# Precision Assessment of the Orthometric Heights Determination in the Northern Part of Libya 

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#### Abstract

The Global Positioning System (GPS), satellite-based technology, has been utilized extensively in the last few years in a wide range of Geometrics and Geographic Information Systems' (GIS) applications. One of the main challenges dealing with GPSbased heights consists of converting them into Mean Sea Level (MSL) heights, which is used in surveys and mapping.

In this research's work, differences in heights of 50 points, in northern part of Libya has been carried out by using both ordinary leveling (in which Geoid is the reference datum) and GPS techniques (in which Ellipsoid is the reference datum). In addition, this study utilized the EGM2008 model to obtain the undulation values between the ellipsoidal and orthometric heights. From these values of ellipsoidal heights can be obtained from GPS observations to compute the orthomteric heights. This research presents a suitable alternative, from an economical point of view, to substitute the expensive traditional leveling technique, particularly, for topographic mapping.


Keywords-Geoid undulation, GPS, ordinary and geodetic leveling, orthometric height.

## I. INTRODUCTION

THE Number of quantities has to be measured in usual survey's works. These quantities may be bearings, angles, or distances (horizontal, vertical or inclined). Reduction of these values leads to points' determination, relative position.

Leveling is the name had been given to the process of measuring the difference in elevation between two or more points. The heights of points relative to a chosen surface are known as the reduced levels of these points. Reference surface is usually known as a datum. Leveling has many applications in engineering surveying that used in all stages of construction projects from the initial site survey to the final setting out [5].

Leveling process can be carried out by using different equipments and techniques of survey. It may be precise; when precise optical or digital levels had been used, or it may be ordinary; upon using ordinary optical, automatic or digital levels. Moreover it could be carried out trigonometrically or barometrically.

## II. ORdinary and Geodetic Leveling

For short distances, the difference in level between two points can easily be determined by setting a staff vertically in each point and then constructing a horizontal line by using

[^0]optical or digital level. The difference in the intersection points, of the horizontal line with both staves, produces the difference in level between these ground points Fig. 1. This technique is known as ordinary leveling [9].
For long distances, considering geoid undulation of the earth, direct leveling doesn't solve the problem and it will be more complicated. This is so because horizontal line doesn't solve the problem directly. Leveling technique, taking the geoid undulation into account, is usually known as geodetic leveling.


Fig. 1 Ordinary leveling

## III. Overview of GPS

GPS is a satellite navigation system established by the United State Department of Defense (DoD), designed to provide 3 -dimensional positioning, velocity, and time information, regardless of the weather, at any time and almost anywhere on the globe. There are at least 24 GPS satellites in 6 orbital planes, each satellite transmits two signals continuously, which are created from a fundamental signal (frequency $=10.15 \mathrm{MHz}$ ), driven by the GPS satellite's atomic clock. The initial frequencies are L1 and L2. The L1 carrier signal is formed by multiplying the fundamental signal by 154 (frequency $=1575.42 \mathrm{MHz}$, wavelength 19.0 cm ). The L2 carrier signal is formed by multiplying the fundamental signal by 120 (frequency $=1227.60 \mathrm{MHz}$, wavelength 24.0 cm ). The L2 signal is used for calibration of signal delay due to the Earth's ionosphere [3]. Additionally, the new civil GPS signals have been developed for different purposes. These signals are L2C, L5 and L1 [6]. Table I shows main information of these signals.

TABLE I
New GPS SiGNALS

| Signal | Benefits | Number of satellites <br> broadcasting now | Availability <br> on 24 satellites |
| :---: | :---: | :---: | :---: |
| L2C | Meets commercial needs <br> for ionosphiric <br> correction | 10 | $\sim 2018$ |
| L5 | Meets requirements for <br> safety of life | 3 | $\sim 2021$ |
|  | transportation <br> GNSS interoperability; <br> performance | Begins lunching in | $\sim 2026$ |

## IV. ElLipsoid and Geoid

The geoid is a surface of constant potential energy that coincides with the mean sea level over the oceans. This definition is not very rigorous. Firstly, mean sea level is not quite a surface of constant potential due to dynamic processes within the ocean. Secondly, the actual equipotential surface under continents is warped by the gravitational attraction of the overlying mass. But geodesists define the geoid as though that mass were always underneath the geoid instead of being above it. The main function of the geoid in geodesy is to serve as a reference surface for leveling. The elevation, measured by leveling, is relative to the geoid.

Regular shape could be approximated by the Ellipsoid. Ellipsoid is a mathematical surface obtained by revolving an ellipse at about its minor axis. Leveling, based on taking the geoid as a reference datum, is then termed geodetic leveling. The dimensions of the ellipse are selected to give the best fit of the ellipsoid to the geoid over a large area, and are based upon surveys made in the area.

The two-dimensional views, which illustrate conceptually the geoid and ellipsoid, are shown in Fig. 2. As illustrated, the geoid contains non uniform undulations, and therefore it's not readily defined mathematically. Ellipsoids, which approximate the geoid and can be defined mathematically, are therefore used to compute positions of widely spaced points that are located.

$h=e l i p s o i d$ height
$\mathrm{H}=$ orthometric height
$\mathrm{N}=$ geoid height
Fig. 2 Geoid and ellipsoid surfaces

## V. Previous Libyan Ellipsoid and Geiod

## A. Libyan Ellipsoid

The Libyan first datum, defined for geodetic network and mapping, is ELD79 based on Hayford International Ellipsoid $1924(a=6378388, f=1 / 297)$. In the 1980's, Libya established a Doppler network, which was initially defined in the WGS-72 datum and then in the International Terrestrial Reference Frame 2000 (ITRF00) datum. Surveying Department of Libya (SDL), later introduced LGD2006, again based on Hayford International ellipsoid $1924(\mathrm{a}=6378388, \mathrm{f}=1 / 297)$.

For this purpose, some of 61 stations were GPS surveyed in 2006 and tied to IGS stations (Epoch: 2006.3822). Thus, precise coordinates were determined in the ITRF00 datum, based on GRS80 ellipsoid $(a=6378137.0 \mathrm{~m}$, $\mathrm{f}=1 / 298.25722101$ ) [8].

## B. Libyan Geoid

Two practical attempts had been tried to compute the Libyan geoid [1]. None of these attempts are included the usage of gravimetric data. The used data and the computation methods are concisely summarized in this section. The plotted results of these two attempts are also provided as below:
1- A geoid map, based on 19 leveled Doppler points, was computed by IGN for the benefit of the Surveying Department of Libya. In its computation, IGN had been used as the only source of data, the deflections of the vertical, which obtained from the comparison of the astronomical coordinates and their respective WGS 72 to the leveled Doppler points above, the same ellipsoid. Observation relations, linking the undulations of the geoid to the ones directly obtained from subtracting the orthometric height from the ellipsoidal height, were formed. A geoid computation program called GEOIDE that solves the system of normal equations and predicts the geoid undulations, was used. From the result of these computations, IGN drew the map of Libyan geoidal undulations [4] (see Fig. 3).
2- A second geoid map was computed by an American company called the Aero-Service Corporation (ASC). Two geoid maps, with relation to two different datums , were computed: one with relation to the local ELD79 datum (see Fig. 4), and the other with relation to WGS 72 datum (see Fig. 5) [2]. In its method, the company used a modal, generated from comparing the vertical deflections differences of each the available 155 Laplace point from all other Laplace points within 1.5 weighted least squares solution considered at IGN stations (see above), where the undulations, considered to be known, were obtained the weight of each observation was taken as inversely proportional to the linear separation between the station.


Fig. 3 IGN Libyan geoid undulation map (WGS72 datum)


Fig. 4 ASC Libyan geoid undulation map (ELD79 datum)


Fig. 5 ASC Libyan geoid undulation map (WGS72 datum)

## VI. The EGM2008 Geopotential Model

The U.S. National Geospatial-Intelligence Agency (NGA) has released publicly in mid 2008. This gravitational model be completed to spherical harmonic degree and order 2159, contains additional coefficients extending to degree 2190 and order 2159. The WGS 84 constants are used to define the reference ellipsoid and the associated normal gravity field, to which the geoid undulations are referenced as follow:

- $a=6378137.00 \mathrm{~m}$ (semi-major axis of WGS 84 ellipsoid),
- $\mathrm{f}=1 / 298.257223563$ (flattening of WGS 84 ellipsoid),
- $\mathrm{GM}=3.986004418 \times 1014 \mathrm{~m} 3 \mathrm{~s}-2$ (Product of the Earth's mass and the Gravitational Constant),
- $\quad \omega=7292115 \times 10-11$ radians/sec (Earth's angular velocity).
All synthesis software, coefficients and pre-computed geoid grids assume a tide free system, as far as permanent tide is concerned [7].


Fig. 6 Gravitational Model EGM2008

## VII. MEASUREMENTS AND Results

In this research's work, ordinary leveling was carried out for 50 points in northern part of Libya. Automatic level had been used to do the job. Level line was started at a known benchmark and end at another one. Observations had been reduced and adjusted. Orthometric heights (H) were obtained on Libyan reference datum. GPS observations were carried out along the same line. Observations had been processed and adjusted to compute ellipsoidal height (h) of all points. Comparison between orthometric height of points and ellipsoidal heights of the same points, can be carried out by computing the undulation ( N ) between both results as shown in Table II. These differences represent the geoid ellipsoid separation in the area.

TABLE II
Geiod Ellipsiod Separation (N)

| Point No. | $\begin{aligned} & \text { Ellipsoid height (h) } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{gathered} \hline \hline \text { Orthometric } \\ \text { height }(\mathrm{H})(\mathrm{m}) \end{gathered}$ | $\begin{aligned} & \hline \hline \text { Undulation } \\ & \mathrm{N}=\mathrm{h}-\mathrm{H}(\mathrm{~m}) \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1 | 61.615 | 33.394 | 28.221 |
| 2 | 66.155 | 37.884 | 28.271 |
| 3 | 87.859 | 59.541 | 28.318 |
| 4 | 44.589 | 16.098 | 28.491 |
| 5 | 45.125 | 16.896 | 28.229 |
| 6 | 39.1 | 10.964 | 28.136 |
| 7 | 68.873 | 40.822 | 28.051 |
| 8 | 37.573 | 9.628 | 27.945 |
| 9 | 37.409 | 9.586 | 27.823 |
| 10 | 45.052 | 17.338 | 27.714 |
| 11 | 28.954 | 1.356 | 27.598 |
| 12 | 34.299 | 6.814 | 27.485 |
| 13 | 37.925 | 10.561 | 27.364 |
| 14 | 41.553 | 14.334 | 27.219 |
| 15 | 39.187 | 12.214 | 26.973 |
| 16 | 40.969 | 14.122 | 26.847 |
| 17 | 34.521 | 8.022 | 26.499 |
| 18 | 27.475 | 1.001 | 26.474 |
| 19 | 43.508 | 17.027 | 26.481 |
| 20 | 53.396 | 27.037 | 26.359 |
| 21 | 56.474 | 30.117 | 26.357 |
| 22 | 26.702 | 0.414 | 26.288 |
| 23 | 42.656 | 16.429 | 26.227 |
| 24 | 44.857 | 18.637 | 26.22 |
| 25 | 25.545 | -0.705 | 26.25 |
| 26 | 47.947 | 21.674 | 26.273 |
| 27 | 25.407 | -0.868 | 26.275 |
| 28 | 41.539 | 15.341 | 26.198 |
| 29 | 30.622 | 4.403 | 26.219 |
| 30 | 21.776 | -3.33 | 25.106 |
| 31 | 24.048 | -2.272 | 26.32 |
| 32 | 23.954 | -2.431 | 26.385 |
| 33 | 52.214 | 25.651 | 26.563 |
| 34 | 45.777 | 19.06 | 26.717 |
| 35 | 36.301 | 8.44 | 27.861 |
| 36 | 33.468 | 6.473 | 26.995 |
| 37 | 43.846 | 16.787 | 27.059 |
| 38 | 53.269 | 26.052 | 27.217 |
| 39 | 43.963 | 16.527 | 27.436 |
| 40 | 50.049 | 22.419 | 27.63 |
| 41 | 56.033 | 28.224 | 27.809 |
| 42 | 57.92 | 29.953 | 27.967 |
| 43 | 43.573 | 15.318 | 28.255 |
| 44 | 46.379 | 17.944 | 28.435 |
| 45 | 32.694 | 4.09 | 28.604 |
| 46 | 64.241 | 35.437 | 28.804 |
| 47 | 61.329 | 32.367 | 28.962 |
| 48 | 43.033 | 14.037 | 28.996 |
| 49 | 41.806 | 12.581 | 29.225 |
| 50 | 51.68 | 22.234 | 29.446 |

Practically, ellipsoidal heights can be reduced to orthometric heights, if geoid ellipsoid separation (N) is known. In this work, EGM2008 geodetic model was used to compute geoid ellipsoid separation (undulation). Reduced geoid undulations for the observed points are listed in Table III.

TABLE III
Reduced EGM2008 Geiod Elliposoid Separation (n)

| Point No. | Latitude |  |  | Longitude |  |  | $\begin{gathered} \text { EGM2008 (N) } \\ \mathrm{m} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | - | , | " | - | , | " |  |
| 1 | 30 | 51 | 29.692 | 17 | 50 | 10.028 | 28.559 |
| 2 | 30 | 49 | 58.673 | 17 | 55 | 23.937 | 28.614 |
| 3 | 30 | 48 | 10.548 | 18 | 3 | 12.222 | 28.621 |
| 4 | 30 | 46 | 36.144 | 18 | 7 | 50.176 | 28.574 |
| 5 | 30 | 44 | 31.639 | 18 | 12 | 5.973 | 28.55 |
| 6 | 30 | 41 | 25.325 | 18 | 14 | 59.211 | 28.496 |
| 7 | 30 | 37 | 52.07 | 18 | 18 | 21.17 | 28.388 |
| 8 | 30 | 34 | 53.268 | 18 | 24 | 44.099 | 28.199 |
| 9 | 30 | 31 | 30.841 | 18 | 29 | 40.448 | 28.07 |
| 10 | 30 | 28 | 19.84 | 18 | 33 | 0.3996 | 27.968 |
| 11 | 30 | 23 | 51.456 | 18 | 38 | 0.5252 | 27.808 |
| 12 | 30 | 21 | 7.3842 | 18 | 43 | 34.214 | 27.667 |
| 13 | 30 | 19 | 32.803 | 18 | 48 | 27.402 | 27.554 |
| 14 | 30 | 17 | 41.672 | 18 | 54 | 19.479 | 27.394 |
| 15 | 30 | 14 | 36.803 | 18 | 59 | 54.007 | 27.184 |
| 16 | 30 | 14 | 10.335 | 19 | 4 | 24.513 | 27.068 |
| 17 | 30 | 14 | 16.709 | 19 | 8 | 50.72 | 26.953 |
| 18 | 30 | 14 | 58.808 | 19 | 14 | 34.88 | 26.836 |
| 19 | 30 | 15 | 16.165 | 19 | 20 | 32.67 | 26.73 |
| 20 | 30 | 16 | 3.8092 | 19 | 26 | 38.396 | 26.604 |
| 21 | 30 | 16 | 0.8909 | 19 | 26 | 44.251 | 26.602 |
| 22 | 30 | 19 | 22.739 | 19 | 30 | 20.854 | 26.558 |
| 23 | 30 | 22 | 14.979 | 19 | 35 | 5.8542 | 26.51 |
| 24 | 30 | 24 | 35.576 | 19 | 40 | 19.721 | 26.5 |
| 25 | 30 | 26 | 40.087 | 19 | 45 | 30.756 | 26.555 |
| 26 | 30 | 24 | 52.447 | 19 | 49 | 59.427 | 26.532 |
| 27 | 30 | 28 | 26.127 | 19 | 55 | 10.322 | 26.518 |
| 28 | 30 | 30 | 51.757 | 20 | 0 | 17.532 | 26.475 |
| 29 | 30 | 34 | 3.7792 | 20 | 4 | 48.96 | 26.453 |
| 30 | 30 | 36 | 0.5795 | 20 | 6 | 47.5 | 26.445 |
| 31 | 30 | 40 | 10.148 | 20 | 10 | 0.7958 | 26.516 |
| 32 | 30 | 42 | 22.292 | 20 | 11 | 30.135 | 26.575 |
| 33 | 30 | 46 | 59.044 | 20 | 16 | 11.233 | 26.748 |
| 34 | 30 | 51 | 30.405 | 20 | 14 | 16.114 | 26.891 |
| 35 | 30 | 55 | 50.756 | 20 | 11 | 13.98 | 27.049 |
| 36 | 30 | 58 | 42.276 | 20 | 11 | 6.4954 | 27.146 |
| 37 | 31 | 2 | 28.56 | 20 | 12 | 46.662 | 27.265 |
| 38 | 31 | 6 | 31.2 | 20 | 14 | 1.2283 | 27.374 |
| 39 | 31 | 12 | 43.531 | 20 | 14 | 14.97 | 27.575 |
| 40 | 31 | 17 | 58.601 | 20 | 13 | 5.2596 | 27.762 |
| 41 | 31 | 22 | 24.836 | 20 | 11 | 19.442 | 27.939 |
| 42 | 31 | 27 | 42.459 | 20 | 9 | 24.568 | 28.164 |
| 43 | 31 | 32 | 14.802 | 20 | 4 | 47.472 | 28.324 |
| 44 | 31 | 38 | 1.2252 | 20 | 1 | 42.487 | 28.544 |
| 45 | 31 | 42 | 12.595 | 19 | 57 | 36.465 | 28.651 |
| 46 | 31 | 46 | 39.198 | 20 | 1 | 0.0107 | 28.852 |
| 47 | 31 | 51 | 34.659 | 20 | 1 | 2.161 | 29.018 |
| 48 | 31 | 56 | 0.208 | 19 | 58 | 8.0644 | 29.087 |
| 49 | 32 | 0 | 56.727 | 20 | 3 | 6.2773 | 29.373 |
| 50 | 32 | 3 | 15.747 | 20 | 6 | 33.715 | 29.58 |

From the obtained results, the average separation can be computed to be 27.588 m . Ortometric heights are then calculated by adding geodetic heights $(\mathrm{H})$ to geoid separation $(\mathrm{N})$ by using the following equation:

$$
\begin{equation*}
\mathrm{N}=\mathrm{H}-\mathrm{h} \tag{1}
\end{equation*}
$$

$$
\begin{equation*}
\text { or } \mathrm{H}=\mathrm{N}+\mathrm{h} \tag{2}
\end{equation*}
$$

where, $H$ represents orthometric height, $h$ represents Ellipsoidal height, $N$ represents geoid ellipsoid undulation.

Computed orhtometric heights, obtained by using (2) and Table III and then compared with actual ortometric heights Table IV, shows the difference between computed heights and actual ortometric heights.

TABLE IV
Difference Between Computed and Actual Orthometric Heights

| Point No. | Computed ortometric $\operatorname{height}(\mathrm{H})(\mathrm{m})$ | Actual ortometric height(H) (m) | Difference |
| :---: | :---: | :---: | :---: |
| 1 | 33.056 | 33.394 | 0.338 |
| 2 | 37.541 | 37.884 | 0.343 |
| 3 | 59.238 | 59.541 | 0.303 |
| 4 | 16.015 | 16.098 | 0.083 |
| 5 | 16.575 | 16.896 | 0.321 |
| 6 | 10.604 | 10.964 | 0.36 |
| 7 | 40.485 | 40.822 | 0.337 |
| 8 | 9.374 | 9.628 | 0.254 |
| 9 | 9.339 | 9.586 | 0.247 |
| 10 | 17.084 | 17.338 | 0.254 |
| 11 | 1.146 | 1.356 | 0.21 |
| 12 | 6.632 | 6.814 | 0.182 |
| 13 | 10.371 | 10.561 | 0.19 |
| 14 | 14.159 | 14.334 | 0.175 |
| 15 | 12.003 | 12.214 | 0.211 |
| 16 | 13.901 | 14.122 | 0.221 |
| 17 | 7.568 | 8.022 | 0.454 |
| 18 | 0.639 | 1.001 | 0.362 |
| 19 | 16.778 | 17.027 | 0.249 |
| 20 | 26.792 | 27.037 | 0.245 |
| 21 | 29.872 | 30.117 | 0.245 |
| 22 | 0.144 | 0.414 | 0.27 |
| 23 | 16.146 | 16.429 | 0.283 |
| 24 | 18.357 | 18.637 | 0.28 |
| 25 | -1.01 | -0.705 | 0.305 |
| 26 | 21.415 | 21.674 | 0.259 |
| 27 | -1.111 | -0.868 | 0.243 |
| 28 | 15.064 | 15.341 | 0.277 |
| 29 | 4.169 | 4.403 | 0.234 |
| 30 | -4.669 | -3.33 | 1.339 |
| 31 | -2.468 | -2.272 | 0.196 |
| 32 | -2.621 | -2.431 | 0.19 |
| 33 | 25.466 | 25.651 | 0.185 |
| 34 | 18.886 | 19.06 | 0.174 |
| 35 | 9.252 | 8.44 | -0.812 |
| 36 | 6.322 | 6.473 | 0.151 |
| 37 | 16.581 | 16.787 | 0.206 |
| 38 | 25.895 | 26.052 | 0.157 |
| 39 | 16.388 | 16.527 | 0.139 |
| 40 | 22.287 | 22.419 | 0.132 |
| 41 | 28.094 | 28.224 | 0.13 |
| 42 | 29.756 | 29.953 | 0.197 |
| 43 | 15.249 | 15.318 | 0.069 |
| 44 | 17.835 | 17.944 | 0.109 |
| 45 | 4.043 | 4.09 | 0.047 |
| 46 | 35.389 | 35.437 | 0.048 |
| 47 | 32.311 | 32.367 | 0.056 |
| 48 | 13.946 | 14.037 | 0.091 |
| 49 | 12.433 | 12.581 | 0.148 |
| 50 | 22.1 | 22.234 | 0.134 |
|  | Average Differen |  | 0.216 |
| Root Mean Square Error of Difference $=$ |  |  | 0.233 |

## VIII. CONCLUSION

Referring to the results obtained above and analysis carried out. It could be directly concluded that:

1. Success of direct utilization of GPS observation in leveling depends on the value of geoid ellipsoid separation in the area. This separation was estimated in the study area with around 28 m .
2. Orthometric heights can be reduced from GPS observation by obtaining the geoid ellipsoid separation (geoid undulation) with aid of one of available geoid models. This can easily be done by subtracting resultant undulation from GPS heights.
3. Applying EGM2008 geoid model to GPS observation in our study area, can successfully produces results estimated with 0.216 m accuracy in orthometric heights. This accuracy in heights can be used to produce contour map scales of 1:5000 and smaller according to surveying department of Libya specification.

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## References

[1] A. Swassi, " Geiod determination for Libya" PhD thesis, institute agronomique et Veterinaire Hassan II, 2000
[2] A. S. C., " Final report covering traverse, Doppler and astronomic work", Surveying department of Libya, Tripoli, Libya, 1985.
[3] G. Bewitt," Basic of the GPS Technique: Observation Equations", Swedish Land Survey, 1997.
[4] I.G.N., "Super horizontal control net", surveying department of Libya, Tripoli, Libya, 1979.
[5] J. Uren and W. F. Price, "Surveying for Engineering", 2 ${ }^{\text {nd }}$ Edition, Macmillan education Lt, 1985.
[6] J.Y. Kim, "U. S. GPS program and policy update", International navigation forum, Moscow, Russia, April 2013.
[7] N. Pavlis, "EGM2008-WGS84 version", April 2013, http://earthinfo.nga.mil/GandG/wgs84/gravitymod/egm2008/egm08_wgs84.html.
[8] SDL Surveying Department of Libya "National annual report 2009", Tripoli, Libya, 2009.
[9] W. Irvine, "Surveying for construction", $4^{\text {th }}$ Edition, Macmillan education Lt, 1995.

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