

# The Slant Helices According to Bishop Frame

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**Abstract**—In this study, we have defined slant helix according to Bishop frame in Euclidean 3-Space. Furthermore, we have given some necessary and sufficient conditions for the slant helix.

**Keywords**—Slant helix, Bishop frame, Parallel transport frame

## I. INTRODUCTION

LET  $M$  be an  $n$ -dimensional smooth manifold equipped with a metric  $\langle \cdot, \cdot \rangle$ . A tangent space  $T_p(M)$  at a point  $p \in M$  is furnished with the canonical inner product. If  $\langle \cdot, \cdot \rangle$  is positive definite, then  $M$  is a Riemannian manifold. A curve on an Riemannian Manifold  $M$  is a smooth mapping  $\alpha: I \rightarrow M$ , where  $I$  is an open interval in the real line  $R^1$ . As an open submanifold of  $R^1$ ,  $I$  has a coordinate system consisting of the identity map  $u$  of  $I$ . The velocity vector of  $\alpha$  at  $s \in I$

$$\alpha'(s) = \frac{d\alpha(u)}{du} \Big|_s \in T_{\alpha(s)}M.$$

A curve  $\alpha(s)$  is said to be regular if  $\alpha'(s)$  is not equal to zero for any  $s$ . Let  $\alpha(s)$  be a curve on  $M$ , denote by  $\{T, N, B\}$  the moving Frenet frame along the curve  $\alpha$ . Then  $T, N$  and  $B$  are the tangent, the principal normal and binormal vectors of the curve  $\alpha$  respectively. If  $\alpha$  is a space curve, then this set of orthogonal unit vectors, known as the Frenet-Serret frame, has the following properties

$$\begin{aligned}\alpha'(s) &= T \\ D_T T &= \kappa N \\ D_T N &= -\kappa T + \tau B \\ D_T B &= -\tau N,\end{aligned}$$

where  $D$  denotes the covariant differentiation in  $M$ .

In a Riemann manifold  $M$ , a curve is described by the Frenet formula. For example, if all curvatures of a curve are identically zero, then the curve a geodesic. If only the

curvature  $\kappa$  is a non-zero constant and the torsion  $\tau$  is all identically zero, then the curve is called a circle. If the curvature  $\kappa$  and the torsion  $\tau$  are non-zero constants, then the curve is called a helix. If the curvature  $\kappa$  and the torsion  $\tau$  are not constant but  $\frac{\kappa}{\tau}$  is constant, then the curve is called a general helix [4,7].

The Bishop frame or parallel transport frame is an alternative approach to defining a moving frame that is well defined even when the curve has vanishing second derivative. we can parallel transport an orthonormal frame along a curve simply by parallel transporting each component of the frame. The parallel transport frame is based on the observation that, while  $T(s)$  for a given curve model is unique, we may choose any convenient arbitrary basis  $(N_1(s), N_2(s))$  for the remainder of the frame, so long as it is in the normal plane perpendicular to  $T(s)$  at each point. If the derivatives of  $(N_1(s), N_2(s))$  depend only on  $T(s)$  and not each other we can make  $N_1(s)$  and  $N_2(s)$  vary smoothly throughout the path regardless of the curvature. Therefore, we have the alternative frame equations

$$\begin{bmatrix} T' \\ N_1' \\ N_2' \end{bmatrix} = \begin{bmatrix} 0 & k_1 & k_2 \\ -k_1 & 0 & 0 \\ -k_2 & 0 & 0 \end{bmatrix} \begin{bmatrix} T \\ N_1 \\ N_2 \end{bmatrix}. \quad (1)$$

One can show (see, Bishop [3]) that

$$\begin{aligned}\kappa(s) &= \sqrt{k_1^2 + k_2^2} \\ \theta(s) &= \arctan\left(\frac{k_2}{k_1}\right), k_1 \neq 0 \\ \tau(s) &= -\frac{d\theta(s)}{ds}\end{aligned}$$

so that  $k_1$  and  $k_2$  effectively correspond to a Cartesian coordinate system for the polar coordinates  $\kappa, \theta$  with  $\theta = -\int \tau(s) ds$ . The orientation of the parallel transport frame includes the arbitrary choice of integration constant  $\theta_0$ , which disappears from  $\tau$  (and hence from the Frenet frame) due to the differentiation [1,2].

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## II. THE SLANT HELICES ACCORDING TO BISHOP FRAME

**Definition 2.1.** A regular curve  $\alpha : I \rightarrow E^3$  is called a slant helix provided the unit vector  $N_1(s)$  of  $\alpha$  has constant angle  $\theta$  with some fixed unit vector  $u$ ; that is,  $\langle N_1(s), u \rangle = \cos \theta$  for all  $s \in I$ .

The condition is not altered by reparametrization, so without loss of generality we may assume that slant helices have unit speed. Slant helices can be identified by a simple condition on natural curvatures.

**Theorem 2.1.** Let  $\alpha : I \rightarrow E^3$  be a unit speed curve with nonzero natural curvatures. Then  $\alpha$  is a slant helix if and only

if  $\frac{k_1}{k_2}$  is constant.

**Proof.** Let  $\alpha$  be slant helix in  $E^3$  and  $\langle N_1, u \rangle = \text{const.}$  Then  $\alpha$  is slant helix; from the definition, we have

$$\langle N_1, u \rangle = \text{const.}$$

where  $u$  is a unit vector, called the axis of slant helix. By differentiation we get

$$\langle N_1', u \rangle = \langle -k_1 T, u \rangle = -k_1 \langle T, u \rangle = 0.$$

Hence

$$\langle T, u \rangle = 0.$$

Again differentiating from the last equality, we can write as follows

$$\begin{aligned} \langle T', u \rangle &= \langle k_1 N_1 + k_2 N_2, u \rangle \\ &= k_1 \langle N_1, u \rangle + k_2 \langle N_2, u \rangle \\ &= k_1 \cos \theta + k_2 \sin \theta = 0. \end{aligned}$$

Therefore we obtain

$$\frac{k_1}{k_2} = -\tan \theta$$

as desired.

Suppose that  $\frac{k_1}{k_2} = -\tan \theta$ . Then we can write

$$u \in \text{Sp}\{N_1, N_2\}, \text{ i.e.,}$$

$$u = N_1 \cos \theta + N_2 \sin \theta.$$

Differentiating the last equality,

$$u' = (k_1 \cos \theta + k_2 \sin \theta) T = 0.$$

So  $u$  is a constant vector. Thus, the proof is done.

**Theorem 2.2.** Let  $\alpha = \alpha(s)$  be a unit speed curve in  $E^3$ .

Then  $\alpha$  is a slant helix iff

$$\det(N_1', N_1'', N_1''') = 0.$$

**Proof.** ( $\Rightarrow$ ) Suppose that  $\frac{k_1}{k_2}$  be constant. We have equalities as

$$\begin{aligned} -N_1' &= k_1 T \\ -N_1'' &= k_1' T + k_1^2 N_1 + k_1 k_2 N_2 \\ -N_1''' &= \left( k_1'' - k_1^3 - k_1 k_2^2 \right) T \\ &\quad + \left( 3k_1 k_1' \right) N_1 + \left( 2k_1' k_2 + k_1 k_2' \right) N_2 \end{aligned}$$

So we get

$$\begin{aligned} \det(N_1', N_1'', N_1''') &= k_1^2 \begin{vmatrix} 1 & 0 & 0 \\ * & k_1 & k_2 \\ 0 & 3k_1 k_1' & 2k_1' k_2 + k_1 k_2' \end{vmatrix} \\ &= k_1 \left( \frac{k_1}{k_2} \right)^2 \left( \frac{k_1}{k_2} \right)' \end{aligned}$$

Since  $\alpha$  is a slant helix,  $\frac{k_1}{k_2}$  is constant. Hence, we have

$$\det(N_1', N_1'', N_1''') = 0, k_2 \neq 0.$$

( $\Leftarrow$ ) Suppose that  $\det(N_1', N_1'', N_1''') = 0$ . Then it is clear

that the  $\frac{k_1}{k_2} = \text{const.}$  for being

$$\left( \frac{k_1}{k_2} \right)' = 0.$$

**Theorem 2.3.** Let  $\alpha = \alpha(s)$  be a unit speed curve in  $E^3$ .

Then  $\alpha$  is a slant helix iff

$$\det(N_2', N_2'', N_2''') = 0$$

**Proof.** ( $\Rightarrow$ ) Suppose that  $\frac{k_1}{k_2}$  be constant. From Eq. (1) one can find

$$-N_2' = -k_2 T$$

and

$$\begin{aligned} -N_2'' &= (k_2') T + (k_1 k_2) N_1 + (k_1 k_2) N_2, \\ -N_2''' &= (k_2'' - k_1^2 k_2 - k_2^3) T \\ &\quad + (2k_1 k_2' + k_1' k_2) N_1 + (3k_2 k_2') N_2. \end{aligned}$$

Moreover, we have

$$\det(N'_2, N''_2, N'''_2) = -k_2^2 \begin{bmatrix} 1 & 0 & 0 \\ * & k_1 & k_2 \\ \circ & 2k_1k'_2 + k'_1k_2 & 3k_2k'_2 \end{bmatrix}$$

$$= k_2^5 \left( \frac{k_1}{k_2} \right)'.$$

Since  $\alpha$  is a slant helix curve  $\frac{k_1}{k_2}$  is constant. Hence, we have

$$\det(N'_2, N''_2, N'''_2) = 0$$

( $\Leftarrow$ ): Suppose that  $\det(N'_2, N''_2, N'''_2) = 0$ . Then it is clear

that the  $\frac{k_1}{k_2} = \text{const.}$  for being

$$\left( \frac{k_1}{k_2} \right)' = 0.$$

Next we consider general slant helices in a Euclidean manifold  $M$ . Then we have equalities

$$\alpha'(s) = T$$

$$D_T T = k_1 N_1 + k_2 N_2$$

$$D_T N_1 = -k_1 T$$

$$D_T N_2 = -k_2 T,$$

for any  $s \in I$ , where  $N_1(s)$  and  $N_2(s)$  are vector fields and  $k_1$  and  $k_2$  are functions of parameter  $s$ .

**Theorem 2.4.** A unit speed curve  $\alpha$  on  $M$  is a general slant helix iff

$$D_T(D_T D_T N_1) = -A D_T N_1 - 3k'_1 D_T T \quad (2)$$

where

$$A = \kappa^2 - \frac{k_1''}{k_1}, k_1^2 + k_2^2 = \kappa^2. \quad (3)$$

**Proof.** Suppose that  $\alpha$  is general slant helix. Then, from Eq. (2), we have

$$D_T(D_T N_1) = D_T(-k_1 T) = -k'_1 T - k_1 D_T T$$

$$= -k'_1 T - k_1^2 N_1 - k_1 k_2 N_2 \quad (4)$$

and

$$D_T(D_T D_T N_1) = (-k_1'' + k_1 k_2^2) T - k_1^2 D_T N_1$$

$$- 2k_1 k'_1 N_1 - 3k'_1 D_T T$$

$$- (k'_1 k_2 - k_1 k'_2) N_2 - k'_1 D_T T. \quad (5)$$

Now, since  $\alpha$  is a general slant helix, we have

$$\frac{k_1}{k_2} = \text{const.}$$

and this upon the derivation give rise to

$$k'_1 k_2 = k_1 k'_2.$$

If we substitute the values

$$T = -\frac{1}{k_1} D_T N_1 \quad (6)$$

and

$$(k_1 k_2)' = 2k'_1 k_2,$$

in Eq.(2.4) we obtain

$$D_T(D_T D_T N_1) = \left( \frac{k_1''}{k_1} - \kappa^2 \right) D_T N_1 - 3k'_1 D_T T.$$

$$D_T(D_T D_T N_1) = \left( \frac{k_1''}{k_1} - \kappa^2 \right) D_T N_1 - 3k'_1 D_T T.$$

So we get as desired.

Conversely let us assume that Eq. (2) holds. We show that the curve  $\alpha$  is general slant helix. Differentiating covariantly Eq. (6) we obtain

$$D_T T = D_T \left( -\frac{1}{k_1} D_T N_1 \right)$$

$$= \frac{k'_1}{k_1^2} D_T N_1 - \frac{1}{k_1} D_T D_T N_1$$

and so,

$$D_T D_T T = \left( \frac{k'_1}{k_1^2} \right)' D_T N_1 + \frac{k'_1}{k_1^2} D_T D_T N_1$$

$$+ \frac{k'_1}{k_1^2} D_T D_T N_1 - \frac{1}{k_1} D_T D_T D_T N_1 \quad (7)$$

If we use Eq. (2) in Eq. (7), we get

$$D_T D_T T = \left[ \left( \frac{k'_1}{k_1^2} \right)' + \frac{A}{k_1} \right] D_T N_1 + \frac{2k'_1}{k_1^2} D_T D_T N_1$$

$$+ \frac{3k'_1}{k_1} D_T T_1$$

Substituting Eq. (4) and Eq. (5) in this last equality we obtain

$$D_T D_T T = \left[ \left( \frac{k'_1}{k_1^2} \right)' + \frac{A}{k_1} \right] D_T N_1 - \frac{2k_1^2 k'_1}{k_1^2} T -$$

$$- 2k'_1 N_1 - \frac{2k'_1 k_2}{k_1} N_2 + 3k'_1 N_1 + \frac{3k'_1 k_2}{k_1} N_2.$$

From the last equality we have

$$D_T D_T T = \left[ \left( \frac{k_1'}{k_1^2} \right)' + \frac{A}{k_1} \right] D_T N_1 - \frac{2k_1'^2}{k_1^2} T + k_1' N_1 + \frac{k_1' k_2'}{k_1} N_2. \quad (8)$$

On the other hand we can write  $D_T D_T T$  as follows

$$D_T D_T T = k_1 D_T N_1 - k_2'^2 T + k_1' N_1 + k_2' N_2. \quad (9)$$

From comparison the Eq. (8) and Eq. (9) we obtain equalities below

$$\frac{k_1' k_2'}{k_1} = k_2'$$

and so

$$\frac{k_1'}{k_1} = \frac{k_2'}{k_2}. \quad (10)$$

Integrating Eq. (10), we get

$$\frac{k_1}{k_2} = \text{const.}$$

Thus  $\alpha$  is a general slant helix. Hence, the proof is done.

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