

Mechanical and Morphological Properties of Polypropylene and High Density Polyethylene Matrix Composites Reinforced with Surface Modified Nano Sized TiO₂ Particles

Mirigul Altan, Huseyin Yildirim

Abstract—Plastics occupy wide place in the applications of automotive, electronics and house goods. Especially reinforced plastics become popular because of their high strength besides their advantages of low weight and easy manufacturability. In this study, mechanical and morphological properties of polypropylene (PP) and high density polyethylene (HDPE) matrix composites reinforced with surface modified nano titan dioxide (TiO₂) particles were investigated. Surface modification was made by coating the nano powders with maleic anhydride grafted styrene ethylene butylene styrene (SEBS-g-MA) and silane, respectively. After surface modification, PP/TiO₂ and HDPE/TiO₂ composites were obtained by using twin screw extruder at titan dioxide loading of 1 wt.%, 3 wt.% and 5 wt.%. Effects of surface modification were determined by thermal and morphological analysis. SEBS-g-MA provided bridging effect between TiO₂ particles and polymer matrix while silane was effective as a dispersant. Depending on that, homogenous structures without agglomeration were obtained. Mechanical tests were performed on the injection moldings of the composites for obtaining the impact strength, tensile strength, stress at break, elongation and elastic modulus. Reinforced HDPE and PP moldings gave higher tensile strength and elastic modulus due to the rigid structure of TiO₂. Slight increment was seen in stress at break. Elongation and impact strength decreased due to the stiffness of the nano titan dioxide.

Keywords—High density polyethylene, mechanical properties, nano TiO₂, polypropylene.

I. INTRODUCTION

POLYMERS filled with inorganic nano particles are very important sort of nano composites based on the use of a polymer matrix. They usually combine the advantages of polymer matrix such as low weight, easy formability with the unique characteristics of the inorganic nano particles. This kind of incorporation of the materials makes the nano composites to gain a series of properties such as optical, mechanical, electrical and magnetic. However, there are some

M. Altan is with the Department of Mechanical Engineering, Yildiz Technical University, Yildiz, Istanbul, 34349, Turkey (corresponding author to provide phone: 902123832895; fax: 902122616659; e-mail: meksi@yildiz.edu.tr).

H.Yildirim is with the Department of Chemistry, Yildiz Technical University, Davutpasa, Istanbul,34210 Turkey and Department of Polymer Engineering, University of Yalova, 77100 Yalova, Turkey (e-mail: husyil@yildiz.edu.tr)

disadvantages of nano particles like agglomeration followed by insufficient dispersion in the polymer matrix. This result generally leads poor optical and mechanical properties [1]-[2]. In order to obtain a homogenous structure, dispersants and some coupling agents are being used. Another problem studying with nano materials is the decreasing of the impact strength due to the stiffness of the inorganic material. Researchers use elastomeric materials such as styrene-ethylene-butylene-styrene (SEBS), ethylene-propylene rubber (EPR) and ethylene-propylene diene monomer elastomer (EPDM) to increase the toughness of the composites [3]. Polypropylene (PP) and high density polyethylene (HDPE) are commonly used polymers. Especially, polypropylene with high modulus and impact strength is desirable for many industrial applications. Titan dioxide, one of the inorganic materials with high mechanical strengths, is used as reinforcement material for polymers. However, it has polar surface while polymer matrix is non polar which makes the surface adhesion between the matrix and titan dioxide poor. The surface adhesion can be enhanced by the compatibilizers and coupling agents. Maleic anhydride grafted SEBS acts as impact modifier and compatibilizer for these kind of composites. [4]-[5]. Especially, it is used with polypropylene or high density polyethylene as coupling agent due to its compatible structure with olefinic block [6].

In this work, modified nano TiO₂ particles with SEBS-g-MA and silane were used for preparing polypropylene and high density polyethylene matrix composites. Thermal, morphological studies were done on the composites and mechanical tests were applied on the injection moldings of reinforced PP and HDPE. Effects of modified nano TiO₂ reinforcement on the mechanical and morphological properties were discussed.

II. EXPERIMENTAL STUDY

A. Materials

Polymer materials used in this study were polypropylene copolymer (56M10, Sabic Company) with melt flow index of 6.2 g/10 min, density of 0.902 kg/cm³ and high density polyethylene (Lanufene, HDI- 6507UV) with melt flow index

of 7.5g/10 min and density of 0.965 kg/cm³. Nano material was TiO₂ (Nabond Company, China). SEBS-g-MA (FG1901X, Kraton, Shell Company) and vinyl trimethoxysilane (VTMS, Aldrich) were used for the surface modification of the nano TiO₂ particles.

B. Modification and Characterization of the Nano Powders

The nano titan dioxide particles were modified by coating them with SEBS-g-MA and then silane, respectively. SEBS-g-MA was used as compatibilizer and by coating the powders with it, the coupling agent property of the SEBS-g-MA was thought to be more effective. In this regard, 3 g SEBS-g-MA was dissolved in 200 g toluene in 48 hours at 25 °C. Then, 100 g nano TiO₂ was added slowly and mixed with a mechanical mixer (IKA RW 20 digital) for 3 hours. SEBS-g-MA coated nano powders were pulverized after drying the mixture at 50 °C for 8 hours. Then, a new solution was prepared for silane coating with 96% absolute alcohol and 4% distilled water with 1% silane. This solution was mixed for 10 minutes with the mechanical mixer and 100 g SEBS-g-MA coated nano TiO₂ particles was added slowly and mixed for 3 hours. The mixture was dried at 50 °C for 8 hours and pulverized continuously. The aim of silane coating was to disperse SEBS-g-MA coated nano particles better in the matrix.

The coated powders were analyzed by scanning electron microscope (SEM) JEOL JSM-5910 LV and energy dispersive spectroscopy (EDS).

C. Blending

The chemical composition of the blends and their coded names are given in Table I. The dried powders and the polymer were loaded into a twin screw extruder (Rondol MicroLab, England) with L/D ratio of 20. The operation temperature was set as 220, 200, 180, 120 and 75 °C. The speed of the screw was 60 rpm. The extrudate strands were granulized and dried at 80° C under vacuum for two hours.

TABLE I
COMPOSITION OF THE BLENDS

Material	Ratio of TiO ₂ (wt %)
Original PP	0
Original HDPE	0
PP/1TiO ₂	1
PP/3TiO ₂	3
PP/5TiO ₂	5
HDPE/1TiO ₂	1
HDPE/3TiO ₂	3
HDPE/5TiO ₂	5

D. Differential Scanning Calorimetry (DSC)

The melting and crystallization behaviors were studied by differential scanning calorimetry (DSC, Perkin Elmer DSC-7) in nitrogen atmosphere. The samples (4-5 mg) were heated from 40 °C to 180 °C at 10 °C/min and held at 180 °C for 5 min and then cooled back to 40 °C at 10 °C/min and held 5 min at 40 °C. Then, second heating cycle was performed to delete the thermal history of the samples. The melting temperature (T_m), crystallization temperature (T_c) and degree of the crystallization (X_c) were obtained. The fusion enthalpy of 100 % crystalline phase of PP and HDPE were taken as 209 J/g and 290 J/g in calculating the degree of the crystallization of the blends, respectively [7].

E. Injection Molding

The dried granules of the composites were injection molded with a 40 tone injection molding machine. Tensile test and impact test specimens were obtained for mechanical tests. The mold temperature was 40 °C, injection pressure was 65 MPa, holding pressure 45 MPa, holding time 15 s and cooling time was taken as 10 s.

F. Mechanical Characterization

Tensile test was carried out by universal tensile machine (Zwick Z010) at room temperature according to ISO 527. The speed of the cross head was 50 mm/min. The izod impact test was performed on the notched specimens by using a 5.4 J pendulum hammer on the Zwick Impact test machine according to ISO 180.

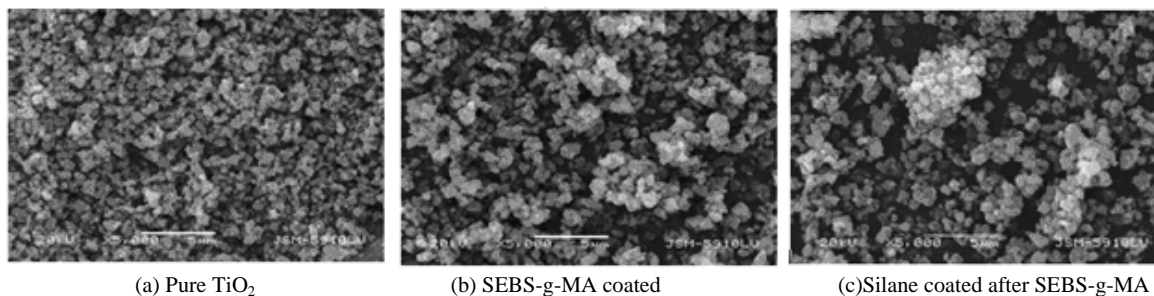
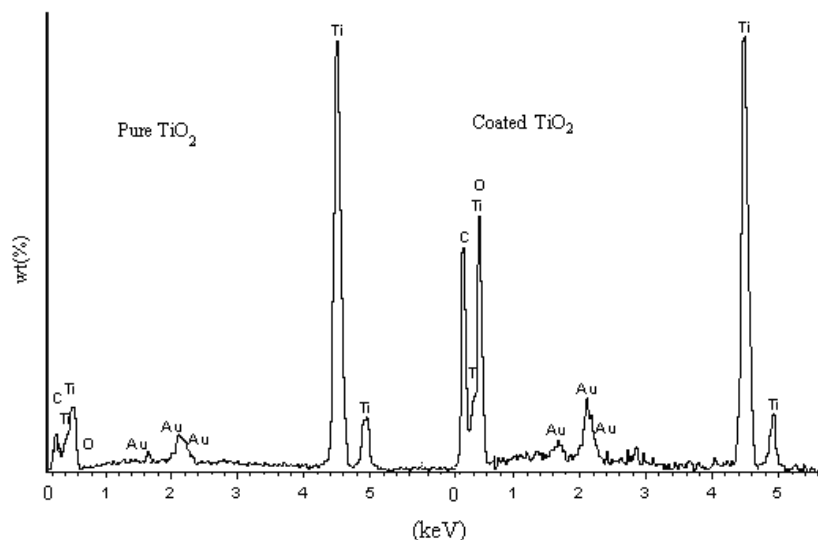
G. Scanning Electron Microscope (SEM)

Morphology of the fracture surface of the each specimen was analyzed by scanning electron microscope (JEOL JSM-5910 LV). The fracture surfaces obtained from the impact tests were etched with tetrahydrofuran (THF) and then washed with acetone and dried under vacuum. Finally, all the specimens were coated with gold.

III. RESULTS AND DISCUSSION

A. Characterization of the powders

The SEM images of the original and coated titan dioxide particles are given in Fig.1. The EDS results are given in Fig. 2. The increments in carbon and oxygen peaks of the coated particles are obvious which is related to the coating with SEBS-g-MA and silane.

Fig. 1 SEM images of the coated TiO₂ powdersFig. 2 EDS results of the pure and coated nano TiO₂ particles

B. Thermal Characterization

The DSC results of the composites are given in Table II and DSC cooling scans of the composites are given in Fig. 3. Melt temperature of the PP matrix composites did not change very much with the addition of TiO₂ which indicates that TiO₂ particles did not influence the stability of the PP. On the other hand, the crystallization temperature and degree of crystallinity of these composites decreased slightly due to the retarding effect of the titan dioxide on PP crystals and physical hindrance of TiO₂ particles to the motion of polymer molecular chains. For HDPE matrix composites, the melt temperature and the crystallization temperature did not change very much by the addition of the TiO₂ particles as given in Table II. However, increase in degree of crystallinity was seen about 25-30 % for HDPE/TiO₂ composites. This increment was probably due to the nucleating agent effect of

the TiO₂ as seen in some earlier studies on similar inorganic fillers used with polyethylene [8]-[9]. Also, the presence of the SEBS-g-MA might favor the crystallization of the HDPE.

TABLE II
THERMAL PROPERTIES OF THE BLENDS

Blend	T _m (°C)	T _c (°C)	Enthalpy (J/g)	X _c (%)
Original PP	166,3	124,9	85,4	40,86
PP/1 TiO ₂	165,8	122,9	82,7	39,57
PP/3 TiO ₂	166,1	124,5	81,2	38,85
PP/5 TiO ₂	166,5	125,1	83,1	39,76
Original HDPE	136,1	118,2	171	58,97
HDPE/1 TiO ₂	136,5	118	219	75,52
HDPE/3 TiO ₂	136,6	117,8	212	73,10
HDPE/5 TiO ₂	134	118,1	208	71,72

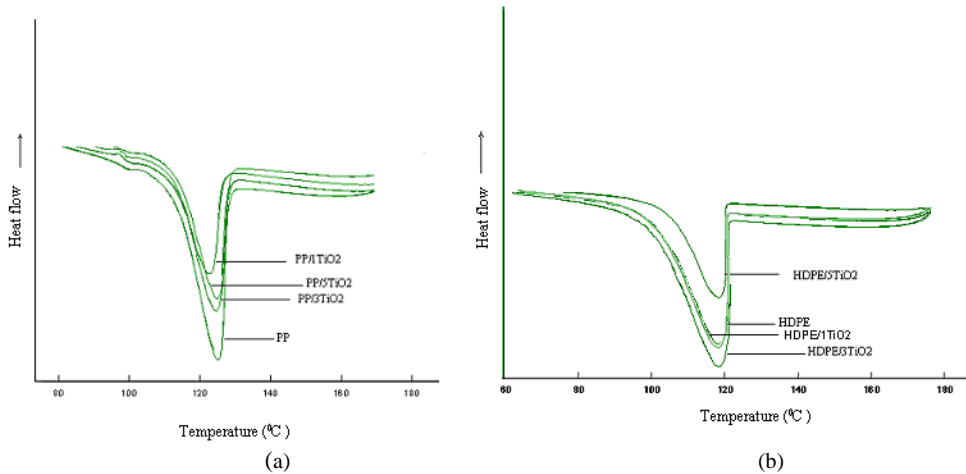


Fig. 3 DSC cooling scans of the TiO₂ reinforced PP (a) and HDPE (b) composites

C. Mechanical Properties

It is known that inorganic nano particles improve the mechanical properties of the polymers [2]-[10]. Generally tensile strength, elastic modulus, stress at break increase while impact strength and elongation decrease. The mechanical properties obtained from tensile test are given in Fig. 4. Tensile strength of both polymers increased while elongation reduced because of the hardness of TiO₂ (Fig. 4a). Stress at break for all the compositions except HDPE/1TiO₂ increased slightly (Fig. 4b).

For HDPE/1TiO₂, SEBS-g-MA was found more effective than in other compositions because elongation of this composition was higher than the original HDPE as seen in Fig. 4(c). This result was also compatible with the results of lower tensile strength and stress at break. Elastic modulus of PP matrix composites increased parallel with the addition of the TiO₂ while HDPE was not affected that much (Fig. 4d).

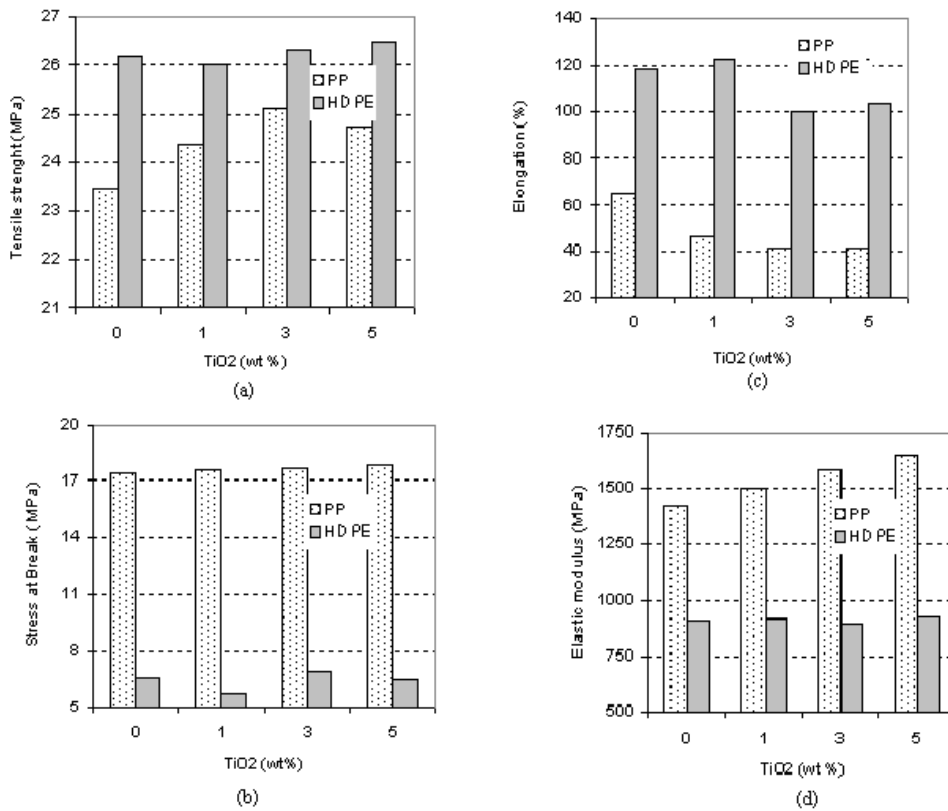


Fig. 4 Mechanical properties of nano TiO₂ reinforced PP and HDPE injection moldings obtained from tensile test

The results of the impact strength are given in Fig. 5. The main problem about nano composites is the reduction of the toughness [3]-[11]. Some researchers used elastomeric materials to increase the impact strength of rigid and stiff structure of the reinforced polymers [12]-[13]. In this study, very small amount of SEBS-g-MA was used for better surface adhesion between TiO_2 and polymer matrix. Therefore, an apparent increase in impact strength was not observed but the elastomeric nature of the SEBS was probably effective in

minimizing the reduction of the impact strength. As a consequence, impact strength reduced according to the increment of TiO_2 ratio (Fig. 5). The decrease in the impact strength of the HDPE composites was higher than that of PP, probably due to the increased degree of crystallinity parallel with the addition of TiO_2 .

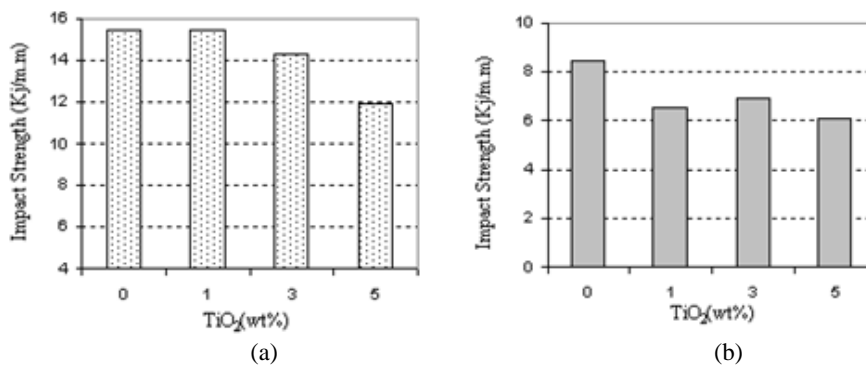


Fig. 5 Impact strength of nano TiO_2 reinforced PP (a) and HDPE (b) injection moldings

D. Morphology

The SEM images of the fracture surfaces of PP/ TiO_2 and HDPE/ TiO_2 are given in Fig. 6 and Fig. 7. The bridging effect between the polymer and nano particle is provided by SEBS-g-MA. The high polarity of the MA group of SEBS-g-MA enhanced the compability between the filler and the polymer matrix. The interface between the polymer matrix and SEBS is strong due to the compatibility of their phases because SEBS could diffuse into the polymer under the formation of miscelles [6]. However, the interaction between TiO_2 and matrix is limited because TiO_2 has polar surface and polymer is non polar. The SEM photographs of the PP given in Fig. 6 indicate strong bonding developed between TiO_2 and PP. TiO_2 particles are almost dispersed in the matrix and they behave like one phase which shows the good compatibility of the two materials.

This chemical bonding is due to the fact that MA functional groups grafted to the ethylene butylenes (EB) mid block of SEBS. Then, it becomes easier for the molecular chains of SEBS-g-MA and the polymer to bond with TiO_2 . Besides, the surface energy of the SEBS-g-MA coated TiO_2 is higher than that of polymer matrix. In order to reduce the surface energy difference, silane coating was applied. Final chemical bonding was resulted in the reactions of the methoxy groups of the silane with the polymer matrix and hydroxyl groups with SEBS-g-MA coated TiO_2 . For HDPE matrix composites, chemical bonding of TiO_2 and HDPE can be seen by the HDPE covering of the individual TiO_2 surface in Fig. 7.

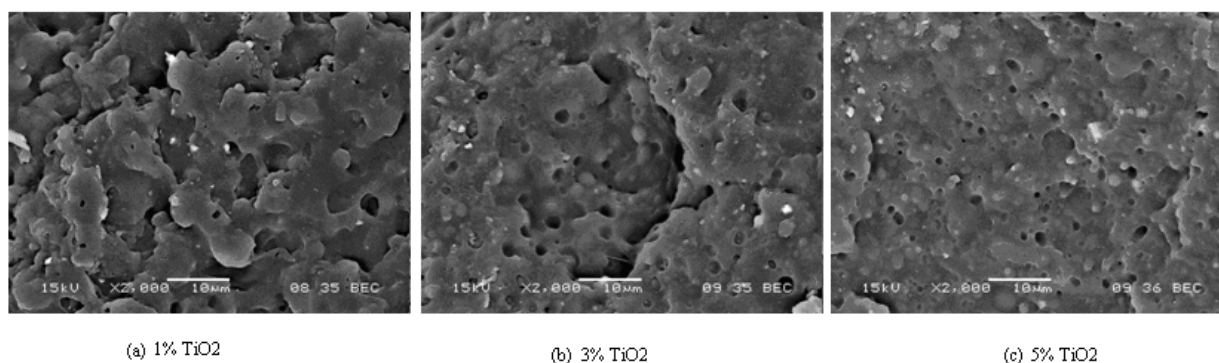


Fig. 6 SEM images of fracture surface of nano TiO_2 reinforced PP

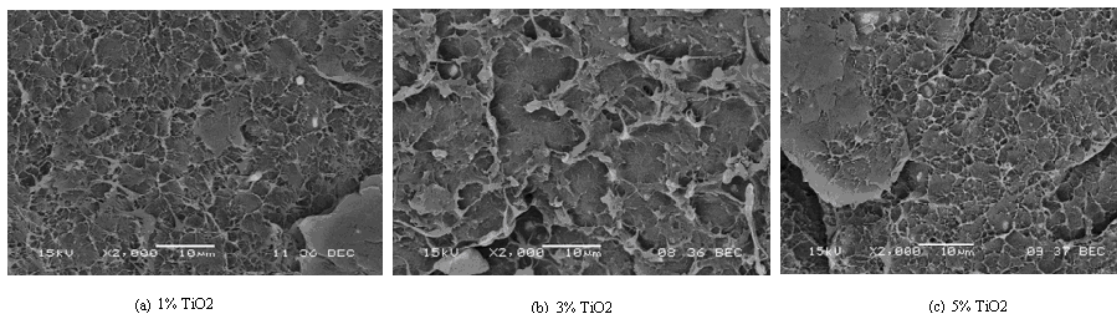


Fig. 7 SEM images of fracture surface of nano TiO₂ reinforced HDPE

IV. CONCLUSION

Polypropylene and high density polyethylene were reinforced with surface modified nano sized TiO₂ particles. Modification was made by coating the powders with SEBS-g-MA and silane, respectively. According to the DSC results of the HDPE matrix composites, TiO₂ behaved like nucleating agent and SEBS-g-MA favored degree of crystallization while degree of crystallization decreased for PP matrix composites due to the hindering effect of TiO₂. SEM results revealed that the presence of SEBS-g-MA and silane increased the surface adhesion and dispersion without agglomeration. Depending on that noteworthy increments were obtained in tensile strength, elastic modulus although small amount of TiO₂ additions were applied. Elongation at break decreased and impact strength reduced normally due to the stiff and rigid structure of TiO₂. Elastomeric nature of the SEBS-g-MA was thought to minimize the reduction of the impact strength besides its strong bridging effect between the inorganic filler and the polymer matrix.

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