

# Wave-Structure Interaction for Submerged Quarter-Circle Breakwaters of Different Radii - Reflection Characteristics

Arkal Vittal Hegde, L. Ravikiran

**Abstract**—The paper presents the results of a series of experiments conducted on physical models of Quarter-circle breakwater (QBW) in a two dimensional monochromatic wave flume. The purpose of the experiments was to evaluate the reflection coefficient  $K_r$  of QBW models of different radii ( $R$ ) for different submergence ratios ( $d/h_c$ ), where  $d$  is the depth of water and  $h_c$  is the height of the breakwater crest from the sea bed. The radii of the breakwater models studied were 20cm, 22.5cm, 25cm, 27.5cm and submergence ratios used varied from 1.067 to 1.667. The wave climate off the Mangalore coast was used for arriving at the various model wave parameters. The incident wave heights ( $H_i$ ) used in the flume varied from 3 to 18cm, and wave periods ( $T$ ) ranged from 1.2 s to 2.2 s. The water depths ( $d$ ) of 40cm, 45cm and 50cm were used in the experiments. The data collected was analyzed to compute variation of reflection coefficient  $K_r = H_r/H_i$  (where  $H_r$ =reflected wave height) with the wave steepness  $H_i/gT^2$  for various  $R/H_i$  ( $R$ =breakwater radius) values. It was found that the reflection coefficient increased as incident wave steepness increased. Also as wave height decreases reflection coefficient decreases and as structure radius  $R$  increased  $K_r$  decreased slightly.

**Keywords**—Incident wave steepness, Quarter-circle breakwater, Reflection coefficient, Submergence ratio.

## I. INTRODUCTION

THE principle purpose of a breakwater system is to intercept the incident waves and cause them to break or reflect, thereby reducing energy of the incoming waves [1]. The submerged type breakwaters, of late, are more frequently used as a 'soft' solution in mitigating coastal engineering problems like providing tranquility in harbors, bays etc. A submerged breakwater is a wave barrier with its crest at or slightly below the still water level. According to [2] submerged coastal structures are widely perceived to be capable of providing beach protection, without the adverse impacts (including loss of beach amenity and aesthetic conditions) often associated with more conventional structures such as revetments and groins. In situations where complete protection from waves is not required, submerged breakwaters offer a potentially economic solution. Submerged breakwaters have been effectively used to protect harbor entrances, to

reduce siltation in entrance channels, for beach erosion mitigation, and for creation of artificial fishing grounds [3]. Quarter-circle breakwater (QBW) is a new type breakwater first proposed by [4] on the basis of semicircular breakwater (SBW) concept. Similar to SBW, QBW is usually placed on a rubble mound foundation and its superstructure consists of a quarter circular surface facing the incident waves, a horizontal bottom and a lee-side vertical wall. The present paper considers a comprehensive laboratory investigation to evaluate the reflection characteristics of the submerged QBW for different radii of physical models, still water levels, wave heights, wave periods etc.

## II. LITERATURE REVIEW – PHYSICAL AND NUMERICAL MODELS

Reference [5] reports “A physical model is a precision device used to predict the behavior of a physical phenomenon. A model can be regarded as reliable only if it is designed correctly”. A few physical and numerical model studies have been carried out by researchers in this area. A series of two-dimensional (vertical) wave numerical model and also physical model studies have been conducted by [6] to research the performances of QBW by comparing the hydraulic behaviors of SBW and QBW under same hydraulic conditions. As far as reflection is concerned they found that the reflection coefficient values of QBW and SBW are closer, with values less than 1.0 under same conditions, even if  $h_c$  reaches 2 to 3 times of incident wave height. The reflection coefficient  $K_r$  increases with  $h_c/H_i$  increasing. They concluded, the flow fields in front of the breakwater in both the cases of submerged and emerged are similar, which imply the resemblance of reflection coefficients for both breakwaters.

Reference [7] discusses about a series of regular and irregular wave experiments conducted to study the reflection and transmitting performances of quarter-circle breakwater in comparison with those of the semicircular breakwater. There were two kinds of reflection coefficients discussed: a). “Resolution reflection coefficient” based on the standard concept of reflection coefficient with the expression of  $K_r = H_r/H_i$  which represents the whole effect of wave reflection by breakwater, and b). “Circular-surface reflection coefficient” which was denoted as  $K_{rc}$  which was used to describe the reflective effect by circular surface on the adjacent flow field in front of the breakwater. They found that the fact of  $K_{rc} < K_r$  at the same relative freeboard height ( $h_c/H_i$ ) indicates that the entire reflective effect of QBW is stronger than that by circular surface on the adjacent flow field. They

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also stated that the reflection and transmission performances of QBW are more sensitive to the relative freeboard height ( $h_c/H_i$ ) than to the wave steepness ( $H_i/L_i$ ).

### III. DIMENSION ANALYSIS AND TEST MODELS

Dimensional analysis was carried out using Buckingham's  $\pi$  theorem. The variables considered in the present investigations are as follows:  $d$ , depth of water;  $L$ , wavelength;  $H_i$ , incident wave height;  $T$ , wave period;  $g$ , acceleration due to gravity;  $h_c$ , height of structure crest (from sea bed). Considering  $H_i$  and  $g$  as repeating variables, the dimensional analysis yielded following non-dimensional  $\pi$  terms:  $H_i/H_i$  (=reflection coefficient  $K_r$ ),  $H_i/gT^2$  (incident wave steepness),  $d/h_c$  (submergence ratio). Four physical models of different radii i.e. 20cm, 22.5cm, 25cm and 27.5cm were used in this study. Each model consisted of two parts, the base slab and the top quarter-circle shaped caisson. The fabrication of the model was done in two steps, one - the casting of base slab, and secondly - the fabrication of the quarter-circle caisson. The bottom slabs of sizes 0.3m X 0.73m X 0.05m, 0.325m X 0.73m X 0.05m, 0.35m X 0.73m X 0.05m and 0.375m X 0.73m X 0.05m were used in the experiments. These dimensions were chosen in order to maintain the weight of the QBW to make them stable during the wave attack.

Galvanized Iron (G.I.) sheet of 0.002m thickness was used to fabricate the quarter-circle shaped caisson and the sheet was coated with cement slurry to simulate concrete surface. The sheet was fixed to the base slab with the help of stiffeners made up of flat plates. Models were then placed over the rubble mound foundation of thickness 0.05m on a scale of 1:30. The prototype minimum thickness of 0.5m is prescribed by [8] and stones weighing from 50 gm to 100 gm were used to form the foundation. A typical submerged QBW model cross section of 0.2m radius is shown in Fig. 1 with all relevant details.

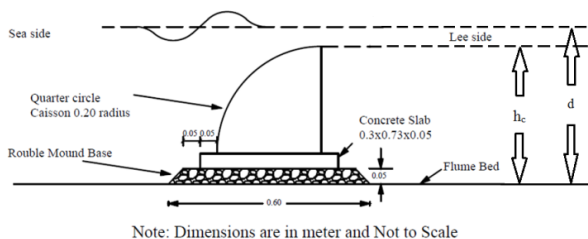


Fig. 1 Quarter-circle breakwater model section of radius 0.2m

### IV. EXPERIMENTAL SETUP

The present study is conducted in the monochromatic wave flume of the Marine Structures laboratory of the Department of Applied Mechanics and Hydraulics, National Institute of Technology Karnataka (N.I.T.K.), Surathkal, Mangalore, Karnataka state in India. The model was placed in the flume 28m away from the wave flap, above the rubble mound foundation. The slope used for the rubble foundation is 1:2 as shown in Fig. 2. Three capacitance type wave probes were used for measuring the incident, reflected and transmitted

wave heights. The wave probes were placed at a distance of 4 m from the centre of the model. Three probes were kept in front of the breakwater to measure the reflected waves using the three-probe method proposed by [9]. The spacing between the probes is kept equal to  $L/3$ , where  $L$  is the wavelength. A burst of five waves are generated to avoid the successive reflection. For the measurement of transmitted waves, a single probe is placed at the leeside of the breakwater. The surface elevation measured by the probes are recorded by the wave recorder and voltage signals are converted into wave heights and wave periods using the laboratory wave recorder software provided by Environmental Measurements and Controls (E.M.C.O.N), Kochi, India.

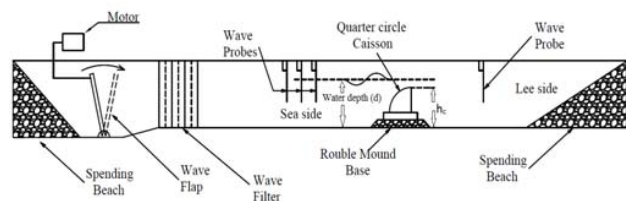


Fig. 2 Monochromatic wave flume setup used for the investigation

TABLE I  
EXPERIMENTAL VARIABLES AND THEIR RANGE OF VALUES

Parameters	Experimental range
Wave-specific parameters	
Incident wave height, $H_i$ (m)	0.03, 0.06, 0.09, 0.12, 0.15, 0.18
Wave period, $T$ (sec)	1.2, 1.4, 1.6, 1.8, 2.0, 2.2
Depth of water, $d$ (m)	0.40, 0.45, 50
Submergence ratio, $d/h_c$	1.06-1.667
Structure-specific parameters	
Radius of the Quarter-circle caisson (m)	0.2, 0.225, 0.25, 0.275

### V. ANALYSIS OF RESULTS AND DISCUSSION

According to [10] when waves get reflected by a structure, the reflected waves cause increased agitation of the water in front of the structure. Clearly, a part of the energy of the incident waves is always reflected by the submerged structure. The amount of reflection depends on the wave parameters and the depth of submergence. The graphs are plotted to understand the variation of  $K_r$  with  $H_i/gT^2$  for the range of  $d/h_c$  and  $R/H_i$  values used in the experiments. Figs. 3-14 show the variation of reflection coefficient  $K_r$  with the incident wave steepness  $H_i/gT^2$  for various submergence ratios  $d/h_c$  and different  $R/H_i$  ranges. The values of  $d/h_c$  used are in the range 1.06-1.66 and  $R/H_i$  values in the range of 1.1-9.5. In all the cases depicted by Figs. 3-14, it may be observed that the reflection coefficient increases logarithmically (best-fit) as incident wave steepness increases for all values of  $d/h_c$  and  $R/H_i$ . Clearly, whatever may be the depth, caisson radius, height of structure crest (from sea bed), there is always increase in reflection coefficient with increase in wave steepness. Hence, steeper waves (greater wave height and lesser wave periods) cause more of reflection from the breakwater structure.

Figs. 15-17 show the variation of reflection coefficient  $K_r$  with  $R/H_i$  (ratio of model radius to incident wave height) for different  $d/gT^2$  values, and for all the values of  $h_c$ . As  $R/H_i$  increases  $K_r$  is found to decrease in a logarithmic variation (best-fit). Fig. 15 shows the same for the  $d/gT^2$  range of 0.008 to 0.028 ( $d=50$  cm). Similarly Figs. 16, 17 represent the same variation for  $d/gT^2$  ranges of 0.009 to 0.0318 ( $d=45$  cm), and 0.01 to 0.035 ( $d=40$  cm) respectively. In other words, as the structure radius  $R$  increases,  $K_r$  decreases. Further, as wave height decreases, reflection coefficient also decreases.

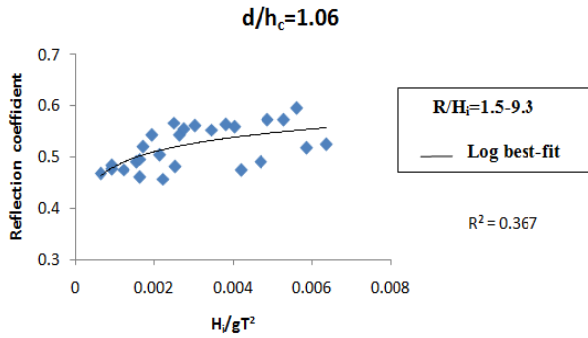


Fig. 3 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.5-9.3$

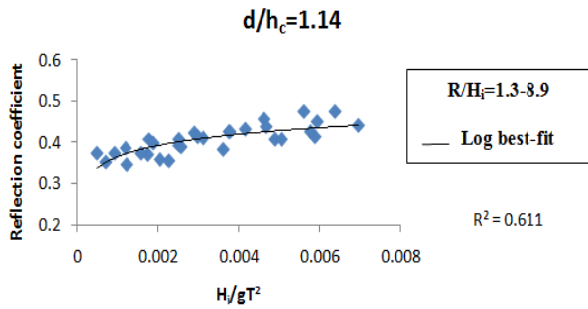


Fig. 4 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.3-8.9$

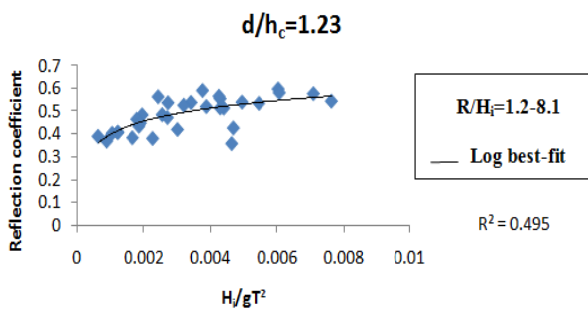


Fig. 5 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.2-8.1$

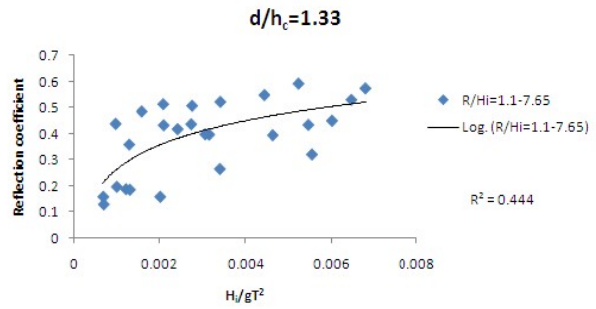


Fig. 6 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.1-7.65$

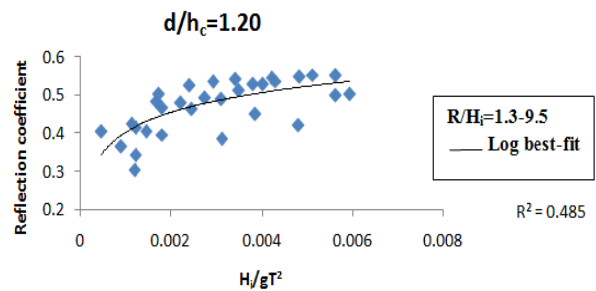


Fig. 7 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.3-9.5$

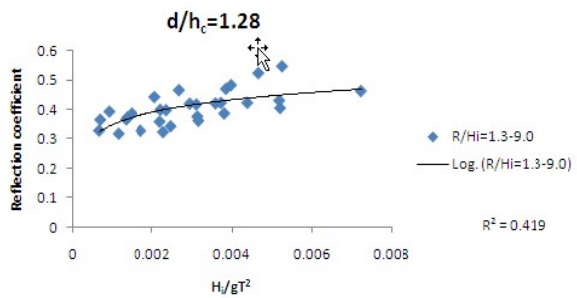


Fig. 8 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.3-9.0$

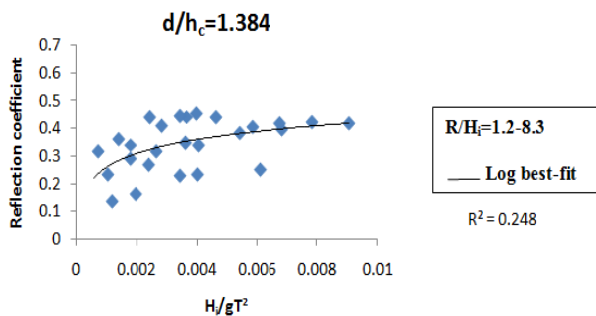
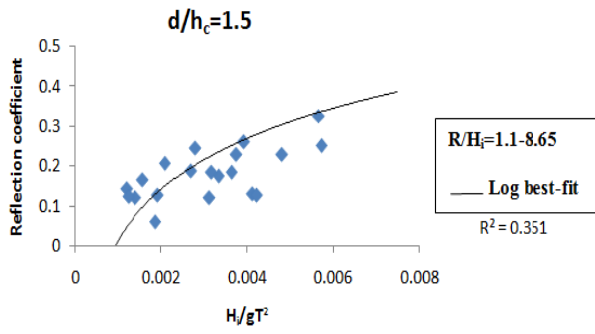
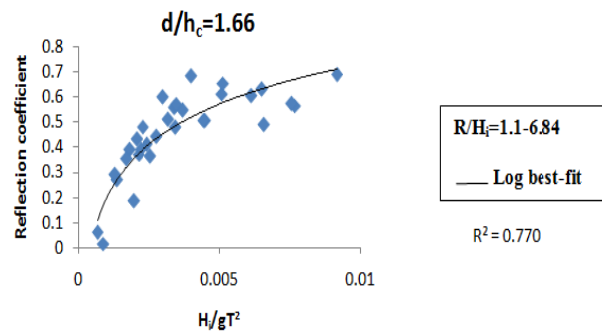
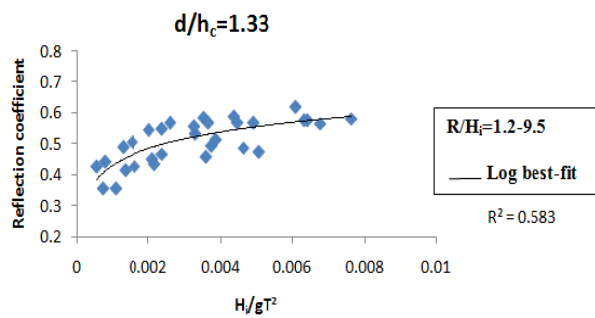
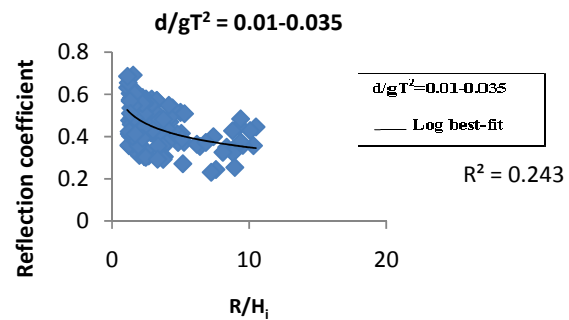
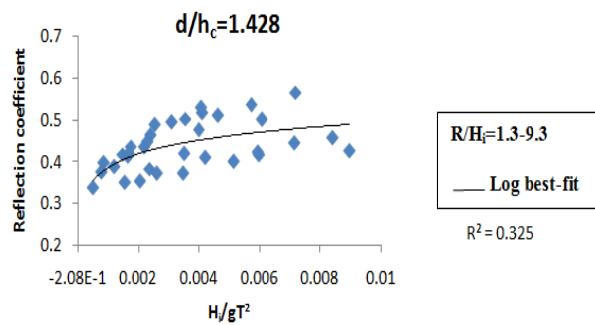
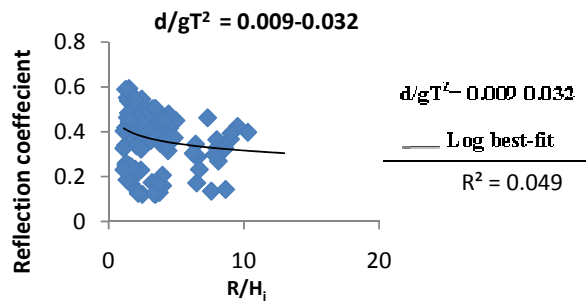
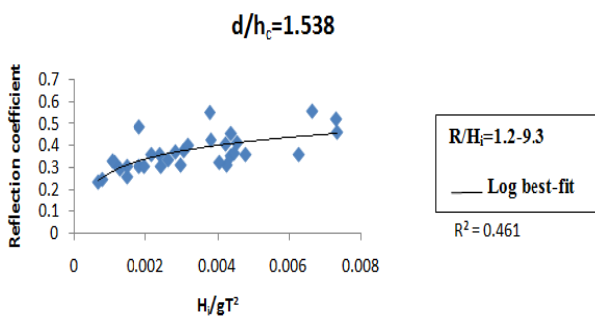
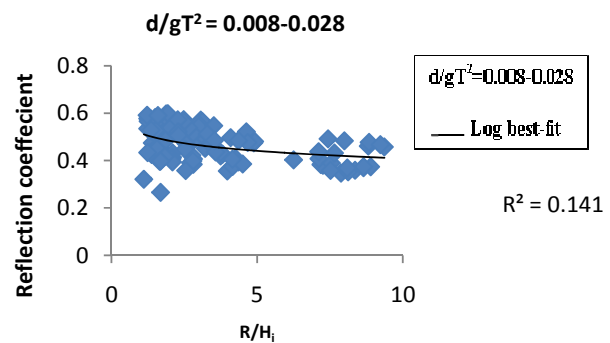


Fig. 9 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.2-8.3$


Fig. 10 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.1-8.65$ 

Fig. 14 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.1-6.84$ 

Fig. 11 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.2-9.5$ 

Fig. 15 Variation of  $K_r$  with  $R/H_i$  for  $d/gT^2=0.01-0.035$ 

Fig. 12 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.3-9.3$ 

Fig. 16 Variation of  $K_r$  with  $R/H_i$  for  $d/gT^2=0.009-0.032$ 

Fig. 13 Variation of  $K_r$  with  $H_i/gT^2$  for  $R/H_i=1.2-9.3$ 

Fig. 17 Variation of  $K_r$  with  $R/H_i$  for  $d/gT^2=0.008-0.028$

## VI. CONCLUSIONS

The paper presents the reflection characteristics of a quarter circle breakwater when subjected to wave action. It is found that reflection coefficient increases logarithmically (best-fit) as incident wave steepness  $H_i/gT^2$  increases, for all values of  $d/h_c$  and  $R/H_i$  used in the experiments. Further, for all the values of  $d/gT^2$  i.e. from 0.008 to 0.035 used in the experiments, reflection coefficient decreases with increase in  $R/H_i$ , which varies from 1.1 to 9.5. Typically, as  $R/H_i$  increases from 1.1 to 9.5,  $K_r$  was found to decrease from about 0.55 to 0.35, which is about 40% and in the logarithmic way.

## ACKNOWLEDGMENT

The authors are thankful to the Director, National Institute of Technology Karnataka, Surathkal, Mangalore, India and also to the Head, Department of Applied Mechanics and Hydraulics, National Institute of Technology Karnataka, Surathkal, Mangalore, India, for their constant support and encouragement in the preparation of this paper.

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