Using Artificial Neural Network Algorithm for Voltage Stability Improvement

Omid Borazjani, Mahmoud Roosta, Khodakhast Isapour, Ali Reza Rajabi

***Abstract*—**This paper presents an application of Artificial Neural Network (ANN) algorithm for improving power system voltage stability. The training data is obtained by solving several normal and abnormal conditions using the Linear Programming technique. The selected objective function gives minimum deviation of the reactive power control variables, which leads to the maximization of minimum Eigen value of load flow Jacobian. The considered reactive power control variables are switchable VAR compensators, OLTC transformers and excitation of generators. The method has been implemented on a modified IEEE 30-bus test system. The results obtain from the test clearly show that the trained neural network is capable of improving the voltage stability in power system with a high level of precision and speed.

***Keywords*—**Artificial Neural Network (ANN), Load Flow, Voltage Stability, Power Systems.

NOMENCLATURE

$[A]$: Square matrix.

a_{ij} : ij^{th} element of square matrix $[A]$.

$[B]$: Bus susceptance matrix.

$\Delta \overline{Ur}$: Deviation of reactive power control variables.

δ_i : Voltage phase angle at bus-i.

η_K : Left Eigen vector corresponding to K^{th} Eigen value.

η_{min} : Left Eigen vector corresponding to minimum Eigen value of load flow Jacobian.

$[G]$: Bus conductance matrix.

$[H]$: System sub-jacobian matrix.

$[J]$: System jacobian matrix.

$[L]$: System sub-jacobian matrix.

λ_K : K^{th} Eigen value of square matrix.

λ_{min} : Minimum Eigen value of load flow Jacobian.

$\lambda_{min\,New}$: New minimum Eigen value of load flow Jacobian.

$\lambda_{min\,Old}$: Old minimum Eigen value of load flow Jacobian.

$[M]$: System sub-Jacobian matrix.

$[N]$: System sub-Jacobian matrix.

NC : Number of system control variables.

P_i : Net active power at bus-i.

Q_c : Shunt capacitive compensations.

Q_G : Reactive power generation.

Q_i : Net reactive power at bus-i.

$\overline{S\lambda}$: Sensitivity of minimum Eigen value with respect to reactive power control variables.

$S\lambda_K$: Sensitivities of minimum Eigen value with respect to K^{th} reactive power control variable.

Tp : Tap changing transformers.

θ_{ij} : Phase angle of ij^{th} element of bus admittance matrix.

$\overline{U}$: System control variables.

$\overline{Ur}$: Reactive power control variables.

$|V_G|$: Voltage magnitude of generator bus.

V_i : Voltage at bus-i.

ξ_K : Right Eigen vector corresponding to K^{th} Eigen value.

ξ_{min} : Right Eigen vector corresponding to minimum Eigen value of load flow Jacobian.

$|Y_{ij}|$: Magnitude of ij^{th} element of bus admittance matrix.

I. INTRODUCTION

MOST of the time, power Systems operate under semi-steady state conditions, various kinds of disturbance frequently occur on electric power system which lead to loss of stability. Voltage stability is concerned with the ability of an electric system to keep acceptable voltages in the system under normal conditions and after being subjected to a disturbance. A system enters a state of voltage instability when a disturbance causes a progressive and uncontrollable decline in voltage. Fundamentally, voltage instability is due to the system inability to meet reactive power demand.

One of the main considerations in power system operation and control is to offer solutions in real time to the system operator in the Energy Control Center (ECC). This can enable system operators to meet the ever growing demand of electric power while maintaining system security.

As a consequence, the terms "voltage instability" and "voltage collapse" are appearing more frequently in the literature and in discussions of system planning and operation. Many approaches have been used for power system voltage stability assessment, e.g., power flow Jacobian matrix technique [1], total active and reactive power losses technique [2], singular value decomposition method [3], multiple load flow solution technique [4], energy function methods[5], and Artificial neural networks (ANN) [6]-[8]. Most of the methods discussed above have assessed the voltage instability based on the indices which depend on load bus voltage magnitudes. However, voltage magnitude alone is not a sufficient indicator of voltage instability. Load bus voltages may be high but the maximum load ability may be very close to the present

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operating point. It is the demand of the day that modern large interconnected power system's load buses should not only have high voltage magnitude but the operating point should have sufficient distance in term of MVA from voltage collapse point. This distance is of extreme importance in the enhancement procedure of voltage stability margin. This can be incorporated via a proximity indicator. Minimum Eigen value of load flow Jacobian is such a proximity indicator that it can be used in this case, but it requires comparatively large computation time and does not offer quick screening of outages and hence is not suitable for online applications.

Artificial Neural Networks (ANN) [9] can give fast, through approximate, but acceptable solutions in real time as they mostly use parallel processing technique for computation.

In this research, a method is introduced to monitor, evaluate, and improve steady state voltage stability in electrical power systems. The proposed method uses artificial neural networks (ANN) as a decision making tool to enhance steady state voltage stability. Learning vector necessary to train the ANN is generated using Linear Programming (LP) technique introduced in the Matlab's optimization toolbox. The selected objective function gives minimum deviation of the control variables, which leads to the maximization of minimum Eigen value of load flow Jacobian. The proposed method was tested on the modified IEEE 30-bus test system.

II. EIGEN SENSITIVITIES

An estimate of absolute sensitivity of Eigen value of λ_K in relation to any element a_{ij} of square matrix $[A]$ can be written as [10]:

$$\frac{\partial \lambda_K}{\partial a_{ij}} \frac{\eta_K(i)\xi_K(j)}{\overline{\eta}_K^T \overline{\xi}_K} \qquad (1)$$

where, a_{ij} is ij^{th} element of square matrix $[A]$; λ_K is k^{th} Eigen value of square matrix $[A]$; $\eta_K(i)$, $\xi_K(j)$ are i^{th} and j^{th} element of left and right Eigen vector corresponding to λ_K; $\overline{\eta}_K, \overline{\xi}_K$ are left and right Eigen vectors respectively corresponding to λ_K. Further each element a_{ij} is a function of system control variables ($\overline{U}$) i.e.;

$$a_{ij} = f(U_1, \ldots, U_{NC}) \qquad (2)$$

Hence, the sensitivity of λ_K with respect to system parameter of control variable can be written using chain rule of differentiation as;

$$\frac{\partial \lambda_K}{\partial U_1} = \sum_{i,j} \frac{\partial \lambda_K}{\partial a_{ij}} \times \frac{\partial a_{ij}}{\partial U_1} \qquad (3)$$

or

$$\frac{\partial \lambda_K}{\partial U_1} = \sum_{i,j} \frac{\eta_K(i)\xi_K(j)}{\eta_K^T \xi_K} \times \frac{\partial a_{ij}}{\partial U_1} \qquad (4)$$

III. FORMULATION OF OBJECTIVE FUNCTION

It has already been emphasized that minimum Eigen value of load flow Jacobian signifies proximity of the present operating point to the voltage collapse point. All Eigen values of load flow Jacobian are positive in upper segment of PV-curve. At least one Eigen value becomes negative in low segment of this nose curve. At voltage collapse point, one of the Eigen value becomes zero. Hence, the magnitude of minimum Eigen value is an indicator of relative voltage stability margin [11]. Sensitivities of minimum Eigen value with respect to reactive power control variables are derived in this section. The load flow Jacobian at solution point can be written as:

$$[J] = \begin{bmatrix} H & N \\ M & L \end{bmatrix} \qquad (5)$$

The elements of sub-Jacobians $[H], [M], [N]$, and $[L]$ are given as follows; Diagonal and off diagonal element of $[H]$;

$$H_{ii} = -Q_i - |V_i|^2 B_{ii} \qquad (6)$$

$$H_{ij} = |V_i||V_j||Y_{ij}|Sin(\delta_i - \delta_j - \theta_{ij}) \qquad (7)$$

Diagonal and off diagonal element of $[M]$;

$$M_{ii} = P_i - |V_i|^2 G_{ii} \qquad (8)$$

$$M_{ij} = -|V_i||V_j||Y_{ij}|Cos(\delta_i - \delta_j - \theta_{ij}) \qquad (9)$$

Diagonal and off diagonal element of $[N]$;

$$N_{ii} = |V_i|G_{ii} + \frac{P_i}{|V_i|} \qquad (10)$$

$$N_{ij} = |V_i||Y_{ij}|Cos(\delta_i - \delta_j - \theta_{ij}) \qquad (11)$$

Diagonal and off diagonal element of $[L]$;

$$L_{ii} = \frac{Q_i}{|V_i|} - |V_i|B_{ii} \qquad (12)$$

$$L_{ij} = |V_i||Y_{ij}|Sin(\delta_i - \delta_j - \theta_{ij}) \qquad (13)$$

Let $\overline{\xi}_{min}$ and $\overline{\eta}_{min}$ are right and left Eigen vectors corresponding to minimum Eigen value (λ_{min}) of load flow Jacobian, then from (3), the sensitivity of λ_{min} with respect to reactive power control variable (U_{r_K}) can be written as;

$$S\lambda_K = \frac{\partial \lambda_{min}}{\partial U_{r_K}} = \sum_{i,j} \frac{\partial \lambda_{min}}{\partial H_{ij}} \times \frac{\partial H_{ij}}{\partial U_{r_K}} + \sum_{i,j} \frac{\partial \lambda_{min}}{\partial M_{ij}} \times \frac{\partial M_{ij}}{\partial U_{r_K}} + \sum_{i,j} \frac{\partial \lambda_{min}}{\partial N_{ij}} \times \frac{\partial N_{ij}}{\partial U_{r_K}} + \sum_{i,j} \frac{\partial \lambda_{min}}{\partial L_{ij}} \times \frac{\partial L_{ij}}{\partial U_{r_K}} \qquad (14)$$

where; $\overline{U_r}$ = Vector of reactive power control variables:

$$\overline{Ur} = [Ur_1, Ur_2, \ldots\ldots\ldots, Ur_{NC}]$$

$$\overline{Ur} = \left[\left. V_G \right| : Q_C : Tp \right]$$

This means reactive power control variables consist of generator-bus voltage, shunt capacitive compensations and tap changing transformers. The sensitivities $\frac{\partial \lambda_{min}}{\partial H_{i,j}}$, $\frac{\partial \lambda_{min}}{\partial M_{i,j}}$, $\frac{\partial \lambda_{min}}{\partial N_{i,j}}$, and $\frac{\partial \lambda_{min}}{\partial L_{i,j}}$ can be evaluated using (1). Expressions for other partial derivatives in (14) are evaluated using the element of load flow Jacobian as given in (5) [12]. The total deviation of minimum Eigen value with respect to all reactive power control variables can be written as;

$$\Delta \lambda_{min} = \sum_{K=1}^{NC} \Delta Ur_K \times S\lambda_K \tag{15}$$

where;

$$\Delta \lambda_{min} = \lambda_{min\,New} - \lambda_{min\,Old} \tag{16}$$

After simplification, the final form of (15) is;

$$\lambda_{min\,New} = \lambda_{min\,Old} + \Delta \overline{Ur}^T \times \overline{S\lambda} \tag{17}$$

Equation (17) is used as the objective function of Linear Programming (LP) technique and from it the minimum rescheduling of reactive power control variables can be obtained.

IV. OPTIMAL REACTIVE POWER CONTROL VARIABLES

The purpose of optimal reactive power control variables is to improve the voltage stability in the power system by the control of generators voltage, transformer tap setting, and switching of VAR sources.

Linear Programming (LP) introduced in the Matlab's optimization toolbox is used to find the optimal value of the minimum Eigen value of load flow Jacobian so as to maintain desired voltage profile with minimum shift in reactive power control variables, such that the limits of reactive power is not violated. Equation (17) has been used as objective function; this function is maximized to obtain the highest minimum Eigen value corresponding to the best voltage stability margin. Therefore;

$$\text{Maximize}_{F(\Delta Ur)} = \lambda_{min\,New} = \lambda_{min\,Old} + \Delta \overline{Ur}^T \times \overline{S\lambda} \tag{18}$$

The constraints of problem are formulated as:

$$V_i^{min} \le V_i \le V_i^{max} \tag{19}$$

$$Q_{Gi}^{min} \le Q_{Gi} \le Q_{Gi}^{max} \tag{20}$$

$$Q_{Ci}^{min} \le Q_{Ci} \le Q_{Ci}^{max} \tag{21}$$

$$Tp_i^{min} \le Tp_i \le Tp_i^{max} \tag{22}$$

V. VOLTAGE STABILITY IMPROVEMENT BY USING ANN

The method proposed is based on using linear programming technique to generate different training patterns and obtain the input data to ANN. In this study, feed-forward ANN which contains three layers (Two hidden layers and one output layer) is trained by using Back propagation algorithm to determine the proper adjustment of the reactive power control variables required to improve voltage stability. The block diagram of the ANN-based algorithm for improving voltage stability in power systems is shown in Fig. 1. Furthermore, to design a neural network, it is very important to train and test the network. The well-trained neural network should give the right decision for both normal and abnormal operating conditions.
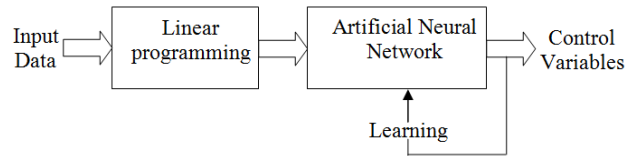

Fig. 1 The block diagram of the ANN-based algorithm for improving voltage stability in power systems

Training is a stage at which all the weighting factors and thresholds are regulated according to a specific rule, in such a way that the objective function may be minimized. The usual method for training a multi-layer feed-forward neural network is the method of error back-propagation (or back-propagation). In order to use this method, both the desired output and the real output of the network must be available. The difference between desired output and real output is called the error. The algorithm of error back-propagation is based on the learning rule of error correction. This algorithm is an iterative method designed for minimizing the average of the squared error.
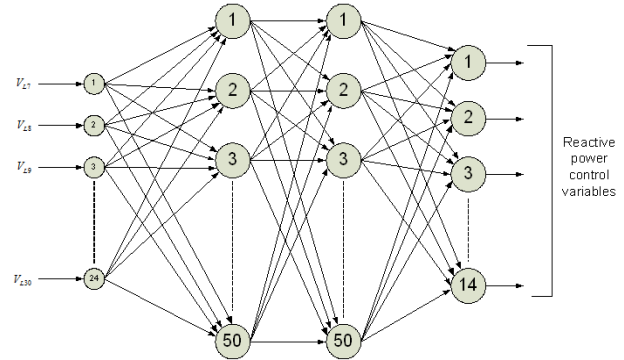
Fig. 2 Structure of neural network concerning IEEE 30-bus test system

In order to improve the performance and speed of the training process, it is very important to reduce the number of training data. In a real power system, the working conditions of the system change by variations in the scale of load demand. The load variations themselves bring about variation in the load bus voltages and sometimes cause buses to violate their voltage limits and in turn cause the system stability to

violate their authorized limits. In this study, in order to improve the voltage stability against load variations in the modified IEEE 30-bus test system, initial load flow analysis is carried out for the considered power system for different load conditions. Voltage instability analysis is performed from the data that obtained from load flow. Sensitivities of minimum Eigen value with respect to reactive power control variables are computed. By performing the LP, the recommendations of transformer taps, shunt capacitors, generator voltages are computed. Voltage profile at load buses are considered as inputs to the neural network. The LP recommendation values form the target vectors (desired output). The considered structure of the neural network is shown in Fig. 2.

VI. THE CASE STUDY

The modified IEEE 30-bus power system given in [13] and shown in Fig. 3 has been studied and considered to test the performance of the proposed method. Its bus data are given in Table I. The limits of bus voltages, tap settings, shunt capacitors, and generators VAR's are given in Table II. The line data of the system are given in Table III.

TABLE I
BUS DATA

Bus No.	P_G (MW)	Q_G (MVAR)	P_L (MW)	Q_L (MVAR)
1	-----	-----	0.00	0.00
2	20.0	-----	21.7	12.7
3	10.0	-----	74.2	19.00
4	10.0	-----	30.0	30.00
5	5.0	-----	0.00	0.00
6	5.0	-----	0.00	0.00
7	0.00	0.00	25.4	1.2
8	0.00	0.00	7.6	1.6
9	0.00	0.00	0.00	0.00
10	0.00	0.00	18.8	10.9
11	0.00	0.00	0.00	0.00
12	0.00	0.00	15.8	2.00
13	0.00	0.00	11.2	7.5
14	0.00	0.00	6.2	1.6
15	0.00	0.00	18.2	2.5
16	0.00	0.00	3.5	1.8
17	0.00	0.00	9.0	5.8
18	0.00	0.00	3.2	0.9
19	0.00	0.00	9.5	3.4
20	0.00	0.00	2.2	0.7
21	0.00	0.00	12.5	11.2
22	0.00	0.00	0.00	0.00
23	0.00	0.00	3.2	1.6
24	0.00	0.00	14.7	6.7
25	0.00	0.00	0.00	0.00
26	0.00	0.00	11.5	2.3
27	0.00	0.00	0.00	0.00
28	0.00	0.00	0.00	0.00

TABLE II
LIMITS OF SYSTEM VARIABLES

	Variables		Limits	
			Low	High
Control variables	(Generator voltage) V_G	p.u.	1.00	1.10
	(Tap setting) Tp	p.u	0.95	1.05
	(VAR source) Q_C	MVAR	-15	36
Dependent variables	(Load bus voltage) V_l	p.u.	0.90	1.10
	(Generator reactive power) Q_G	MVAR	-40	100
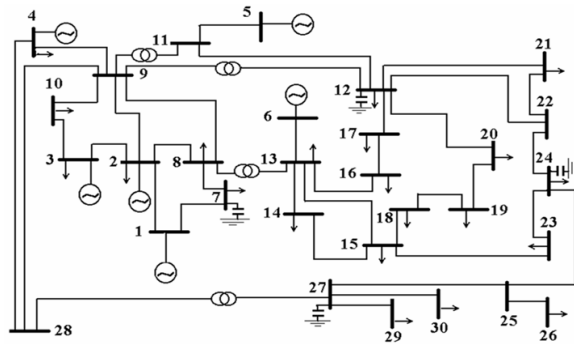
Fig. 3 The modified IEEE 30-bus test system

TABLE III
LINE DATA

From bus	To bus	R (P.U)	X (P.U)	B/2 (P.U)	Tap Ratio
1	2	0.0192	0.0575	0.0264	-
1	7	0.0452	0.1852	0.0204	-
2	8	0.057	0.1737	0.0184	-
7	8	0.0132	0.0379	0.0042	-
2	3	0.0472	0.1983	0.0209	-
2	9	0.0581	0.1763	0.0187	-
8	9	0.0119	0.0414	0.0045	-
3	10	0.046	0.116	0.0102	-
9	10	0.0267	0.082	0.0085	-
9	4	0.012	0.042	0.0045	-
9	11	0	0.208	0	1
9	12	0	0.556	0	1
11	5	0	0.208	0	-
11	12	0	0.11	0	-
8	13	0	0.256	0	1
13	6	0	0.14	0	-
13	14	0.1231	0.2559	0	-
13	15	0.0662	0.1304	0	-
13	16	0.0945	0.1987	0	-
14	15	0.221	0.1997	0	-
16	17	0.0824	0.1923	0	-
15	18	0.1073	0.2185	0	-
18	19	0.0639	0.1292	0	-
19	20	0.034	0.068	0	-
12	20	0.0936	0.209	0	-
12	17	0.0324	0.0845	0	-
12	21	0.0348	0.0749	0	-
12	22	0.0727	0.1499	0	-
21	22	0.0116	0.0236	0	-
15	23	0.1	0.202	0	-
22	24	0.115	0.179	0	-
23	24	0.132	0.27	0	-
24	25	0.1885	0.3292	0	-
25	26	0.2544	0.38	0	-
25	27	0.1093	0.2087	0	-
28	27	0	0.396	0	1
27	29	0.2198	0.4153	0	-
27	30	0.3202	0.6027	0	-
29	30	0.2399	0.4533	0	-
4	28	0.0636	0.2	0.0214	-
9	28	0.0169	0.0599	0.065	-

VII. RESULTS

Both methods of linear programming and artificial neural networks have been simulated in MATLAB software and have been applied to the modified IEEE 30-bus test system. The ANN was trained with the three sets of data as shown in Tables IV and V, obtained by performing load flow and voltage instability analysis for different load factors such as 0.8, 1.0, and 1.2.

TABLE IV
INPUT DATA USED FOR TRAINING THE ANN

No. Load bus	Voltage with load factor 80% (P.U)	Voltage with load factor 100% (P.U)	Voltage with load factor 120% (P.U)
7	0.98	0.98	0.97
8	0.98	0.98	0.97
9	0.99	0.98	0.98
10	0.99	0.98	0.98
11	0.98	0.97	0.96
12	0.96	0.95	0.93
13	0.98	0.97	0.95
14	0.96	0.95	0.93
15	0.95	0.94	0.92
16	0.96	0.95	0.93
17	0.96	0.94	0.92
18	0.94	0.93	0.9
19	0.94	0.92	0.9
20	0.95	0.93	0.91
21	0.95	0.93	0.91
22	0.95	0.93	0.91
23	0.94	0.92	0.9
24	0.93	0.91	0.88
25	0.93	0.91	0.88
26	0.9	0.86	0.82
27	0.95	0.93	0.9
28	0.99	0.98	0.97
29	0.92	0.89	0.85
30	0.91	0.88	0.84

TABLE V
INPUT DATA (DESIRED) USED FOR TRAINING THE ANN

Type of Control variables	Recommendations Provided by LP Technique		
	Control variables with load factor 80% (P.U)	Control variables with load factor 100% (P.U)	Control variables with load factor 120% (P.U)
V_G -1	1.07	1.09	1.1
V_G -2	1.02	1.04	1.04
V_G -3	1	1.05	1.06
V_G -4	1.01	1	1
V_G -5	1.08	1	1
V_G -6	1.05	1.05	1.07
Qc at bus-7	-0.12	0.36	0.369
Qc at bus-12	0.221	0.198	-0.12
Qc at bus-24	0.293	0.179	0.382
Qc at bus-27	0.035	0.159	0.112
Tp 9-11	0.974	0.98	0.982
Tp 9-12	1.041	1.04	1.027
Tp 8-13	0.95	0.95	0.965
Tp 28-27	0.995	1.011	1.028

The data indicated in Table VI are used for testing the ANN; these data are obtained in exactly the same way as the training set. The ANN is tested with data corresponding to load factors of 0.75 and 1.3 to determine the effectiveness of the proposed method. Proper actions suggested by both techniques are shown in Table VII.

TABLE VI
INPUT DATA USED FOR TESTING THE ANN

No. Load bus	Voltage with load factor 75% (P.U)	Voltage with load factor 130% (P.U)
7	0.99	0.96
8	0.99	0.96
9	0.99	0.97
10	0.99	0.97
11	0.98	0.95
12	0.96	0.92
13	0.98	0.95
14	0.96	0.92
15	0.96	0.91
16	0.97	0.93
17	0.96	0.91
18	0.95	0.89
19	0.95	0.89
20	0.95	0.9
21	0.95	0.9
22	0.95	0.9
23	0.94	0.88
24	0.94	0.86
25	0.94	0.86
26	0.91	0.79
27	0.95	0.89
28	0.99	0.96
29	0.92	0.83
30	0.92	0.82

TABLE VII
THE RECOMMENDATIONS PROVIDED BY BOTH TECHNIQUES (LP AND ANN)

Type of Control variables	Recommendations Provided by LP Technique		Recommendations Provided by ANN Technique	
	Control variables with load factor 75% (P.U)	Control variables with load factor 130% (P.U)	Control variables with load factor 75% (P.U)	Control variables with load factor 130% (P.U)
V_G -1	1.06	1.09	1.06	1.089
V_G -2	1.03	1.05	1.03	1.045
V_G -3	1.02	1.04	1.01	1.06
V_G -4	1.0	1.0	1.0	0.998
V_G -5	1.1	1.04	1.2	1.04
V_G -6	1.06	1.01	1.05	1.015
Qc at bus-7	0.36	0.38	0.35	0.38
Qc at bus-12	0.026	0.039	0.025	0.035
Qc at bus-24	0.055	0.32	0.057	0.34
Qc at bus-27	0.082	0.156	0.08	0.16
Tp 9-11	0.98	1.024	0.98	1.025
Tp 9-12	1.037	0.95	1.04	0.95
Tp 8-13	0.956	0.983	0.95	0.97
Tp 28-27	0.987	1.030	0.99	1.03

TABLE VIII
COMPUTATION TIMES FOR LP AND ANN METHODS

Method	LP	ANN
Time (Sec.)	6.39	0.21

The decision of each method (LP and ANN) are almost coincident, however the ANN gives these decisions in almost on time. A comparison between the computational time of the proposed ANN technique and LP is shown in Table VIII. It is clearly shown that the ANN technique requires very small computational time to improve voltage stability. These results have been achieved by using a computer with Pentium CPU of 2.6 GHz, 512MB RAM specifications.

The results of pre and post optimization conditions for full load conditions (unity load factor) are shown in Table IX. We can conclude that the voltage profile has increased from 0.86 to 0.968 at bus-26, as the minimum Eigen value is increased from 0.194 to 0.214 and the power loss is reduced from 24.27MW to 20.46MW.

TABLE IX
THE PRE AND POST OPTIMIZATION CONDITIONS WITH FULL LOAD STATE

Load factor (unity)	Pre Optimization	Post Optimization
V_{min}	0.86 P.U.	0.968 P.U.
λ_{min}	0.194	0.214
power losses	24.27 MW	20.46MW

VIII. RESULTS

A quick technique to monitor and improve power system voltage stability is proposed, the strategy is based on ANN. Three layers feed-forward ANN with back-propagation is trained to offer the proper rescheduling of reactive power control variables required to reach voltage stability in the day-to-day operation. The considered reactive power control variables are switchable VAR compensators, OLTC transformers and excitation of generators. The training data is obtained by solving several conditions utilizing the LP technique. The outcomes obtained show clearly that the ANN approach is capable of improving voltage stability in power systems. The trained network is capable of improving the power system voltage stability from minimum to maximum range of load variations at very high speed. A comparison with the LP technique shows the clear superiority of the proposed ANN in achieving the control decision in a short computational time. Furthermore, the ANN is easy in structure and easy to operate compared with linear programming technique. Thus, the method can be used as a guide by the operator in Energy Control Center (ECC) for power system control. The proposed method indicates an important improvement in voltage stability which eventually results in a considerable decrease in system losses.

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