

Interaction between Unsteady Supersonic Jet and Vortex Rings

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Abstract—The unsteady supersonic jet formed by a shock tube with a small high-pressure chamber was used as a simple alternative model for pulsed laser ablation. Understanding the vortex ring formed by the shock wave is crucial in clarifying the behavior of unsteady supersonic jet discharged from an elliptical cell. Therefore, this study investigated the behavior of vortex rings and a jet. The experiment and numerical calculation were conducted using the schlieren method and by solving the axisymmetric two-dimensional compressible Navier–Stokes equations, respectively. In both, the calculation and the experiment, laser ablation is conducted for a certain duration, followed by discharge through the exit. Moreover, a parametric study was performed to demonstrate the effect of pressure ratio on the interaction among vortex rings and the supersonic jet. The interaction between the supersonic jet and the vortex rings increased the velocity of the supersonic jet up to the magnitude of the velocity at the center of the vortex rings. The interaction between the vortex rings increased the velocity at the center of the vortex ring.

Keywords—Computational fluid dynamics, shock wave, unsteady jet, vortex ring.

I. INTRODUCTION

PULSED laser ablation (PLA) is a promising technique that has been applied to the growth of high-quality thin films. PLA has recently been used for forming nanoclusters under a high background gas pressure [1]. Subsequently, thin films can be formed by layering the clusters discharged through pulsed lasing, and the optimal size cluster can then be selected through conventional pulsed laser deposition [2], [3].

Iwata et al. [4] proposed a method for producing monodispersed clusters; this method, which uses an interaction phenomenon between the plume and shock wave arising in an elliptical cell following laser ablation under inert gas, is expected to facilitate the direct generation of monodispersed clusters. For simplifying the numerical analysis, the laser-ablated plume is substituted with a supersonic jet formed by a shock tube with a small high-pressure chamber. An adequately small shock tube can describe the pulsed expansion dynamics of the gas flow. This approach is a good alternative to

describe gas ejection from the target during PLA. The high-pressure region formed by the laser irradiation, the laser-ablated plume, and the substrate correspond to the shock wave with a small high-pressure section, the supersonic jet injected from the shock tube, and the impingement plate, respectively.

Sakamoto et al. proposed vortex ring formation due to shock wave discharge from the exit of the elliptical cell [5]. However, little research has been conducted on the interaction between vortex rings and jets. Therefore, the present study investigated the behavior of vortex rings and a jet.

II. NUMERICAL METHOD

The axisymmetric two-dimensional compressible Navier–Stokes equations are solved using the finite-volume method with the total variation diminishing scheme in curvilinear generalized coordinates. The inviscid flux is evaluated by third-order Roe’s approximate Riemann solver. The grid number is 1259×713 . The flow field is shown in Fig. 1. For the boundary conditions, non-slip conditions are applied to the cell wall. The pressure ratio P_h/P_b is the calculation parameter, where P_h and P_b are the pressures of the high-pressure section and backpressure, respectively. The area downstream of the elliptical cell is focused on.

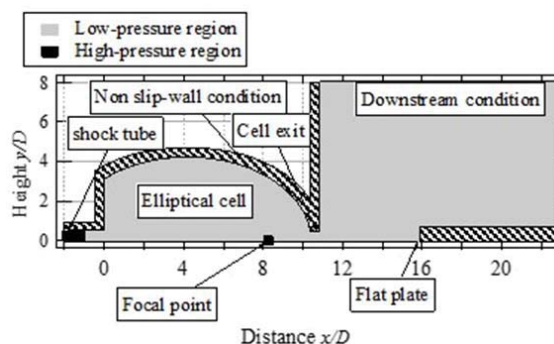


Fig. 1 Flow field for computation and boundary conditions

III. EXPERIMENTAL APPARATUS

Fig. 2 shows a schematic diagram of the experimental apparatus. The high-pressure section was filled with high-pressure air from an air bottle. The high pressure air was discharged into the atmosphere by bursting the diaphragm using a needle. The pressure in the high-pressure section was monitored using a semi-conductor pressure sensor. Unsteady pressure at the center of the flat plate is carried out by a high frequency semi-conductor pressure sensor and a 14bit

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AD-converter to monitor characteristics of the jet. The flow was visualized by schlieren method using still camera and high-speed camera as a continuous light source with a metal halide lamp.

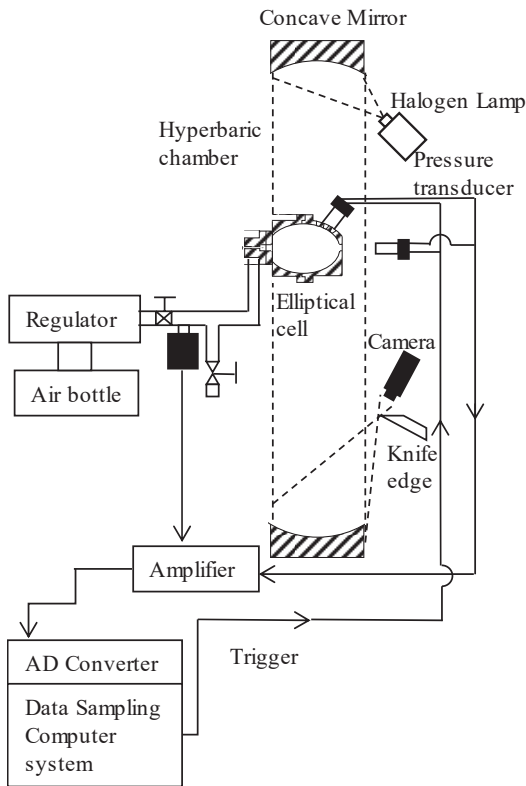


Fig. 2 Experimental apparatus

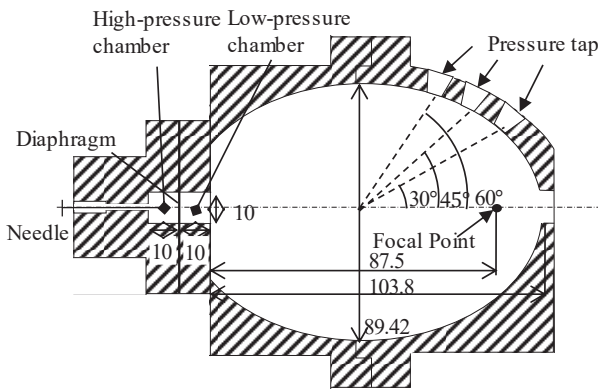


Fig. 3 Side view of elliptical cell with shock tube

The simple open-ended shock tube has a diameter, D , of 10 mm and total length of 20 mm, with the length of the driver section being 10 mm (Fig. 3). A sheet of Lumirror (polyethylene terephthalate) was used as the diaphragm. The pressure ratio P_H/P_b of the shock tube was sequentially set to 10.7, 20.6, 36.0, and 47.4, which corresponds to film thicknesses of 25, 50, 75, and 100 μm .

IV. RESULTS AND DISCUSSION

In Fig. 4, the evolution process of the flow field of our computational results is compared with the experimental results. The experimental sequence pictures and numerical results were obtained using the schlieren method for $P_H/P_b = 46.4$ and the computer schlieren contours for $P_H/P_b = 47.4$, respectively. The figure shows the generation and evolution process of the vortex ring. The arrows indicate the vortex ring and the shock wave. The position of the evolving vortex ring and the propagation of shock waves in the calculation and experiment agreed well.

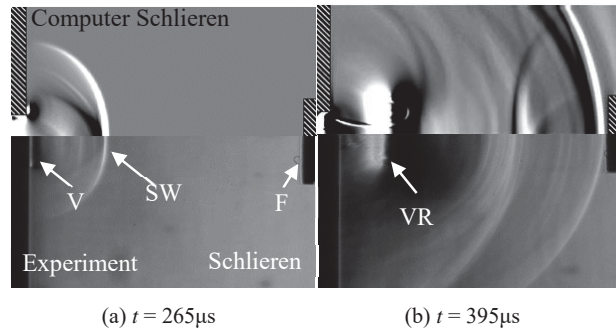


Fig. 4 Comparison of first generated vortex ring evolution process of computational results with the corresponding experimental results (VR: Vortex ring; SW: Shock wave; F: Flat plate)

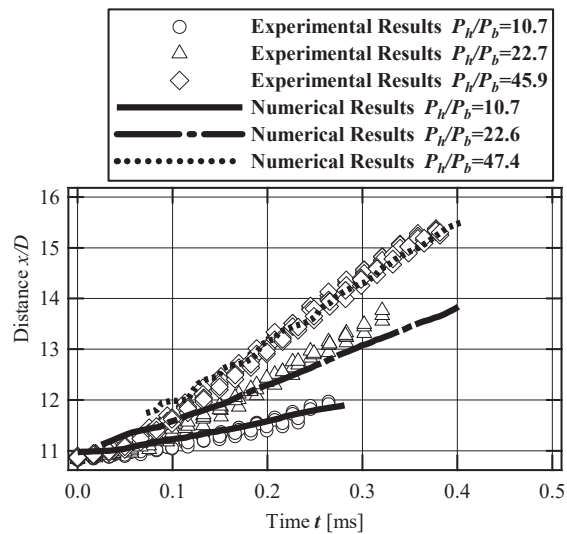


Fig. 5 Comparison of first generated vortex ring trajectories of computational results with the corresponding experimental results

The vortex ring trajectories of the computational results is compared in Fig. 5 with experimental results. x/D monotonically increased with time, and the gradient of x/D increased with P_H/P_b . The vortex ring trajectories in the calculation and experiment were consistent with each other.

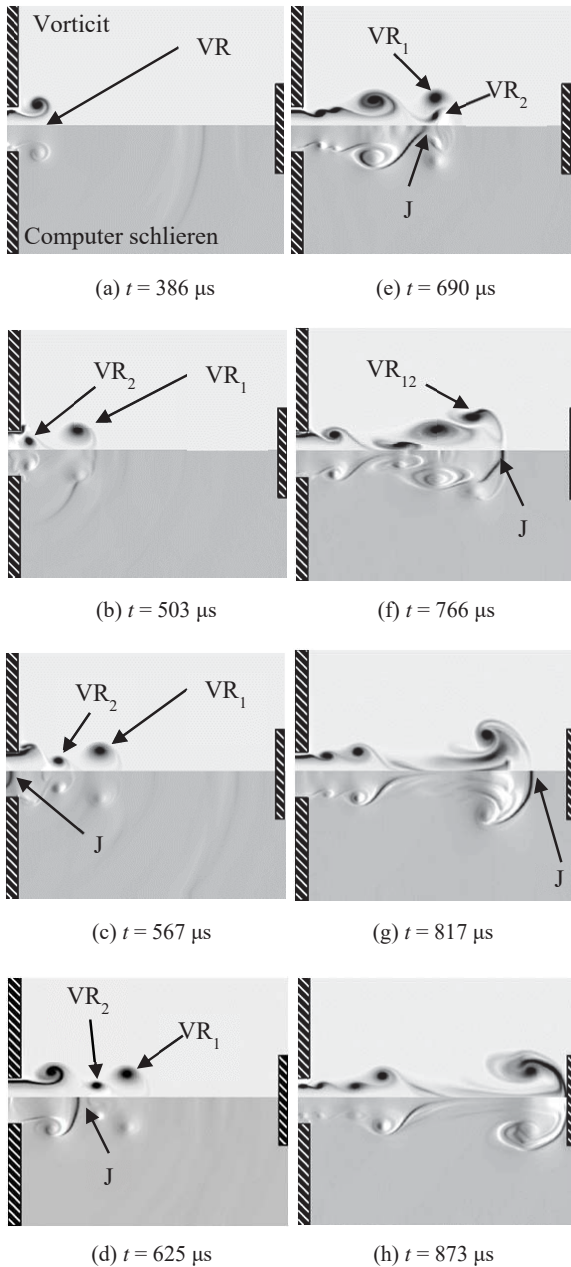


Fig. 6 Vorticity and computer schlieren variations for $P_t/P_b = 22.6$ (VR₁: first generated vortex ring; VR₂: second generated vortex ring; VR₁₂: merging vortex ring; J: Jet head)

Figs. 6 (a)–(f) show the calculated vorticity contours and computer schlieren images for $P_t/P_b = 22.6$, where t denotes the time elapsed from the moment of the jet injection. Fig. 6 (a) shows the formation of the vortex ring. Fig. 6 (b) shows the formation of the second generated vortex ring. We refer to first generated vortex ring and second generated vortex ring as "VR₁" and "VR₂", respectively. VR₂ is formed by VR₁ because of Kelvin-Helmholtz instability [6]. Fig. 6 (c) shows the jet discharged from the cell exit. In Fig. 6 (d), the distances among VR₁, VR₂, and the jet decreased relative to that in Fig. 6 (c) are

given. Fig. 6 (e) shows the interaction among VR₁, VR₂ and the jet, and Fig. 6 (f) depicts VR₁ and VR₂ merging into the *merging vortex ring* (VR₁₂). At this time, the jet is closer to the flat plate than it is to VR₁₂, which shows that the jet passes through the vortex ring because the velocity of the jet is higher than those of the vortex rings.

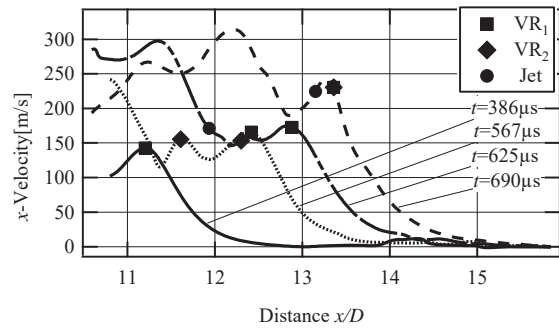


Fig. 7 Velocity profiles along the center axis at the indicated times for $P_t/P_b = 22.6$

For the interaction between the jet and the vortex ring, it is important to determine the effect of the vortex rings on the velocity of the jet. The velocity profiles along the center axis for $P_t/P_b = 22.6$ are shown in Fig. 7. In Fig. 7, the peaks occur at $x/D = 11.2, 12.4, 12.9,$ and 13.4 at $t = 386, 567, 625,$ and $690 \mu s$, respectively; these peaks were consistent with the position of VR₁. The peak velocity is probably due to the axial velocity of VR₁. The other peaks occurred at $x/D = 11.6, 12.3,$ and 13.4 at $t = 567, 625,$ and $690 \mu s$, respectively, which were attributed to VR₂. At $t = 690 \mu s$, the peak velocity caused by VR₁ was the highest for the distance between VR₁ and VR₂ ($L/D = 0$); the next highest was for $L/D = 0.58$ at $t = 625 \mu s$, and the lowest was for $L/D = 0.81$ at $t = 567 \mu s$. These peaks increased in magnitude with decrease in the L/D . The superimposition of VR₁ and VR₂ result in the maximum peak velocity.

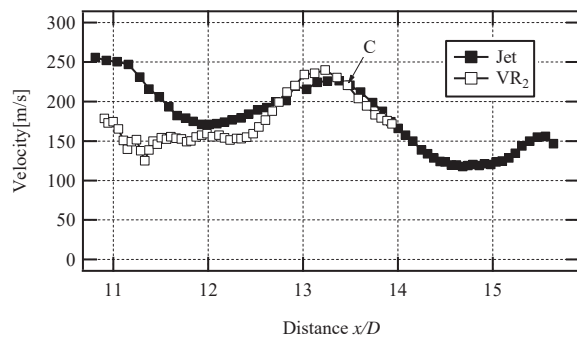


Fig. 8 x -Velocity at the center of 2nd vortex ring and Jet velocity versus axial distance from the shock tube for $P_t/P_b = 22.6$ (C: position at which the jet and the vortex ring are superimposed)

VR₁ and VR₂ produce the peak axial velocity. It has been felt that the peak axial velocity affects the velocity of the jet because the jet interacts with the vortex rings. For the investigation of the effect of the vortex ring on the jet, the

velocity variation of the jet and the axial velocity of VR₂ are shown in Fig. 8, where C indicates the position at which the jet and the vortex ring are superimposed ($x/D = 13.3$). The velocity of the jet and the axial velocity of VR₂ increased from $x/D = 12.0$ and 12.3 reaching a maximum at $x/D = 13.3$ and 13.2 , respectively, before decreasing. The velocity of the jet corresponds to the axial velocity of the vortex ring at $x/D = 13.3$. It is found that the jet is thus accelerated by the vortex ring.

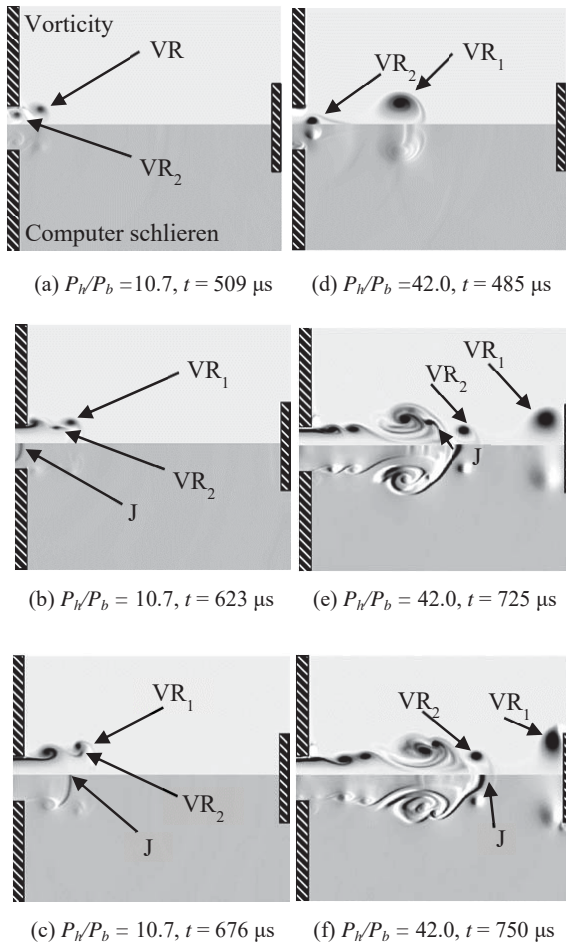


Fig. 9 Vorticity and computer schlieren showing the vortex rings ((a)–(c): $P_t/P_b = 10.7$, (d)–(f): $P_t/P_b = 42.0$)

The calculated vorticity contours and computer schlieren images for $P_t/P_b = 10.7$ and 42.0 are shown in Figs. 9(a)–(c) and (d)–(f), respectively. Fig. 9 (a) shows the formations of VR₁ and VR₂, Figs. 9 (b) and (c) show the interaction among VR₁, VR₂ and the jet, Fig. 9 (d) shows the formations of VR₁ and VR₂, and Figs. 9 (e) and (f) show the interaction between VR₂ and the jet. The vortex rings for $P_t/P_b = 10.7$ exhibit a quite different behavior for $P_t/P_b = 42.0$. It is that the translational velocity of VR₁ for $P_t/P_b = 42.0$ is higher than that for $P_t/P_b = 10.7$. Thus, the vortex ring interaction differs from that of P_t/P_b .

It is found to be the behavior of the interaction between VR₁ and VR₂ for P_t/P_b . The relationship between jet position and velocity is illustrated in Fig. 10. For $P_t/P_b = 10.7$, the jet velocity decreased monotonically. Fig. 10 shows the peak velocity of the jet at $x/D = 13.4$ and 13.9 for $P_t/P_b = 22.6$ and 42.0 , respectively; The peak velocity for $P_t/P_b = 22.6$ is higher than that for $P_t/P_b = 42.0$ because of the interaction between VR₁ and VR₂ for $P_t/P_b = 22.6$. The black squares indicate the velocity at the center of the vortex ring. The superimposition of the head of the jet and the center of the vortex ring increases the jet velocity up to the axial velocity magnitude of the vortex ring.

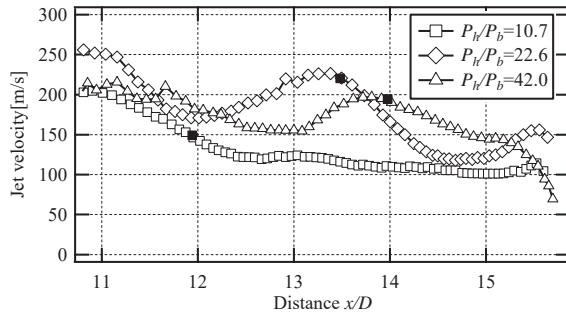


Fig. 10 Jet velocity versus axial distance from the shock tube for $P_t/P_b = 10.7$, 22.6 and 42.0 (black squares indicating the position at which the jet and the vortex ring are superimposed)

V. CONCLUSIONS

The conclusions of this study can be summarized as:

- 1) The position of the evolving vortex ring and the propagation of shock waves in the calculation and experiment agreed well.
- 2) The jet passes through the vortex ring because the velocity of the jet is higher than those of the vortex rings.
- 3) The axial velocity peaks at the vortex ring tended to increase with decrease in the distance between VR₁ and VR₂ for $P_t/P_b = 22.6$.
- 4) The superimposition of the jet head and the center of the vortex ring increases the velocity of the jet up to the axial velocity magnitude of the vortex ring for $P_t/P_b = 22.6$ – 42.0 .
- 5) The peak jet velocity for $P_t/P_b = 22.6$ is higher than that for $P_t/P_b = 42.0$ because of the interaction between the vortex rings for $P_t/P_b = 22.6$.

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