

# One Some Effective Solutions of Stokes Axisymmetric Equation for a Viscous Fluid

N. Khatiashvili, K. Pirumova, and D. Janjgava

**Abstract**—The Stokes equation connected with the fluid flow over the axisymmetric bodies in a cylindrical area is considered. The equation is studied in a moving coordinate system with the appropriate boundary conditions. Effective formulas for the velocity components are obtained. The graphs of the velocity components and velocity profile are plotted.

**Keywords**—Stokes system, viscous fluid.

## I. INTRODUCTION

THE stationary and non-stationary Newtonian fluids are investigated by numerous of authors by means of Navier-Stokes equation with the specific boundary conditions (see for example [1]-[11]).

We consider the fluid flow over some axisymmetric bodies which moves in the infinite cylindrical channel filled with a viscous fluid. These bodies have the same axis of symmetry. We admit that the pressure fall is a constant. In this case the velocity of the fluid satisfies the linearized Navier-Stokes equation with the appropriate initial-boundary conditions. The solutions of this equation have been obtained. Hence, the velocity components of the Stokes flow are found.

## II. STATEMENT OF THE PROBLEM

Let fluid occupied some cylindrical channel of the diameter  $d$  ( $d > 0$ ) and consider in this channel the motion of some system of axisymmetric bodies at a speed  $\vec{V}_0(V_x^0, V_y^0, V_z^0)$ . For low Reynolds number the Stokes equation with the equation of continuity are valid [1]-[6]:

$$\frac{\partial \vec{V}}{\partial t} = \vec{F} - \frac{1}{\rho} \text{grad} P + \nu \Delta \vec{V} \quad (1)$$

$$\frac{\partial V_x}{\partial t} + \frac{\partial V_y}{\partial y} + \frac{\partial V_z}{\partial z} = 0 \quad (2)$$

where  $\vec{V}(V_x, V_y, V_z)$  is the velocity vector,  $P$  is the pressure,  $\vec{F}(F_x, F_y, F_z)$  is the external force,  $\rho$  is a density of the fluid,  $\nu$  is a viscosity.

Equation (1) can be rewritten in terms of velocity components in the form:

$$\frac{\partial V_x}{\partial t} = F_x - \frac{1}{\rho} \frac{\partial P}{\partial x} + \nu \Delta V_x \quad (3)$$

$$\frac{\partial V_y}{\partial t} = F_y - \frac{1}{\rho} \frac{\partial P}{\partial y} + \nu \Delta V_y \quad (4)$$

$$\frac{\partial V_z}{\partial t} = F_z - \frac{1}{\rho} \frac{\partial P}{\partial z} + \nu \Delta V_z \quad (5)$$

Also the following boundary conditions are satisfied:

$$V_x|_{S_0} = 0, V_y|_{S_0} = 0, V_z|_{S_0} = 0 \quad (6)$$

$$V_x|_S = V_x^0(t), V_y|_S = V_y^0(t), V_z|_S = V_z^0(t) \quad (7)$$

where  $V_x^0(t), V_y^0(t), V_z^0(t)$ , are the given functions,  $S$  is a surface of the moving bodies,  $S_0$  is a surface of the cylindrical channel. The surface  $S$  and the width of a channel  $d$  will be defined according to the solutions.

Let the axis of symmetry is  $ox$  and consider the moving coordinate system. Suppose, that the bodies move parallel to the axis of symmetry at a constant speed  $\vec{V}_0(V_x^0, V_y^0, V_z^0)$  and

$$\frac{1}{\rho} \frac{\partial P}{\partial x} - F_x = C_0, \quad \frac{1}{\rho} \frac{\partial P}{\partial r} - F_r = 0,$$

where  $C_0$  is a definite constant,  $F_x, F_r$  are the components of the force in the cylindrical coordinates.

In a cylindrical coordinates (2), (3), (4), (5), becomes

$$\Delta V_x + \frac{1}{r} \frac{\partial V_x}{\partial r} = 2C_1 \quad (8)$$

N. Khatiashvili is with the I. Vekua Institute of. Iv. Javakhishvili Tbilisi State University, University St. 2, 0186 Tbilisi, Georgia (phone: 995 32 230-30-40; e-mail: ninakhatia@gmail.com).

K. Pirumova is with the Iv. Javakhishvili Tbilisi State University, 2, University St., 0186 Tbilisi, Georgia (e-mail: chr4mk@gmail.com).

D. Janjgava was with the Iv. Javakhishvili Tbilisi State University, 2, University St., 0186 Tbilisi, Georgia. He is now with the Logistic Center Lilo1, Iumashev St. 14, 0198 Tbilisi, Georgia (e-mail: admin@lilo1.com).

$$\Delta V_r + \frac{1}{r} \frac{\partial V_r}{\partial r} - \frac{V_r}{r^2} = 0 \tag{9}$$

$$\frac{\partial V_x}{\partial x} + \frac{\partial V_r}{\partial r} + \frac{V_r}{r} = 0 \tag{10}$$

where  $V_x, V_r$ , are the components of the velocity,

$$r = \sqrt{y^2 + z^2}, \quad C_1 = \frac{C_0}{2\nu}.$$

The boundary conditions will be given by:

$$V_x \Big|_{r=\pm h} = -V_x^0, \quad V_x \Big|_{\Gamma} = 0 \tag{11}$$

$$V_r \Big|_{r=\pm h} = 0, \quad V_r \Big|_{\Gamma} = 0 \tag{12}$$

where  $\Gamma$  is the contour of the bodies,  $h = d/2$ .

In the next chapter we will find the bounded solutions of the system (8), (9), (10), (11), (12), and  $\Gamma$ .

### III. SOLUTION OF THE PROBLEM

The function:

$$U = C^* - q \left\{ \frac{1}{\sqrt{(x+c)^2 + r^2}} - \frac{1}{\sqrt{(x-c)^2 + r^2}} \right\};$$

$C^* = const,$

where  $q$  and  $c$  are the certain parameters, is the solution of (8) for  $C_1 = 0$ , [11].

By direct verification we obtain, that the pair of functions:

$$V_x = \frac{\partial U}{\partial x} + C_1 r^2 - A, \quad V_r = \frac{\partial U}{\partial r}$$

where  $A$  ( $A > 0$ ) is the definite constant, is the solution of the system (8), (9), (10). Also, the pair of functions:

$$V_{xm} = \frac{\partial^m}{\partial x^m} \left( \frac{\partial U}{\partial x} \right) + C_1 r^2 - A, \quad V_{rm} = \frac{\partial^m}{\partial x^m} \left( \frac{\partial U}{\partial r} \right),$$

will be the solution of this system.

1. For odd  $m, m = 2n - 1, n = 1, 2, \dots$  the solutions of the system (8), (9), (10) are given by the formulas

$$V_{xm} = q \sum_{k=1}^n \left( \frac{\alpha_k r^{2k}}{\sqrt{(x+c)^2 + r^2}^{2k+1+2n}} - \frac{\alpha_k r^{2k}}{\sqrt{(x-c)^2 + r^2}^{2k+1+2n}} \right) + C_1 r^2 - A, \tag{13}$$

$$V_{rm} = q \sum_{k=1}^n \left( \frac{\alpha_k^* r^{2k-1} (x+c)}{\sqrt{(x+c)^2 + r^2}^{2k+1+2n}} - \frac{\alpha_k^* r^{2k-1} (x-c)}{\sqrt{(x-c)^2 + r^2}^{2k+1+2n}} \right) \tag{14}$$

where  $\alpha_k, \alpha_k^*$ , are the definite constants.

2. For even  $m, m = 2n, n = 1, 2, \dots$  the solutions of system (8), (9), (10) are given by

$$V_{xm} = q \sum_{k=0}^n \left( \frac{\beta_k r^{2k} (x+c)}{\sqrt{(x+c)^2 + r^2}^{2k+3+2n}} - \frac{\beta_k r^{2k} (x-c)}{\sqrt{(x-c)^2 + r^2}^{2k+3+2n}} \right) + C_1 r^2 - A, \tag{15}$$

$$V_{rm} = q \sum_{k=1}^{n+1} \left( \frac{\beta_k^* r^{2k-1}}{\sqrt{(x+c)^2 + r^2}^{2k+1+2n}} - \frac{\beta_k^* r^{2k-1}}{\sqrt{(x-c)^2 + r^2}^{2k+1+2n}} \right) \tag{16}$$

where  $\beta_k, \beta_k^*$ , are the definite constants.

For the different values of  $q, c$ , and  $A$  we obtain the different fluid flow over some axisymmetric bodies, the shape of which will be defined by the formulas

$$\frac{\partial^m}{\partial x^m} \left( \frac{\partial U}{\partial x} \right) + C_1 r^2 - A = 0 \tag{17}$$

$$\frac{\partial^m}{\partial x^m} \left( \frac{\partial U}{\partial r} \right) \approx 0 \tag{18}$$

In the following chapter some examples are given and the graphics of velocity components and velocity profile are plotted by using Maple.

**Note.** The Stokes equation has a real physical sense for low velocities only. So not for each parameters  $q, c$ , and  $A$ , the solutions of (8), (9), (10), (11), (12), are suitable according to the physical viewpoint.

### IV. THE CASE OF $m = 1$ AND $m = 2$ , EXAMPLES

1. In case of  $m = 1$ , by (13), (14), we obtain

$$V_{x1} = -\frac{2q}{(r^2 + (x+c)^2)^{\frac{3}{2}}} + \frac{2q}{(r^2 + (x-c)^2)^{\frac{3}{2}}} + \frac{3qr^2}{(r^2 + (x+c)^2)^{\frac{5}{2}}} - \frac{3qr^2}{(r^2 + (x-c)^2)^{\frac{5}{2}}} + C_1 r^2 - A,$$

$$V_{r1} = -\frac{3qr(x+c)}{(r^2 + (x+c)^2)^{\frac{5}{2}}} + \frac{3qr(x-c)}{(r^2 + (x-c)^2)^{\frac{5}{2}}}.$$

In Fig. 1, the lateral cross-section of the cylindrical area with the axisymmetric body is represented.

In Fig. 2 graphics of the corresponding velocity components are given (the black surface is  $V_{x1}$ , the gray surface is  $V_{r1}$ ) in case of  $c = 1/5; C_1 = 1; A = 9; q = 1/10$ . In Fig. 3 the corresponding velocity profile  $|V|, |V| = \sqrt{V_{x1}^2 + V_{r1}^2}$ , is plotted.

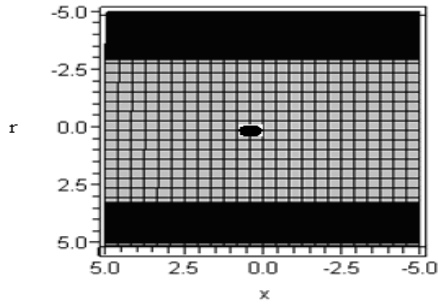


Fig. 1 The lateral cross-section of the cylinder of width  $1 < d < 2$  in case of  $c = 1/5; C_1 = 1; A = 9; q = 1/10$

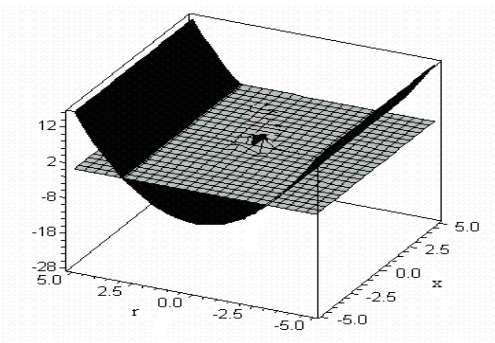


Fig. 2 The graphics of  $V_{x1}$  (black surface), and  $V_{r1}$  (gray surface) in case of  $c = 1/5; C_1 = 1; A = 9; q = 1/10$

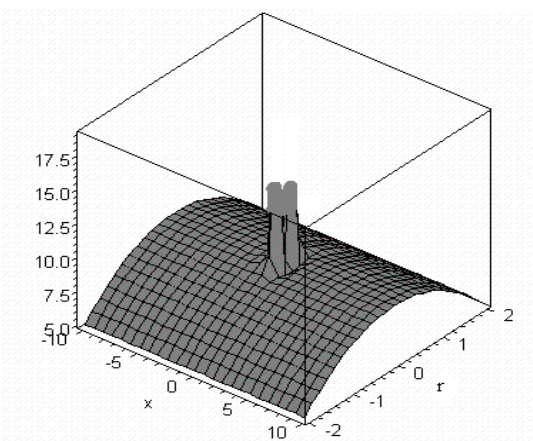


Fig. 3 The graphic of the velocity profile in case of  $c = 1/5; C_1 = 1; A = 9; q = 1/10$

2. In case of  $m=2$  by (15), (16), we obtain

$$V_{x2} = \frac{6q(x+c)}{(r^2 + (x+c)^2)^{\frac{5}{2}}} - \frac{6q(x-c)}{(r^2 + (x-c)^2)^{\frac{5}{2}}} - \frac{15qr^2(x+c)}{(r^2 + (x+c)^2)^{\frac{7}{2}}} + \frac{15qr^2(x-c)}{(r^2 + (x-c)^2)^{\frac{7}{2}}} + C_1 r^2 - A,$$

$$V_{r2} = \frac{12qr}{(r^2 + (x+c)^2)^{\frac{5}{2}}} - \frac{12qr}{(r^2 + (x-c)^2)^{\frac{5}{2}}} - \frac{15qr^3}{(r^2 + (x+c)^2)^{\frac{7}{2}}} + \frac{15qr^3}{(r^2 + (x-c)^2)^{\frac{7}{2}}}.$$

In Fig. 4, the lateral cross-section of the cylindrical area with the axisymmetric body is represented.

In Fig. 5 graphics of the corresponding velocity components are given (the black surface is  $V_{x2}$ , the gray surface is  $V_{r2}$ ) in case of  $c = 1; C_1 = 1; A = 9; q = 1/10$ . In Fig. 6 the corresponding velocity profile  $|V|, |V| = \sqrt{V_{x2}^2 + V_{r2}^2}$ , is plotted.

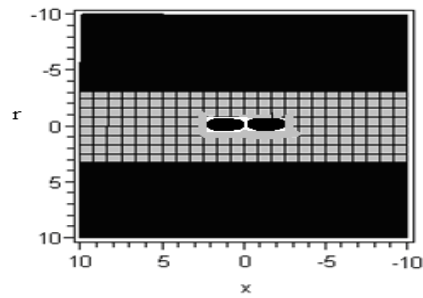


Fig. 4 The lateral cross-section of the cylinder of width  $1 < d < 3$ , in case of  $c = 1; C_1 = 1; A = 9; q = 1/10$

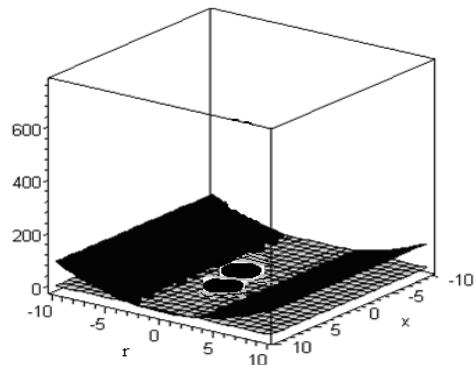


Fig. 5 The graphics of  $V_{x2}$  (black surface), and  $V_{r2}$  (gray surface) in case of  $c = 1/5; C_1 = 1; A = 9; q = 1/10$

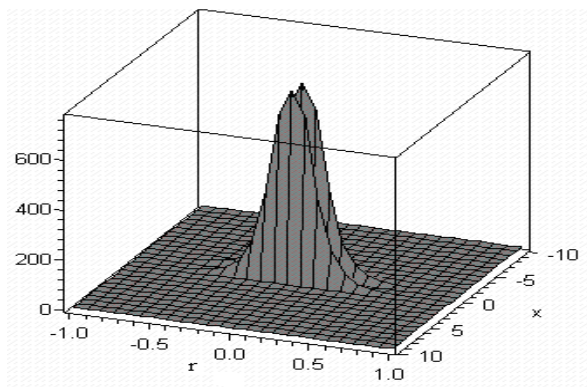


Fig. 6 The graphic of the velocity profile in case of  
 $c = 1; C_1 = 1; A = 9; q = 1/10$

#### V. CONCLUSION

The effective solutions of the system (1), (2), with the initial-boundary conditions (6), (7), in the axisymmetric case are given by the formulas 1. (13), (14); or 2. (15), (16); and these solutions represent fluid flow over the system of axisymmetric bodies, contours of which are given by the formulas (17), (18), respectively.

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#### REFERENCES

- [1] G. K. Batchelor, *An Introduction to Fluid Dynamics*, Cambridge Univ. Press, 1967.
- [2] L. D. Landau, E.M. Lifshitz, *Fluid Mechanics*, Course of Theoretical Physics, 6, Pergamon Press, 1987.
- [3] L. M. Milne-Thompson, *Theoretical Hydrodynamics*. (5-th ed) Macmillan, 1968.
- [4] G. G. Stokes, "On the steady motion of incompressible fluids". *Transactions of the Cambridge Philosophical Society* 7: 439–453, Mathematical and Physical Papers, Cambridge University Press, 1880.
- [5] H. Lamb, *Hydrodynamics* (6th ed.). Cambridge University Press, 1994.
- [6] R. Temam, *Navier-Stokes Equations, Theory and numerical Analysis*, AMS Chelsea, 2001.
- [7] B. J. Kirby, *Micro- and Nanoscale Fluid Mechanics: Transport in Microfluidic Devices*. Cambridge University Press, 2010.
- [8] Ockendon, & J. R. Ockendon, *Viscous Flow*, Cambridge University Press, 1995.
- [9] A. Chwang, and T. Wu, "Hydromechanics of low-Reynolds-number flow. Part 2. Singularity method for Stokes flows". *J. Fluid Mech.* 62(6), part 4, 1974.
- [10] S. Kim, J. Karrila, *Microhydrodynamics: Principles and Selected Applications*, Dover, 2005.
- [11] M. A. Lavrentiev & B. V. Shabat, *Problems in Hydrodynamics and their Mathematical models*. Nauka, Moscow, 1977 (in Russian).