI classification guide as shown in Fig. 7, is used to specified the level of hydrophobicity for the specimens [16,17]. HC level for tested specimen was evaluated. The evaluation results are shown in Fig. 8 and are shown in Table III.

After 30,000 test cycles, reduction of hydrophobicity level on all specimens was obtained when comparing with the new specimen. As illustrated in Table III, largest reduction of hydrophobicity (HC5) was measured on trunk surface of all specimens. For shed surface, reduction of hydrophobicity level at HC3 was measured.



Fig. 7 Classification of hydrophobicity (HC1-HC6)[15]



New Type-B Specimen







Type-B Specimen No. 1 Type-B Specimen No. 2 Fig. 8 Comparison of reduction of hydrophobicity

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			Speci	imen			Position
Position		Type-A			Type-B		Energized end
	New	No. 1	No. 2	New	No. 1	No. 2	5
1	$\mathbf{T}$	HC3	HC5	$\mathbf{T}$	HC3	HC4	.)
2	Ì	HC3	HC3	Ì	HC4	HC4	
3		HC4	HC2		HC3	HC3	
4		HC5	HC4		HC5	HC5	
5		HC4	HC4		HC4	HC4	4 5
6		HC3	HC3		HC3	HC3	7 6
7		HC5	HC4		HC4	HC5	/ 8
8		HC3	HC4		HC4	HC4	10 9
9	-	HC3	HC3	CI-	HC3	HC3	
10	Ŧ	HC5	HC4	H 	HC5	HC5	
11		HC4	HC4		HC4	HC4	16 15
12		HC3	HC3		HC3	HC3	10 17
13		HC3	HC3		HC5	HC5	$P^{19}$ 18
14		HC4	HC3		HC4	HC4	:
15		HC3	HC3		HC3	HC2	
16		HC4	HC3		HC5	HC4	()
17		HC3	HC3		HC4	HC4	ビ
18	j	HC4	HC3	ļ	HC3	HC2	Grounded end
19	¥	HC3	HC3	¥	HC4	HC4	

REDUCTION OF HYDROPHOBICITY AFTER 30,000 TEST CYCLES	TABLE III	
	REDUCTION OF HYDROPHOBICITY AFTER 30,000	TEST CYCLES

## D. ATR-FTIR Analysis

ATR-FTIR (attenuated total reflection Fourier transform infrared spectroscopy) is chemical analysis technique for the chemical bonds changing inspection. Side chains bond (Si-CH<sub>3</sub>) at wave number 1258 cm<sup>-1</sup> and back bond (Si-O) at wave number 1010 cm<sup>-1</sup> of silicone rubber surface were analyzed. Reduction of Si-CH<sub>3</sub> indicates side chain scission. Reduction of Si-O spectrum indicates back bond scission. An example of ATR-FTIR spectrum of trunk surface at position 10 of tested surface comparing with the new specimen surface is illustrated in Fig. 9.After 30,000 test cycles, decreasing of side chain and back bond spectrums were obtained for both types of tested specimens when comparing with the new specimen. Mostly changing of side chain and back bone bonds were measured on trunk surface when comparing with shed surface. ATR-FTIR analysis results for all position of all-type specimens are illustrated in Table IV and Table V.



Fig. 9 ATR- FTIR spectrum of Type-A specimen at position 10

# International Journal of Electrical, Electronic and Communication Sciences ISSN: 2517-9438 Vol:5, No:12, 2011

TRANSMITTANCE OF SI-CH $_3$ BOND AFTER 30,000 TEST CYCLES								
		Transm	Position					
Position	Т	Type-A Specimen Type-B Specimen				Energized end		
	New	No. 1	No. 2	New	No. 1	No. 2		
1		49.60	53.86		22.20	36.38	ר ( ר	
2	$\mathbf{T}$	77.79	80.70	$\uparrow$	77.65	80.36		
3		79.11	86.18		84.99	80.37		
4		59.08	41.07		13.60	30.96		
5		79.03	75.34		82.39	77.35	4 3	
6		82.25	88.65		88.35	70.83	5	
7		42.75	26.59		45.43	67.78	7 6	
8		85.02	88.44		78.56	77.67		
9	00	83.93	84.41	-00	95.17	82.42	10 11	
10	Ī	68.07	51.91	Ī	36.00	66.30	13 12	
11		74.26	81.95		76.66	84.61	15 14	
12		82.16	88.78		81.81	80.28	16 15	
13		75.60	22.14		64.19	43.66	17	
14		83.18	97.42		85.93	73.61		
15		85.75	97.43		83.07	83.43	:	
16		69.19	49.02		71.42	70.57	$L^{L}$	
17		78.77	94.55		82.76	75.57	ン)	
18		73.83	91.29		73.49	70.04	Grounded end	
19	$\downarrow$	68.18	26.95	Ý	37.83	21.46	Grounded the	

TABLE IV	
RANSMITTANCE OF SI-CH3 BOND AFTER 30,000 TEST CY	CL

TABLE V
TRANSMITTANCE OF SI-O BOND AFTER 30,000 TEST CYCLES

		Transi	Position				
Position	Т	ype-A Specim	en	Ту	pe-B Specim	ien	Energized end
	New	No. 1	No. 2	New	No. 1	No. 2	Ň
1		79.01	75.33		63.70	80.40	5)
2	$\uparrow$	78.81	86.04	$\uparrow$	92.73	88.83	
3		80.09	87.98		92.74	89.42	
4		84.90	69.26		93.37	69.76	
5		82.33	81.80		89.90	88.35	
6		86.58	91.80		93.88	85.56	4 5
7		69.10	63.31		85.57	68.68	7 6
8		85.87	88.98		99.61	84.99	8
9	-00	83.24	86.19	-00	96.05	87.37	10 11
10	Ť	87.43	80.33	Ī	70.49	86.04	
11		79.74	84.57		92.87	91.04	13 14
12		84.37	88.89		93.34	84.12	16 15
13		83.54	57.47		90.28	80.18	17
14		91.51	96.44		92.07	92.94	
15		88.26	96.41		94.02	86.74	
16		85.93	81.23		94.20	85.82	μ
17		84.02	94.35		91.73	89.73	り)
18		78.69	91.22		92.90	87.93	Grounded end
19	Ý	87.52	40.87	Ý	79.43	52.01	Grounded end

## E. Hardness Measurement Results

In this study, hardness was measured based on ISO 686-Shore hardness [18] by using Shore durometer. Measurement results of hardness are shown in Table VI. As shown in Table VI, increasing in hardness of all tested specimens was obtained when comparing with new

specimen. Increasing in surface hardness indicate the occurrence of oxidation crosslink of polydymethylsiloxane matrix. More increasing in hardness was measured on specimen type–A when comparing specimen type-B. In addition, increasing of surface hardness confirmed the chemical reaction in the specimen surface.

		H	ARDNESS OF S	TABLE PECIMEN AFT	VI er 30,000 tes	ST CYCLES		
			Position					
Position	Type-A Specimen Type-B Specimen				Type-A Specimen		en	Energized end
	New	No. 1	No. 2	New	No. 1	No. 2	$\square$	
1		51.68	52.80		52.24	55.20	り)	
2	$\mathbf{T}$	61.36	63.04	$\mathbf{T}$	56.96	56.88	ÍÍ	
3		51.52	63.28		50.80	53.36	:	
4		42.16	50.40		49.76	48.48		
5		53.48	63.12		53.04	54.32	4 3	
6		62.56	63.52		57.76	56.40		
7		42.56	47.92		50.32	48.24	7 8	
8		61.84	61.84		57.84	56.64		
9	08	61.92	62.72	- 36 -	51.28	52.40	10 11	
10	-38.	42.40	51.28	- 43	50.32	48.24	13 12	
11		62.40	62.80		54.72	55.60	14	
12		62.48	62.96		58.16	55.36	16 15 17	
13		43.28	46.00		74.2	46.96	19 18	
14		62.16	62.80		58.64	57.04	$\mathbf{P}^{\prime}$	
15		61.76	62.64		54.16	55.20	:	
16		47.12	46.64		49.04	54.56	LΥ	
17		62.96	63.20		56.96	54.56	い)	
18		63.20	62.88		53.04	56.80	Ground end	
19	$\downarrow$	54.24	52.64	$\downarrow$	54.16	50.64	Ground end	

#### IV. CONCLUSION

Silicone rubber polymer insulators having same configurations and dimensions from two manufacturers were tested under salt water dip wheel test for 30,000 cycles and were subjected to electric field at 35 V ac /mm. Surface tracking and trunk puncture were observed on both type specimen surfaces after 30,000 test cycles. However, severely tracking was observed on specimen type–A comparing with specimen type– B. Physical analysis results and chemical analysis results confirmed the experimental results as well.

#### ACKNOWLEDGMENT

The authors would like to thank you Suranaree University of Technology and Precise Electric Manufacturing CO., LTD. for kind financial support.

#### REFERENCES

 M. G. Danikas, "Polymer Outdoor Insulators", Department of Electrical and Computer Engineering, Democritus University of Thrace, Vol. 40, No. 1, pp. 3-10, 1999.

- [2] J. Grasaesom, S. Thong-om, W. Payakcho and B. Marungsri, "Ageing Deterioration of Silicone Rubber Polymer Insulator under Salt Water Dip Wheel Test", *World Academy of Science, Engineering and Technology*, Issue 80, August 2011, pp. 211-217.
- [3] S. Thong-om, W. Payakcho, J. Grasaesom and B. Marungsri, "Study of Ageing Deterioration of Silicone Rubber Housing Material for Outdoor Polymer Insulators", *World Academy of Science, Engineering and Technology*, Issue 80, August 2011, pp. 533-539.
- [4] S. Kumagai, B. Marungsri, H. Shinokubo, R. Matsuoka and N. Yoshimura, "Comparison of Leakage Current and Aging of Silicone Rubbers and Porcelain in both Field and Salt-fog Tests", *IEEE Transaction on Dielectrics and Electrical Insulation*, Vol. 13, pp. 1286-1302, 2006.
- [5] W. Payakcho, J. Grasaesom, S. Thong-om and B. Marungsri, "Artificial Accelerated Ageing Test of Silicone Rubber Housing Material for Lightning Arrester", World Academy of Science, Engineering and Technology, Issue 80, August 2011, pp. 650-655.
- [6] Y. Yu, L. Xidong, Z. Yuanxiang and L. Xuesong, "Study of Tracking Wheel Test Method under DC Voltage", *International Conference on Properties and Applications of Dielectric Materials*, Vol. 1, No. 1, pp. 439-442, 2003.
- [7] A. Muncivi, P. Sarkar and A. Haddae, "Tracking Wheel Test Facilities", in Conference Record of IEEE International Conference on Communications, pp. 1-5, 2009.
- [8] IEC 62217 Ed. 1.0, Committed Draft, Sep, 2002.

## International Journal of Electrical, Electronic and Communication Sciences ISSN: 2517-9438 Vol:5, No:12, 2011

- [9] M. Amin and M. salman, "Aging of Polymer Insulators (An Overview)", Department of Electrical Engineering, University of Engineering and Technology, 2006.
- N. Yoshimura and S. Kumagai, "Electrical Environmental Aging of [10] Silicone Rubber Used in Outdoor Insulation", IEEE Transaction on Dielectrics and Electrical Insulation, Vol. 6, pp. 632-650, 1999.
- [11] B. Marungsri, H. Shinokubo and R. Matsuoka, "Effect of Specimen Configuration on Deterioration of Silicone Rubber for Polymer Insulators in Salt Fog Ageing Test", IEEE Transaction on Dielectrics and Electrical Insulation, Vol. 13, pp. 129-138, 2006.
- [12] I. J. S. Lopes, S. H Jayaram and E. A. Cherney, "A Method for Detecting the Transition from Corona from Water Droplets to Dry-Band Arcing on Silicone Rubber Insulators", IEEE Trans .on DEI., Vol. 6, pp. 964-971, 2002.
- [13] J. Burnham, "Guideline for Visual Identification of Damage Polymer Insulators" France 1998
- [14] M. A. Salam, N. Mohammad, Z. Nadir and A. A. Magrashi, "Measurement of Conductivity and Equivalent Salt Deposit Density of Contaminated Glass Plate", TENCON 2004, 2004 IEEE Region 10 Conference, Vol. 3, pp.268-270, 2004.
- [15] IEC 60507 Ed. 2 b: 1991, "Artificial pollution tests on high-voltage insulators to be used on AC systems"
- [16] H. Gao, Z. Jia, Y. Moa, Z. Guan and L. Wang, "Effect of Hydrophobicity on Electric Field Distribution and Discharges along Various Wetted Hydrophobic Surfaces", IEEE Transaction Dielectrics and Electrical Insulation, Vol. 15, pp. 435-443, 2008.
- [17] STRI Guide, "Hydrophobicity Classification Guide", 92/1, 1992.
- [18] ISO 868, "Plastics and ebonite Determination of indentation hardness by means of a durometer (Shore hardness)".



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